

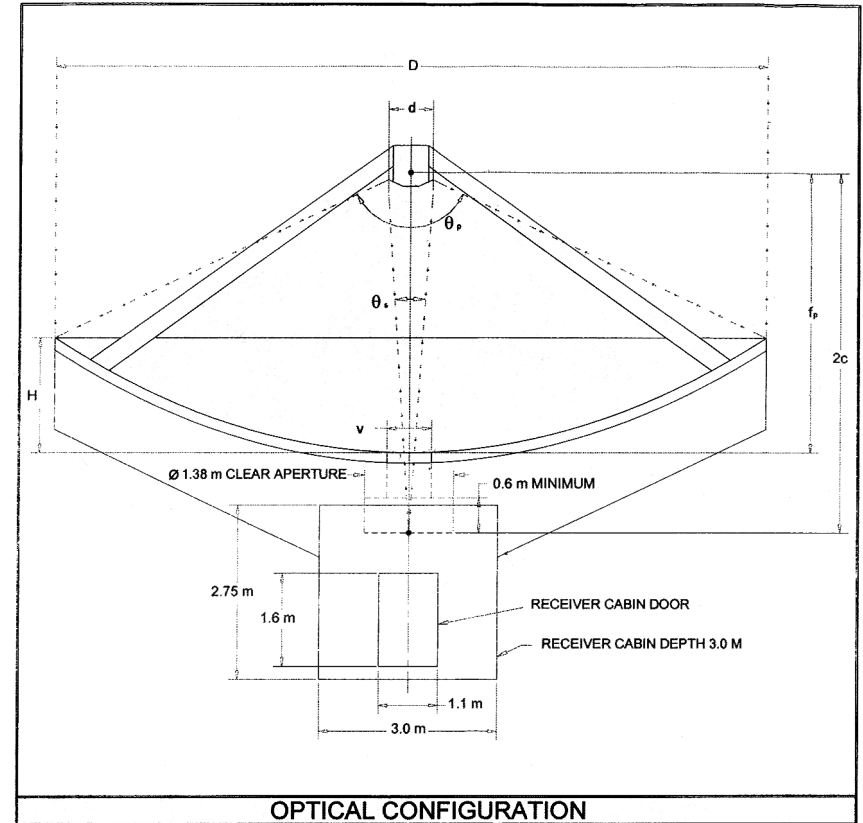
ALMA Bandpass Calibration: Standing Waves

Aurore Bacmann (ESO)

Stéphane Guilloteau (IRAM)

Standing Waves: background

- Reflection of incident wave on feed system of standing waves between receiver and sub-reflector
- On single-dish telescopes: standing waves between receiver and calibration load



ALMA antenna

Frequency of standing waves

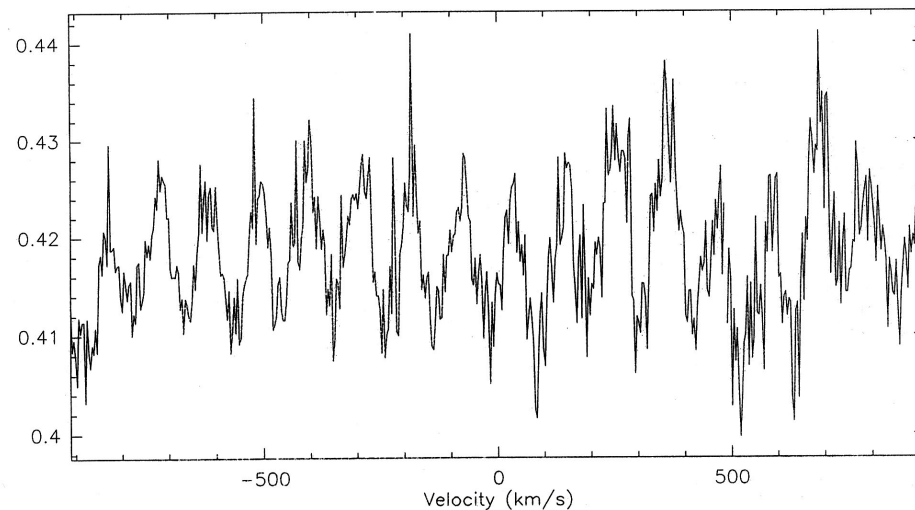
$$\nu_n = \frac{n \cdot c}{2 \cdot D}$$

Where D is the distance between the feed and the secondary

Consequence: ripple of frequency $\nu_{\text{ripple}} = \frac{c}{2D}$

Example: spectrum at the IRAM 30m

$D = 5 \text{ m} \Rightarrow \nu = 30 \text{ MHz}$



Reducing standing waves

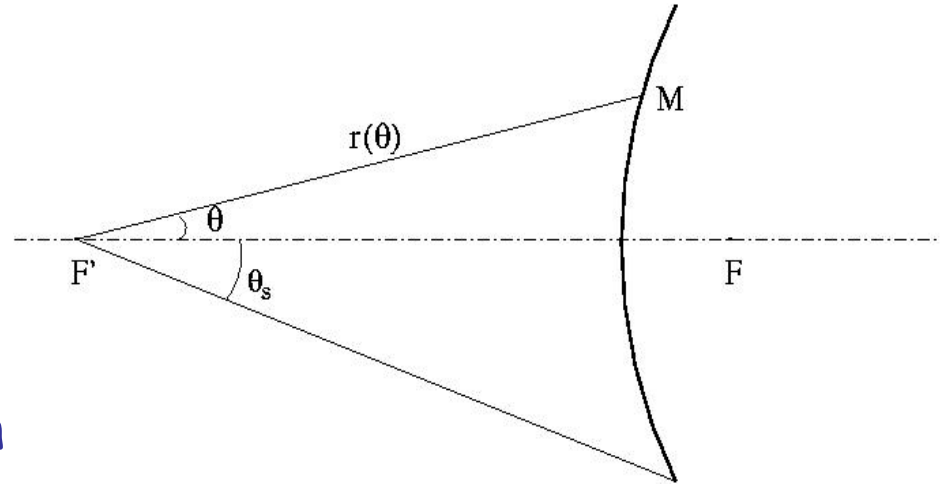
- Baseline ripple substantially degrades spectral observations
 - During observations: reflection receiver-secondary mirror "high frequency ripple"
 - During calibration scans: reflection receiver - calibration load
also end up in observed spectrum
- reducing the amplitude of the ripple \Rightarrow reducing the reflection coefficient
 - No control of the reflection on the feed
 - Need to reduce the reflection coefficient on the sub-reflector

Reflection coefficient

$$\gamma = \int_{\text{subref}} \Psi (\Psi^*)^* \cdot dS$$

$$\Psi = F(\theta) \cdot \exp(-jkr(\theta))$$

F : gaussian illumination function



$$\gamma = \int_0^{\theta_s} 2\pi \cdot F^2(\theta) \sin(\theta) \exp(-2jkr(\theta)) d\theta$$

Asymptotical expression

$$\gamma = \frac{2\pi}{2jkLe(e-1)} \times \left[F^2(\theta_0)(e \cos(\theta_0) - 1)^2 \exp(-2jkr(\theta_0)) \right. \\ \left. - F^2(\theta_s)(e \cos(\theta_s) - 1)^2 \exp(-2jkr(\theta_s)) \right]$$

e: eccentricity

L: distance to mirror vertex

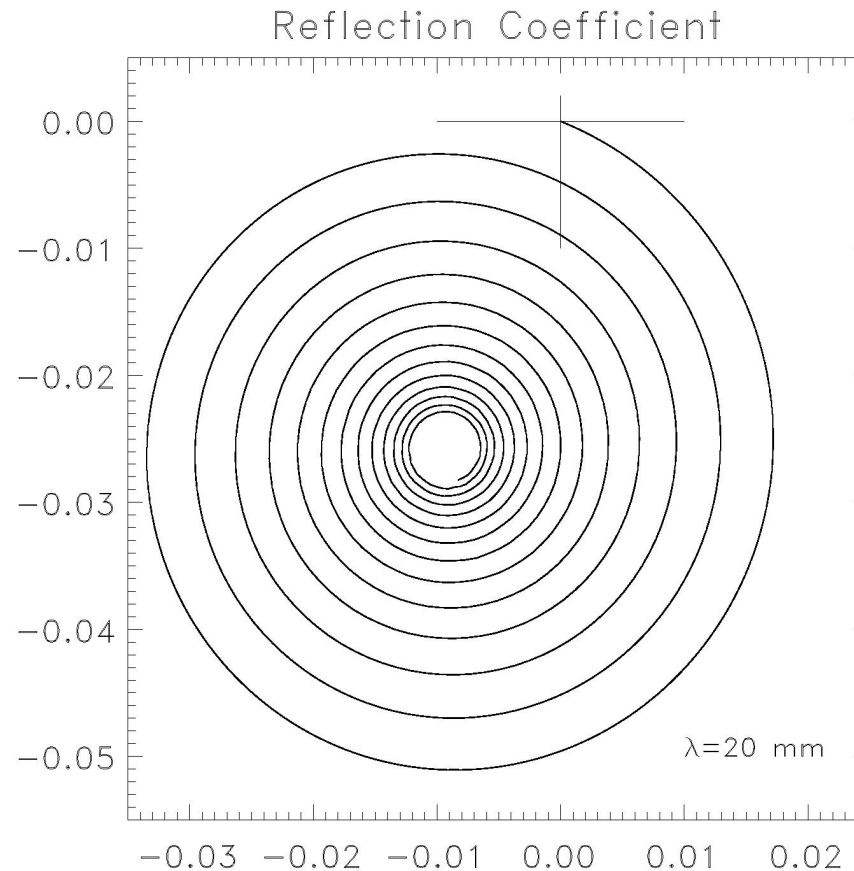
Due to gaussian tapering, the second term can be neglected

$$\Rightarrow \gamma \propto \lambda$$

Standing waves are most disturbing at long wavelengths

If both terms are considered: γ will oscillate with λ around an increasing mean value

Representation of reflection coefficient in the complex plane



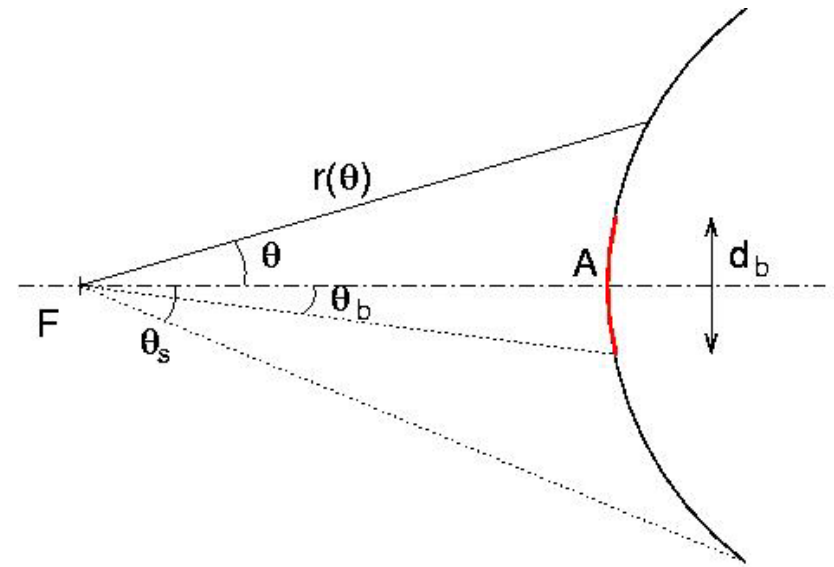
Considered Sub-reflector Geometries

Study of the effect of various sub-reflector geometries on the reflection coefficient

- Effect of an absorber on the blocage zone
- Effect of a discontinuity (aperture in sub-reflector)
- Effect of a scattering cone

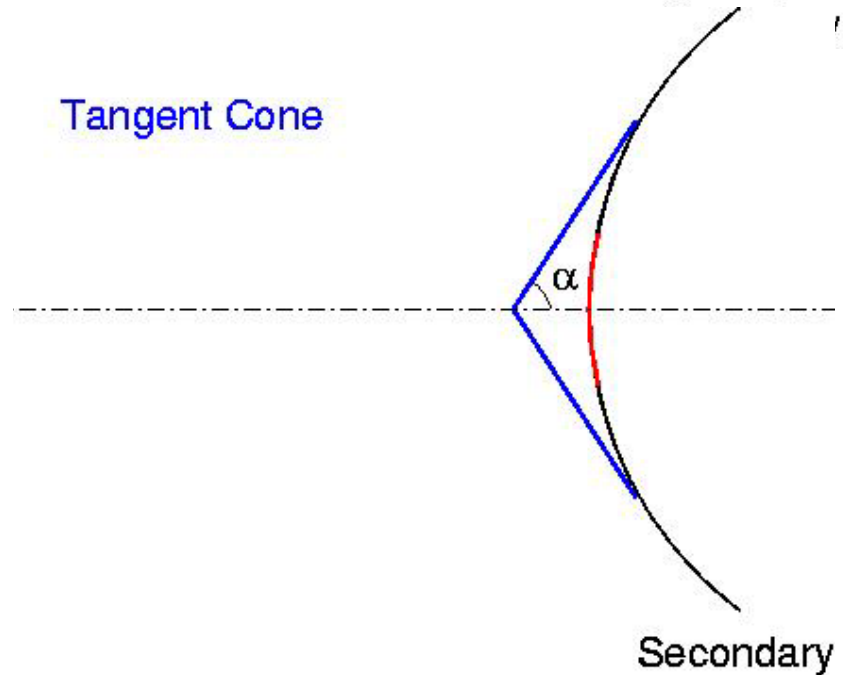
Mirror alone

Mirror with absorbing disk
between 0 and θ_b

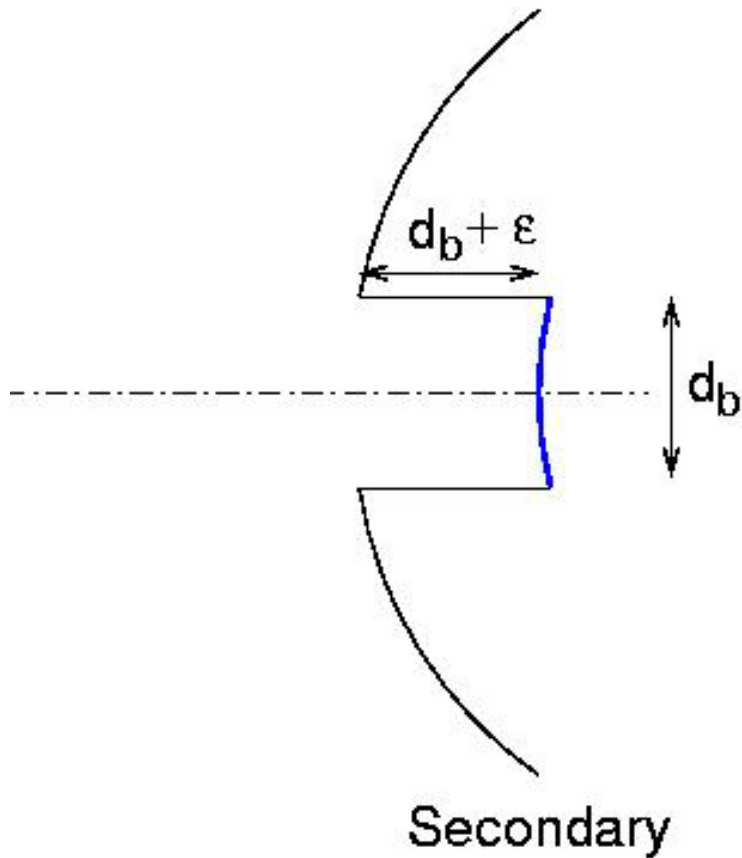


Tangent Cone

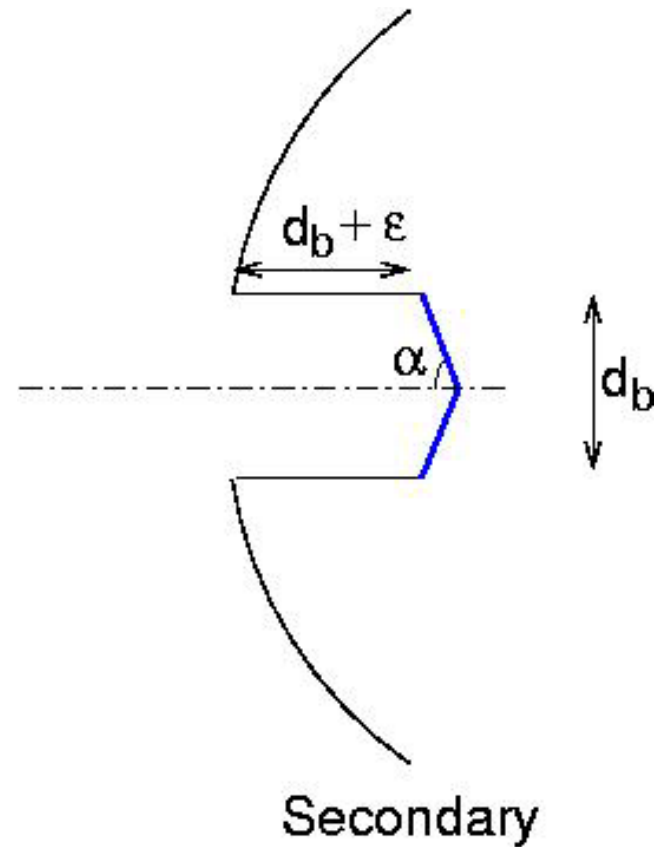
Mirror with tangent cone
of semi-angle α



Sub-reflector with aperture



Sub-reflector with aperture, cone within aperture



Possible design for sub-reflector

Aperture in sub-reflector

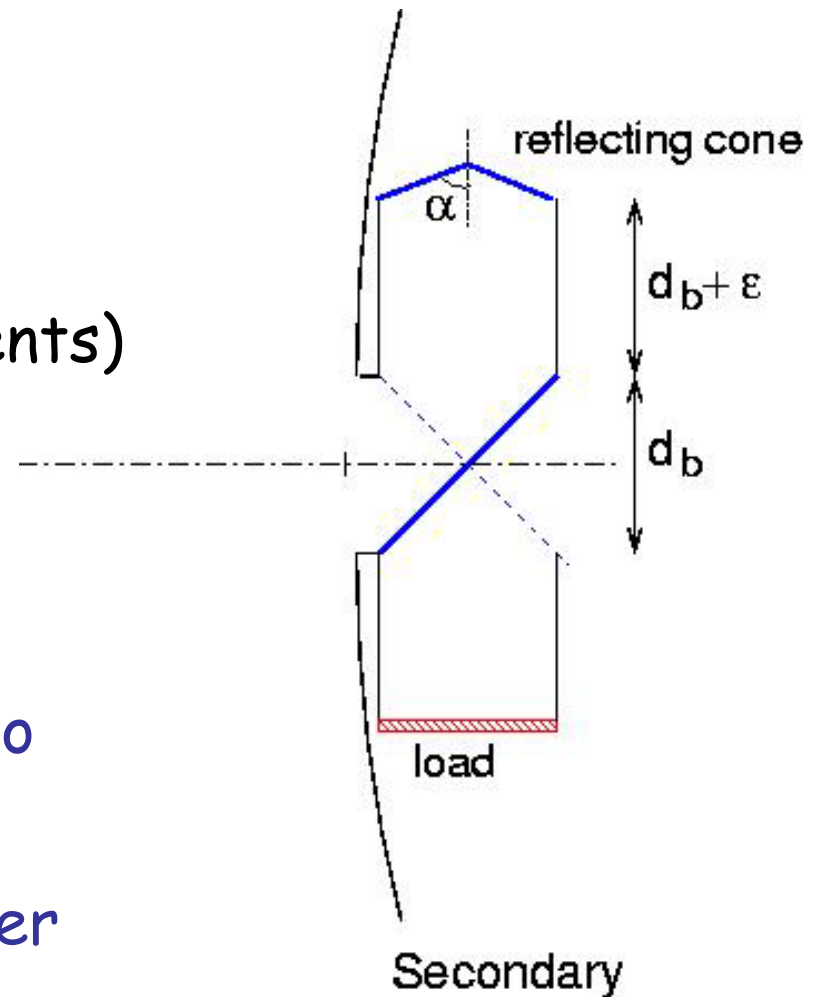
45° mirror

deflecting light towards

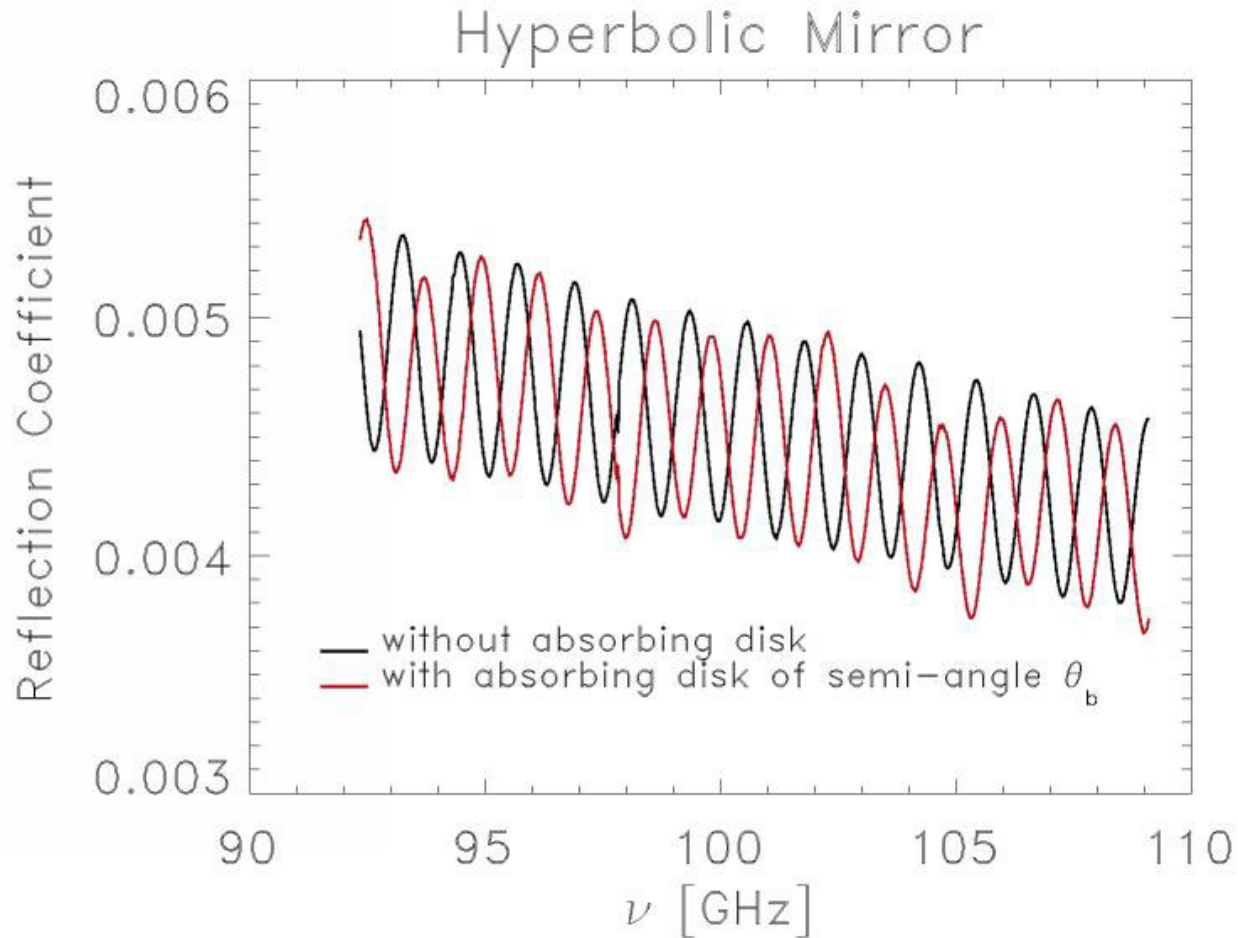
- load (calibration measurements)
- cone (observations)

Calibration: coupling of load to receiver ~ 1%

⇒ Avoids saturation of receiver

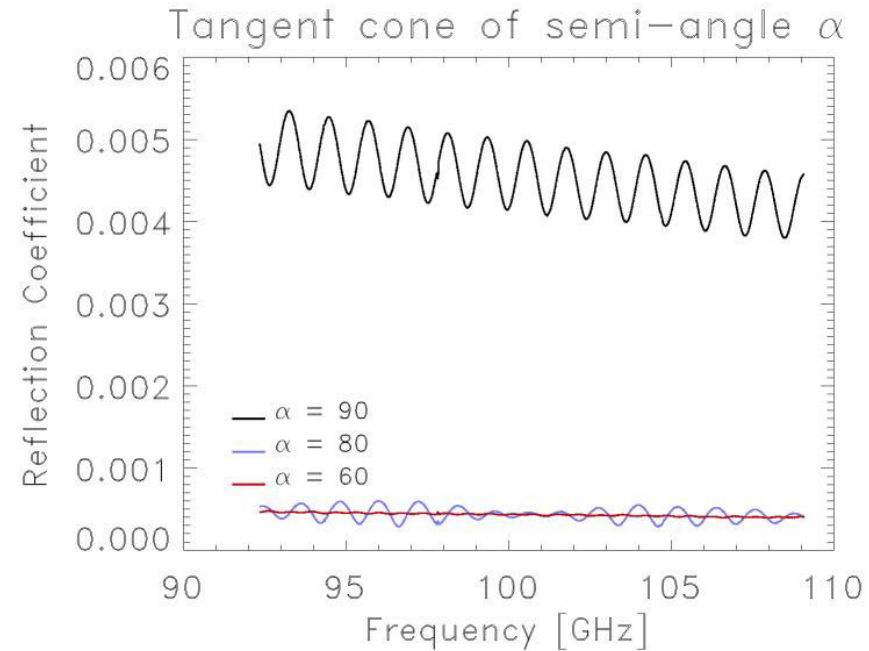
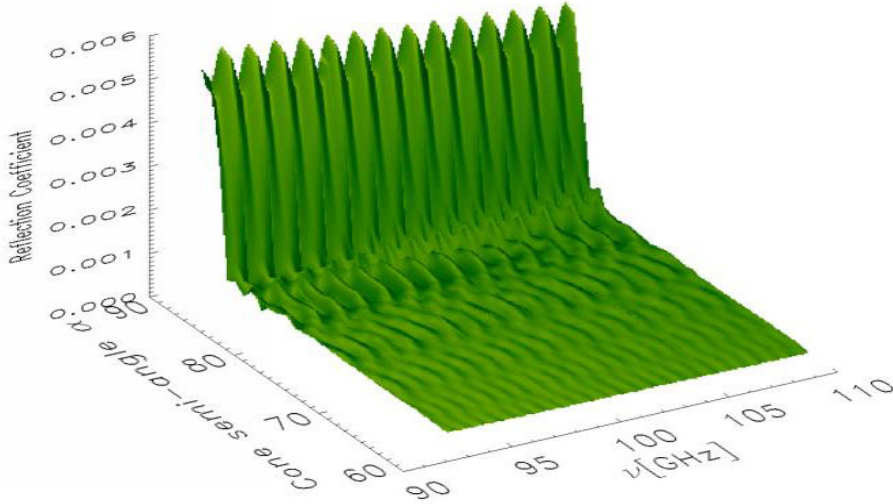


Simple sub-reflector



Tangent cone on Sub-reflector

3 mm

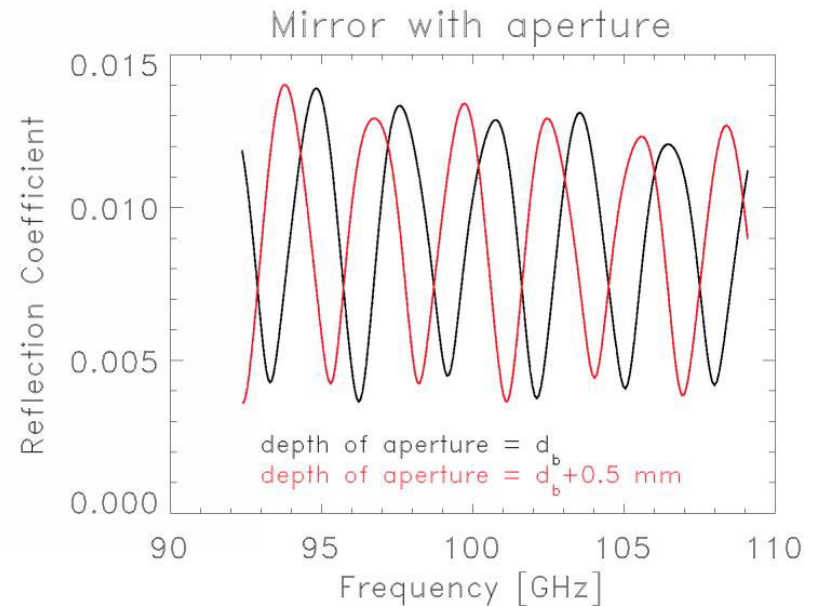
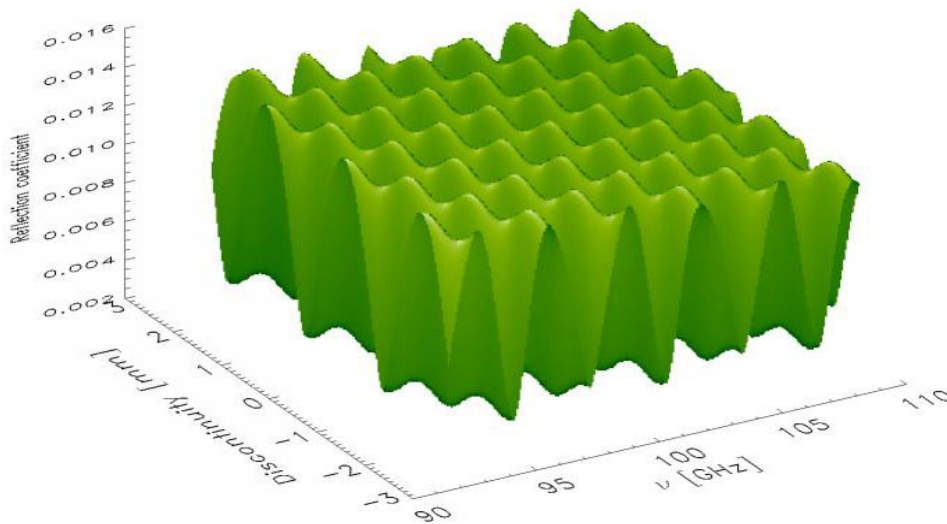


$$\Rightarrow \alpha < 87^\circ$$

But if α is small, the cone covers much of the sub-reflector

Sub-reflector with discontinuity

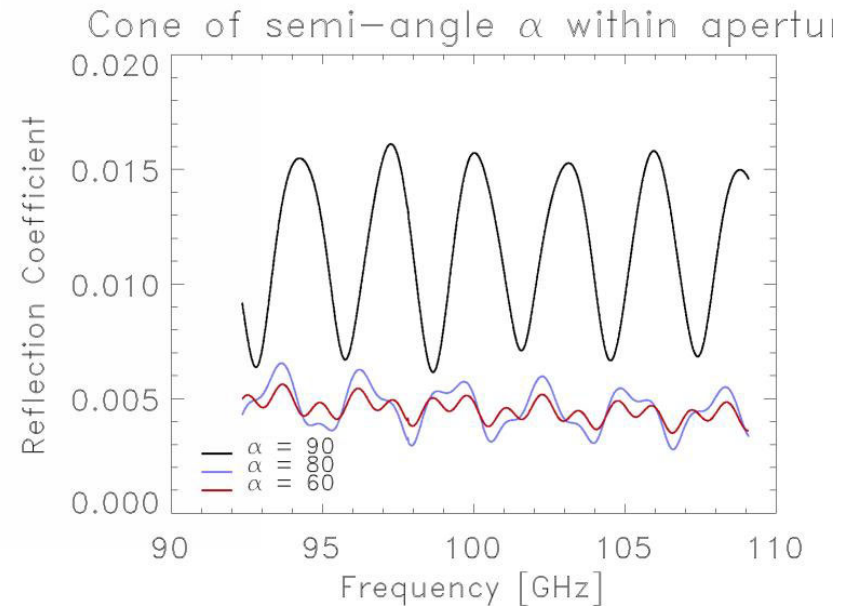
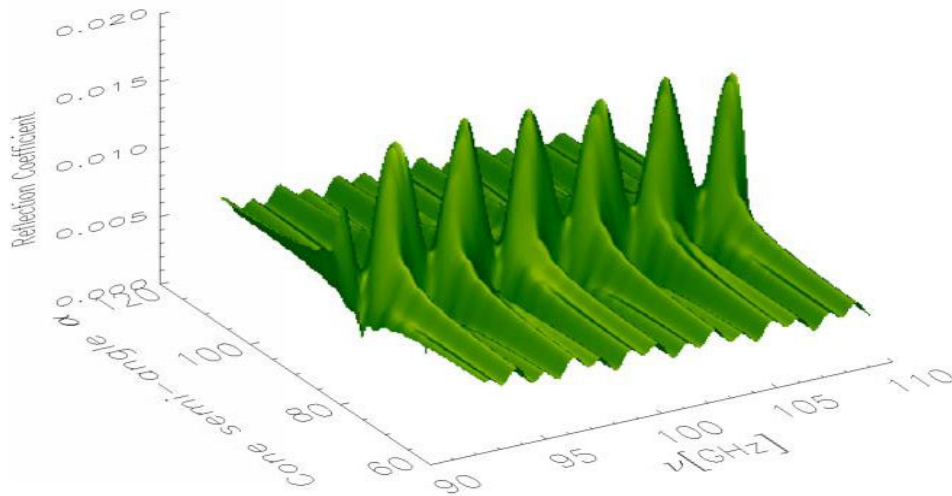
at 3 mm



$\gamma \sim 0.009$ with discontinuity
 $\gamma \sim 0.0045$ with absorbing disk

Aperture with cone

at 3 mm

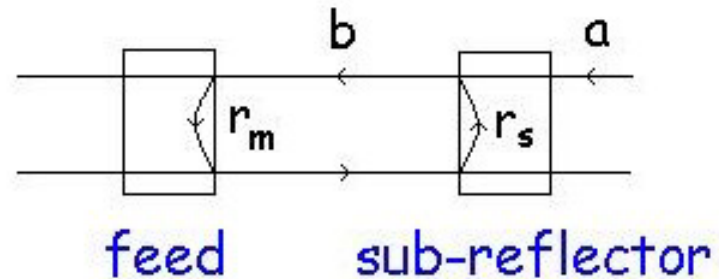


At angles $< 85^\circ$, $\gamma \sim$ same value as without aperture (0.005)

Standing Wave Ratio

- Incident amplitude on the feed:

$$b = \frac{a \cdot t_s}{1 - r_s r_m \exp(-2j\psi)}$$



In amplitude: $\frac{|b_{\max}|}{|b_{\min}|} \approx 1 + 2 \cdot r_s r_m$

In power: $\frac{P_{\max}}{P_{\min}} \approx 1 + 4 \cdot r_s r_m$

Values for ALMA

peak-to-peak ripple at 3mm

For $r_m \sim 0.4$

Absorbing disk	0.7%
Tangent cone	0.08%
Aperture without cone	1.3%
Aperture with cone	0.8%

Summary

- At 3 mm, baseline ripple can reach ~1%
- Aperture in sub-reflector increases ripple by a factor of 2
- Can be reduced with cone within aperture
- Tangent cone is the best solution but choice of α = compromise