

# Turnstile Junction Orthomode Transducer

An option for EVLA X-Band Receiver

X-Band OMT Design Review Meeting; AOC, Socorro; October 1, 2009



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Expanded Very Large Array  
Robert C. Byrd Green Bank Telescope  
Very Long Baseline Array



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1. Introduction
2. Selection process
3. Optimization, analysis
4. Mechanical design
5. Measurements
6. Conclusions

# Specifications of X-band OMT

Bandwidth 8 to 12 GHz (1.5:1 BW ratio)

Return loss > 25 dB

Insertion loss ≤ 0.2 dB

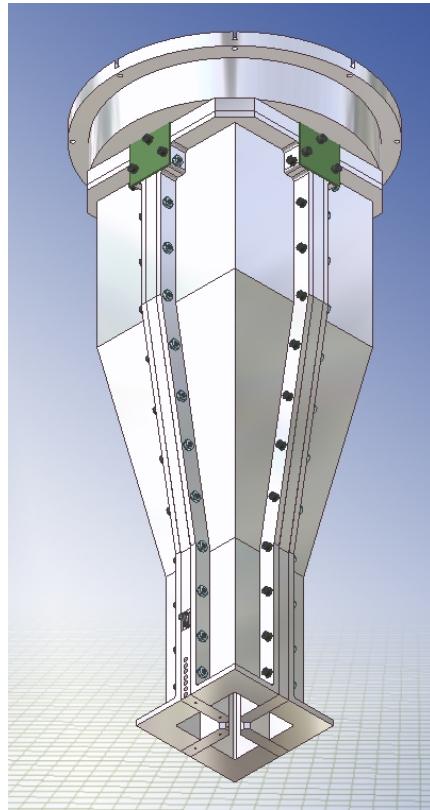
Crosspolarization ≤ -40 dB

Isolation ≤ -40 dB

Size ??????

Weight ?????

# Septum Polarizer, Quadridged OMT



Septum Polarizer Length ~ 3.75" ( $2.7\lambda$ ); BW ratio 1.28:1

L-band Quadridged OMT scaled to 8 to 12 GHz; Length = 3.975" ( $3.4\lambda$ )

BW ratio 2:1

# Boifot Junction OMT

Lengths:

Circular-square transition = 2.318"

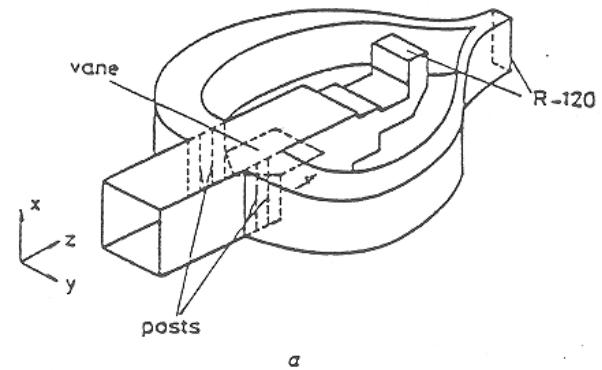
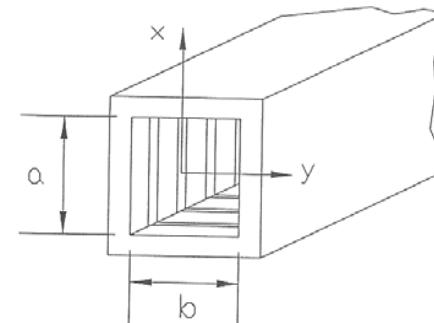
Phase shifter = 7.875" (6.67 $\lambda$ )

45 twist = 3.454"

Boifot OMJ = 6.400" (5.4 $\lambda$ )

Total = 20.047"

(OMJ scaled from Ka-band)



BW ratio ~1.5:1

# Symmetrical and Odd-symmetrical modes

Anton M. Beifot — Classification of Ortho-Mode Transducers

$$\lambda_c = \frac{2}{\sqrt{\left(\frac{m}{x_1}\right)^2 + \left(\frac{n}{y_1}\right)^2}}$$

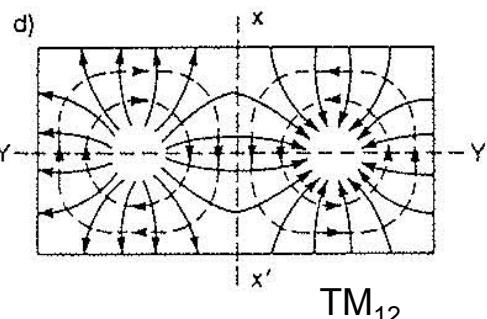
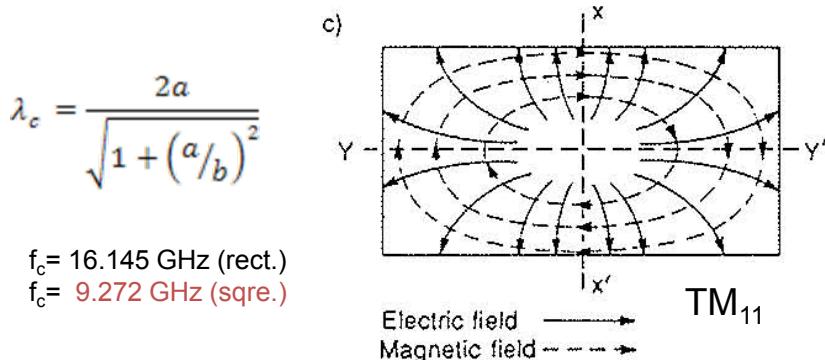
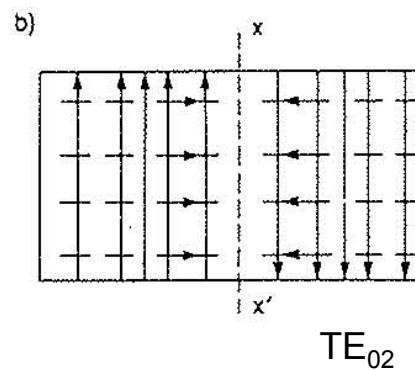
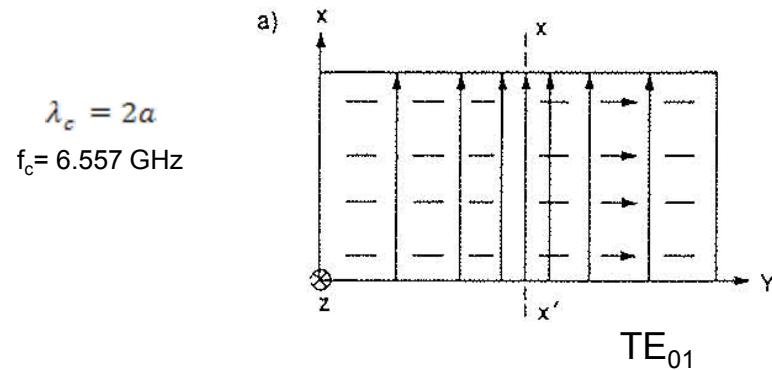
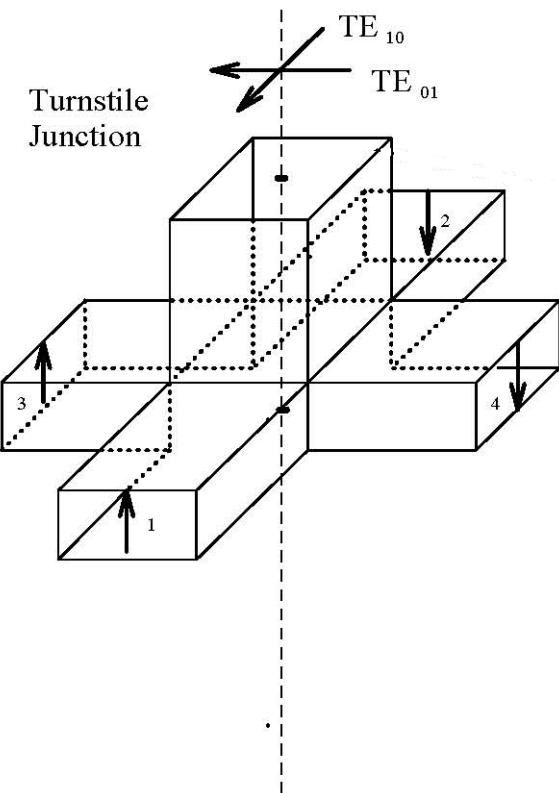
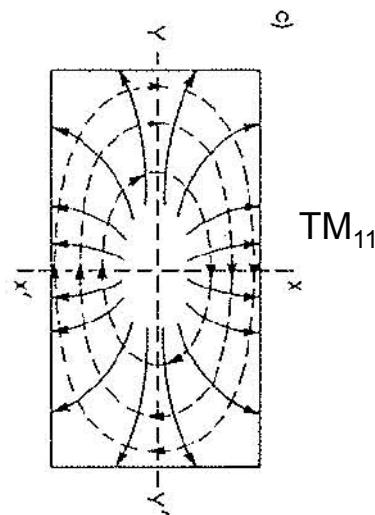
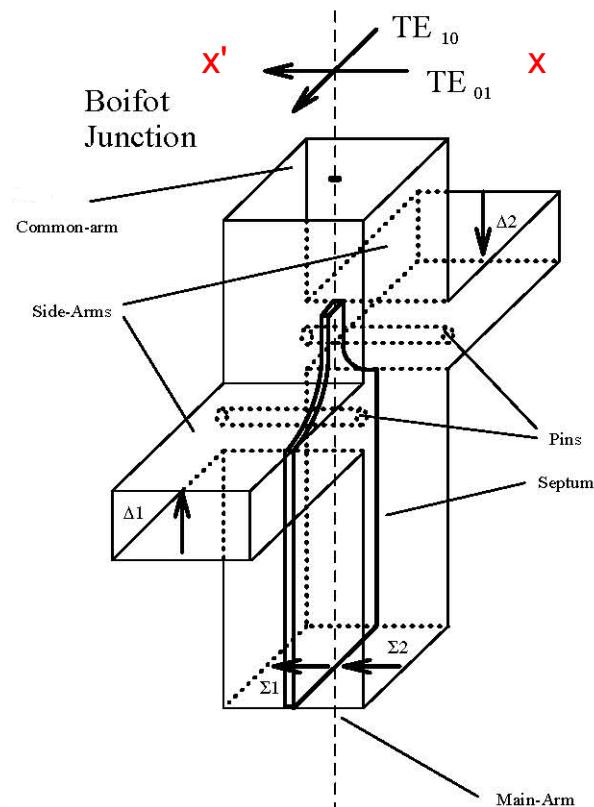


Fig. 1 - Definition of symmetry. The  $\text{TE}_{01}$  mode in a) is symmetrical about  $XX'$ , the  $\text{TE}_{02}$  mode in b) has odd symmetry about  $XX'$ , the  $\text{TM}_{11}$  mode in c) is symmetrical both about  $XX'$  and  $YY'$ , while the  $\text{TM}_{12}$  mode in d) has odd symmetry about  $XX'$  and symmetry about  $YY'$ .

# Turnstile Junctions



# E-plane, H-plane bends

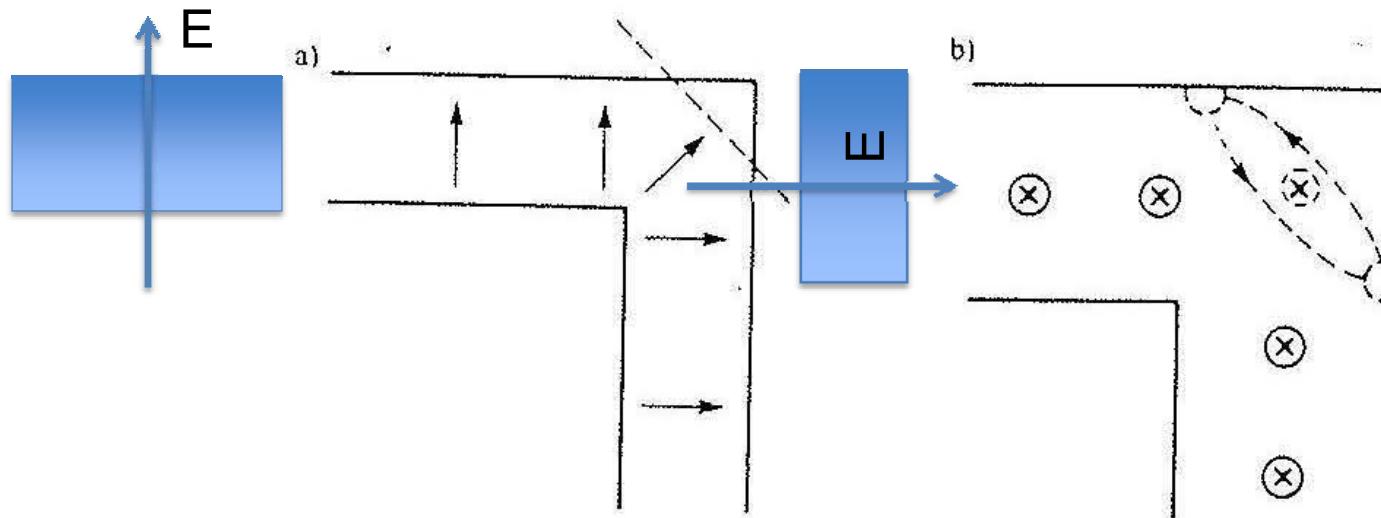
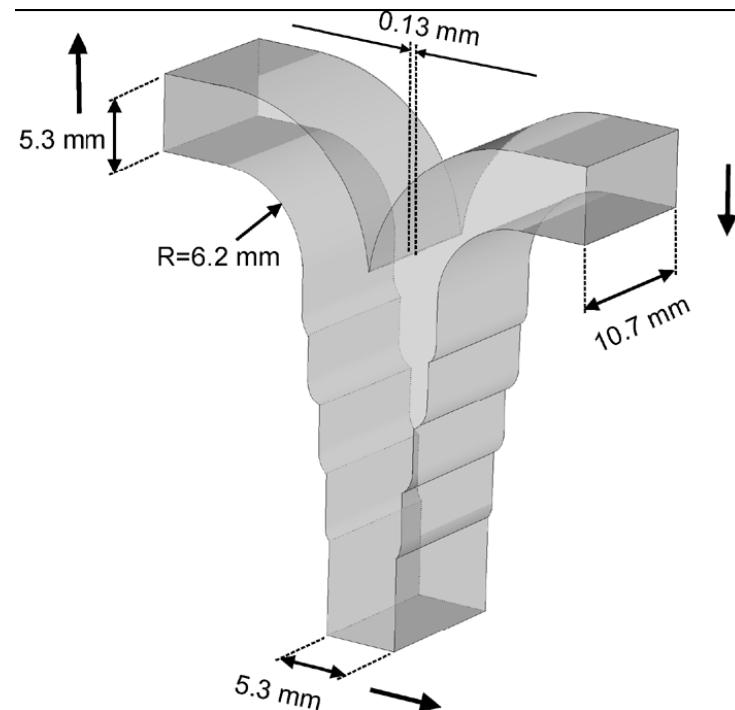
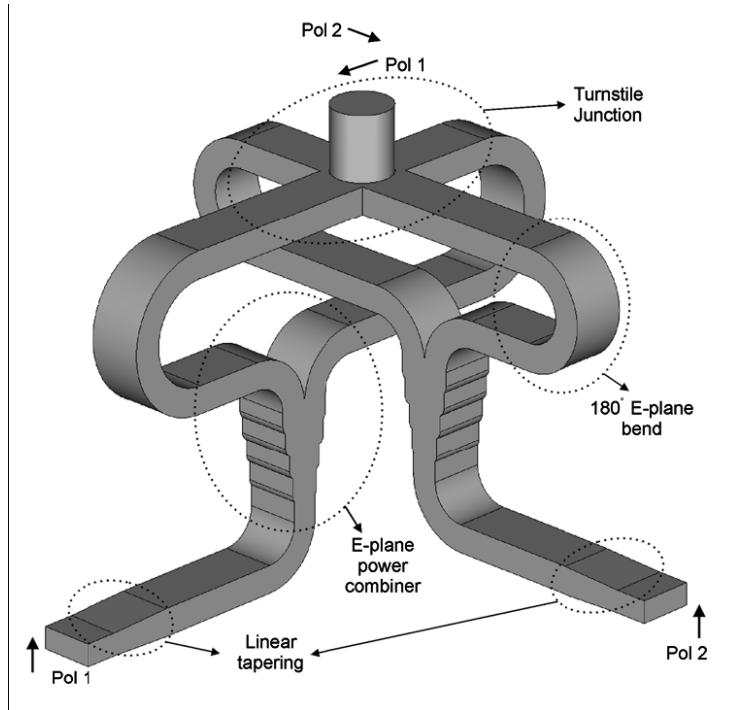


Fig. 4 - Corners with different matching properties. The *E*-plane bend in a) generates only symmetrical modes, while the *H*-plane bend in b) generates both symmetrical and odd symmetrical modes.

# A Turnstile Junction Waveguide Orthomode Transducer

A. Navarrini and R. L. Plambeck

EVLA



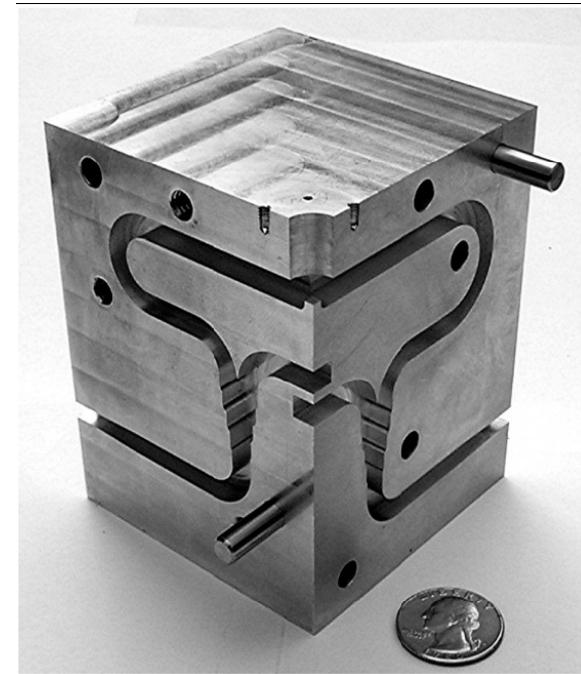
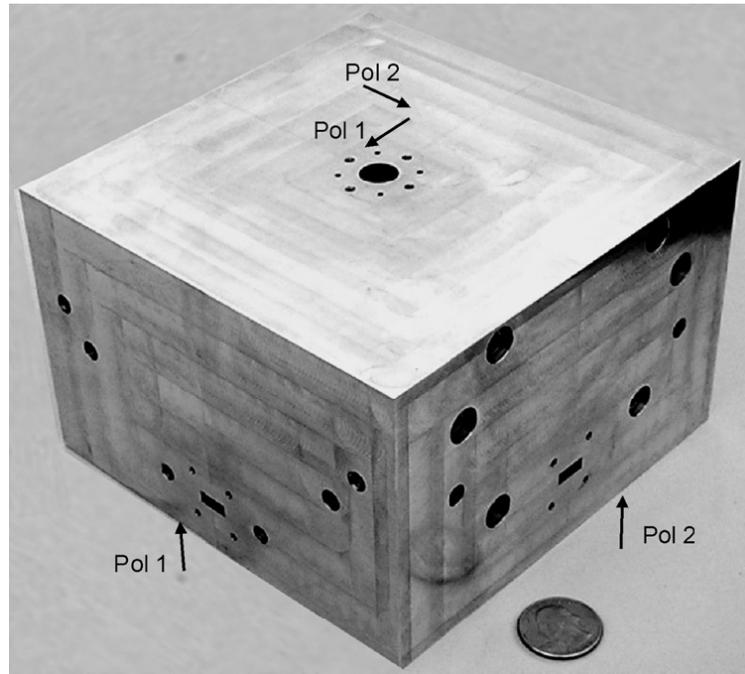
18-26 GHz; Circ. Dia=0.457"; Waveguide=0.420"x0.208"; Stub: 0.173"x0.173"x0.087"; Prototype for 210 to 270 GHz

$S_{11} < -23$  dB (Turnstile jn.) ;  $S_{11} < -32$  dB (combiner) ; Linear taper to 0.420"x0.170" –  $S_{11} < -33$  dB



# A Turnstile Junction Waveguide Orthomode Transducer

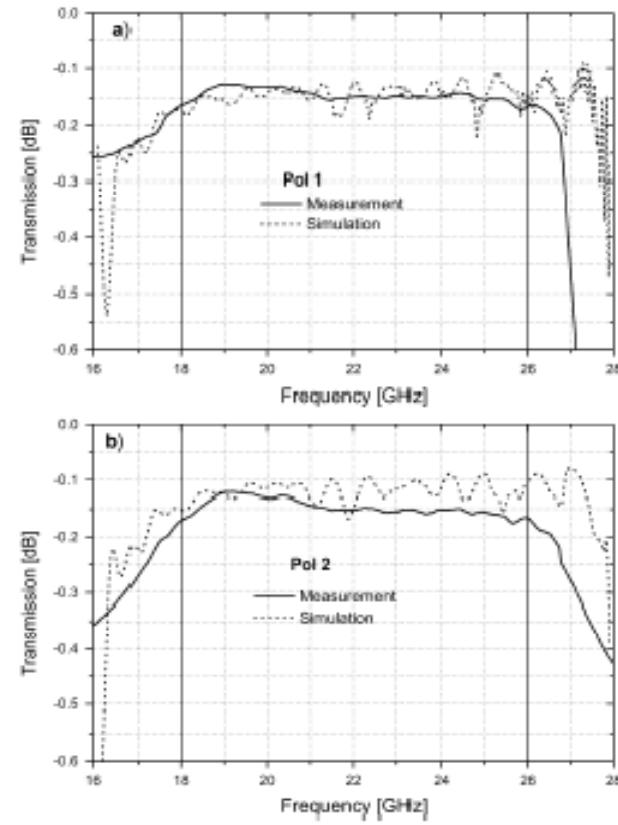
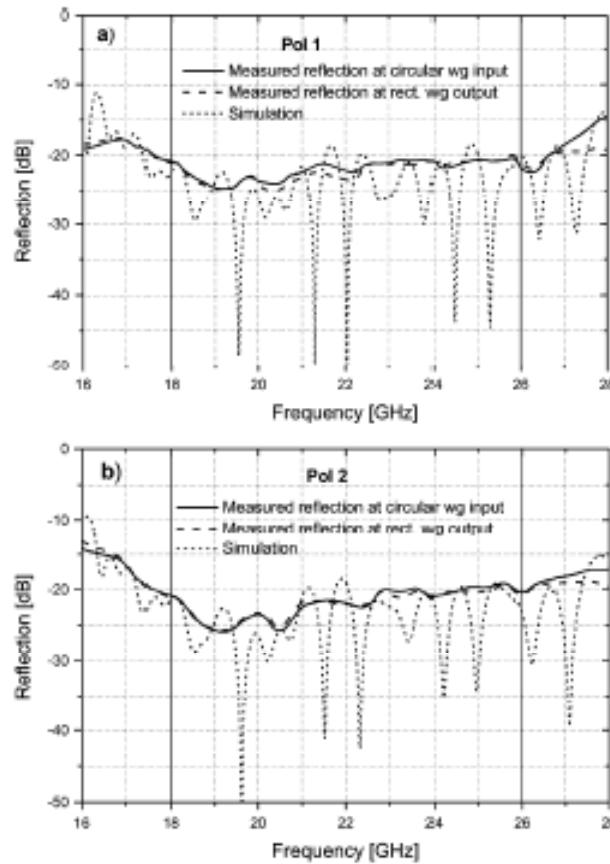
A. Navarrini and R. L. Plambeck



Split in E-planes; Path length = 9.84" (25 cms); External dim: 5.8"x5.8"x3.8"

# A Turnstile Junction Waveguide Orthomode Transducer

A. Navarrini and R. L. Plambeck



S11 < -19 dB; S21 ~ -0.15 dB; Isolation <-48 dB; (over 1.44:1 BW)

Scaling to X-band 13"x13"x8.5"

# Double Ridged Orthogonal Mode Transducer for the 16-26 GHZ Microwave Band

Alex Dunning

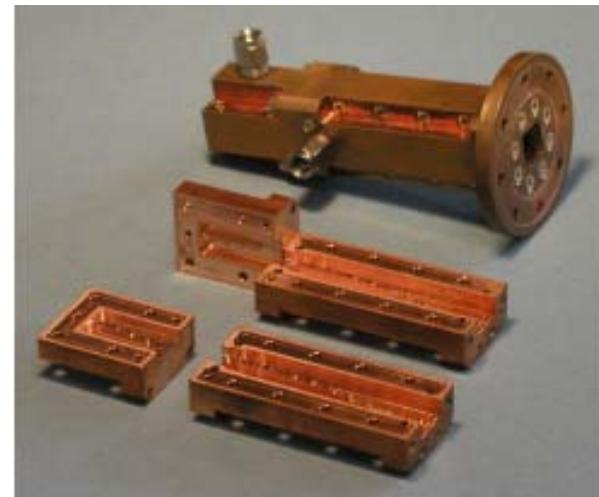
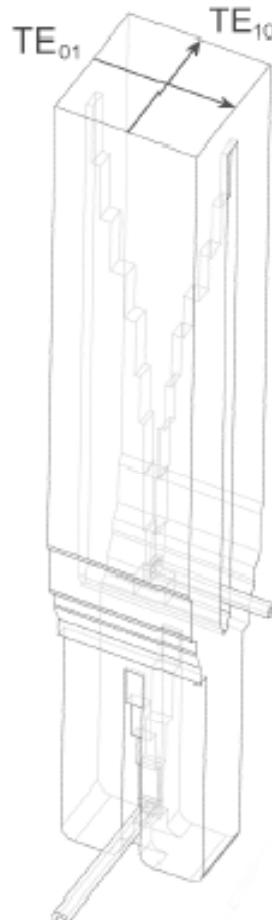


Figure 1a. Complete copper OMT and split sections

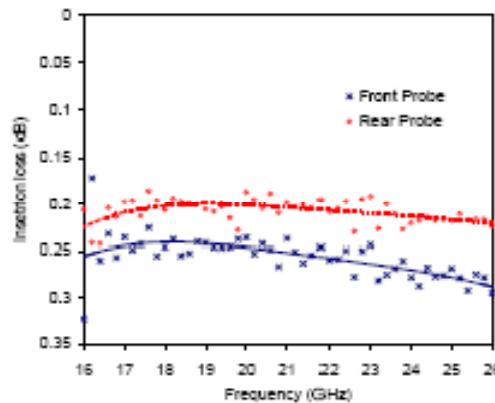
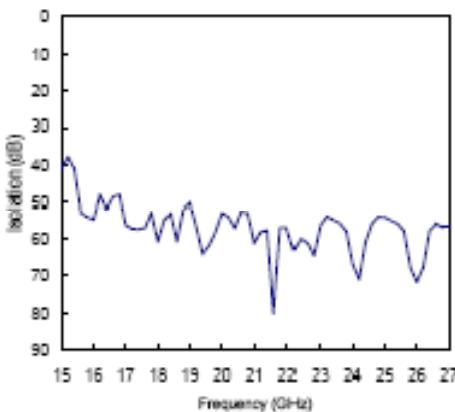
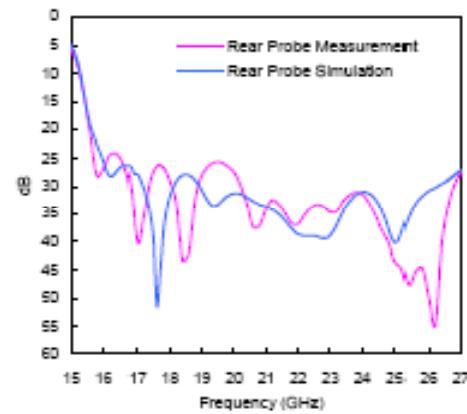
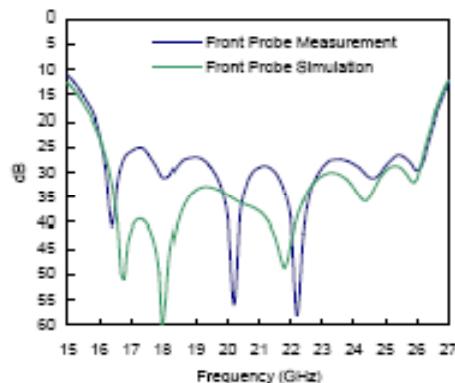
Split planes perpendicular to ridges

9 steps for  $TE01$ ; Ridge  $t=0.055"$   
NOT SYMMETRICAL; All modes except  $TE10$  cut off in Rect. Wg.

# Double Ridged Orthogonal Mode Transducer for the 16-26 GHz Microwave Band

Alex Dunning

EVLA



$S_{11} < -25$  dB; Isolation  $< -40$  dB; Insertion loss  $< -0.25$  dB (frnt);  $< -0.20$  dB (rear) over 1.6:1 BW

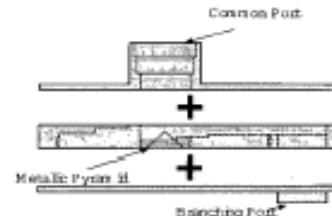
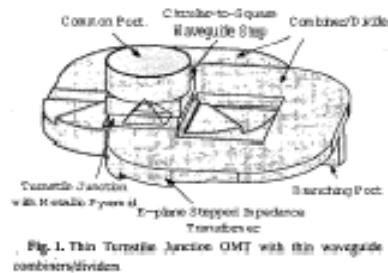
Length = 3.4" (16 – 26 GHz)

Scaling to X-band L=7.3"

# Ultra-Thin Broadband OMT with Turnstile Junction

Y. Aramaki, N. Yoneda, M. Miyazaki and T. Horie  
Mitsubishi Electric Corporation

## Ku-band (10-15 GHz)



Circ. To Sq. transition – dia : 0.945", I step: 0.748"x0.748", II step: 0.630"x0.630 "

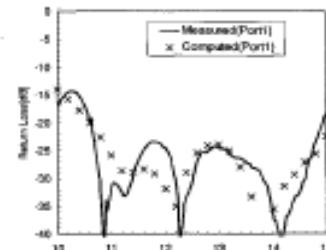
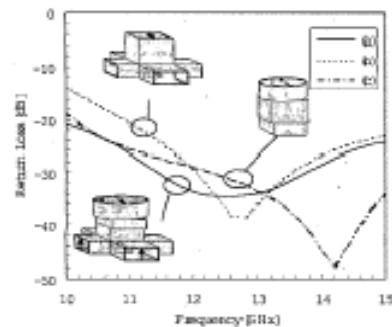
Turnstile Jnc.- Rect. Waveguide 0.630"x0.315", Pyrmd. Stub 0.394"x0.394"x0.275"

Combiner – E-pln stepped imp. Transformer, H-pln bend, E-pln T-junction 0.630"x0.236"  
( $h=0.315$  to  $0.118$ )

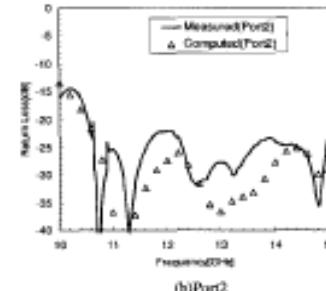
# Ultra-Thin Broadband OMT with Turnstile Junction

EVLA

Y. Aramaki, N. Yoneda, M. Miyazaki and T. Horie  
Mitsubishi Electric Corporation



(a) Port1



(b) Port2

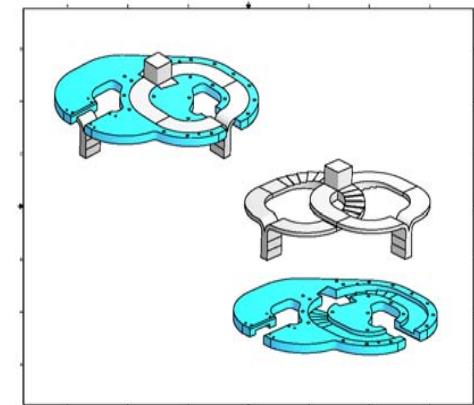
$S_{11}$  : Turnstile jnc. with stub <-14 dB (10-15); <-20 dB (11.5-15)  
Turnstile jnc. with stub + Cir. To sq. step <-20 dB (10-15)

OMT  $S_{11}$  <-22 dB (11-15); <-15 dB (10-15)  
Insertion loss <0.1 dB  
Isolation better than -40 dB

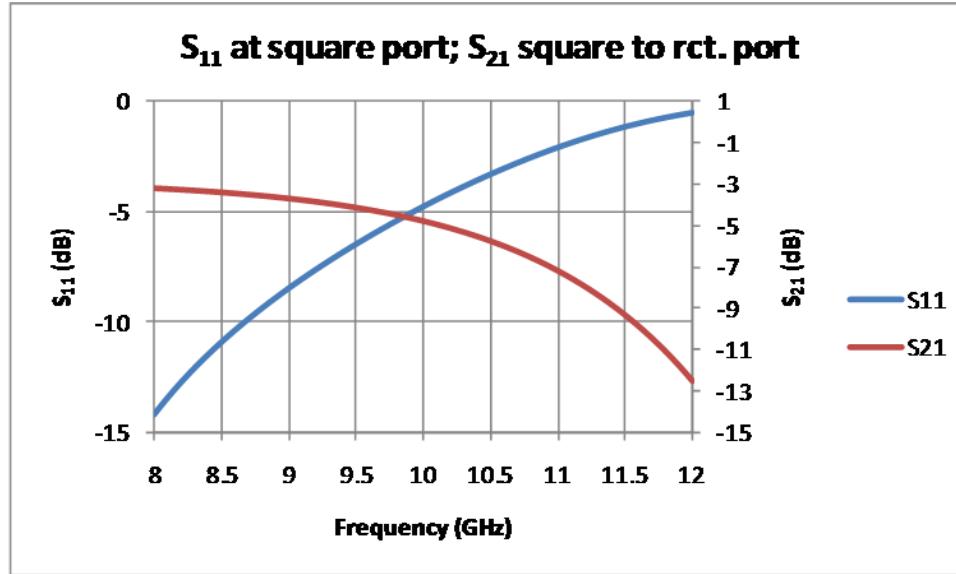
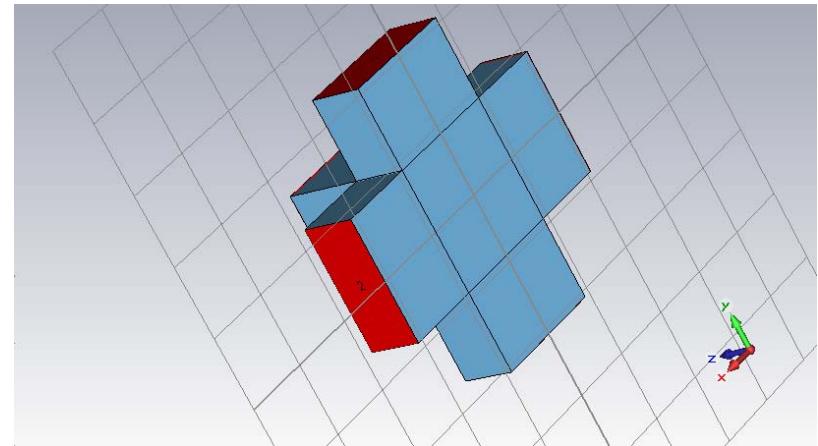
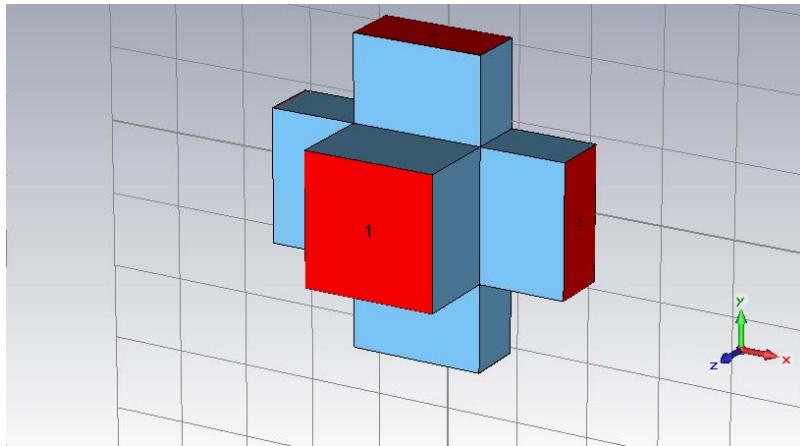
Height from bottom of II step to bottom of combiner = 0.800";  
Cross-section dia ~ 5.5"  
Scaling to X-band : Ht = 1.000"; Dia = 7.0"

# Optimization Of Components Of The OMT

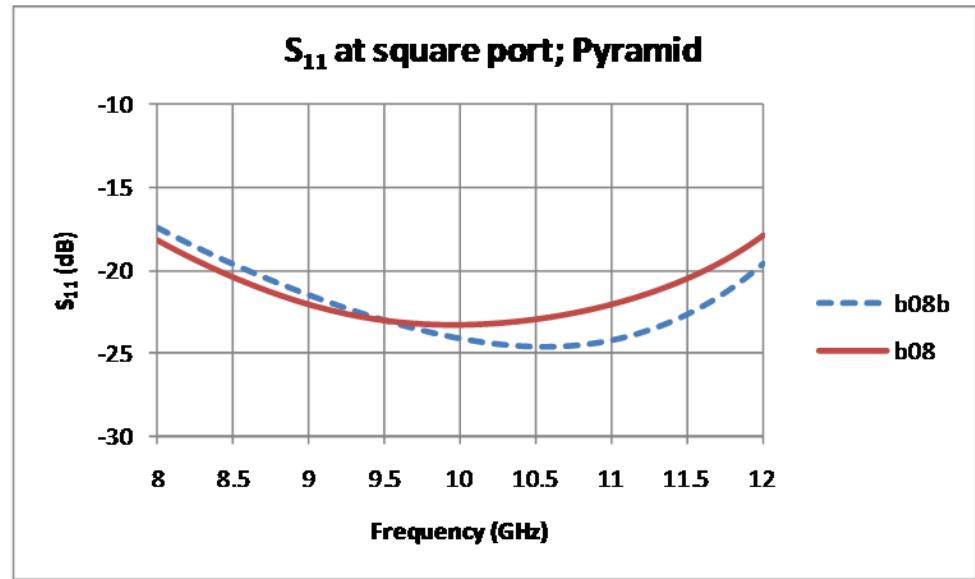
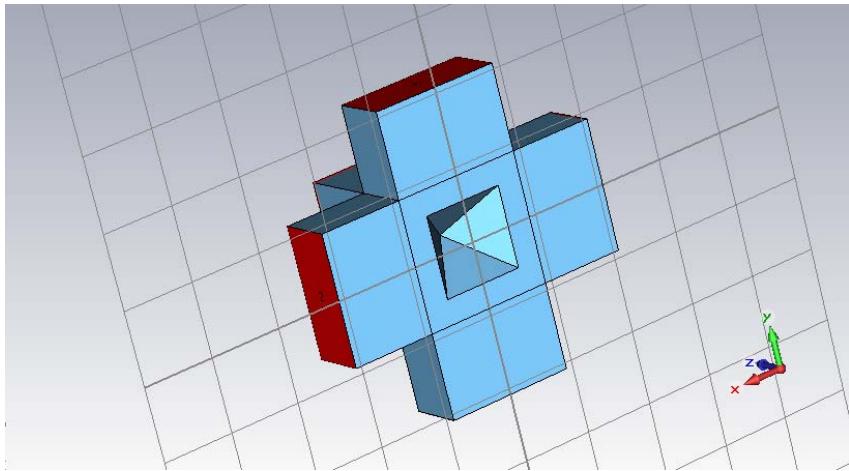
- 1. Turnstile Junction
- 2. Side arms with waveguide bends
- 3. 0.900x0.400 to 0.900x0.180 stepped transformer
- 4. Y-Junction
- 5. 0.900x0.380 to 0.900x0.400 stepped transformer
- Used CST Microwave Studio in all the optimization and analysis



# Turnstile Junction

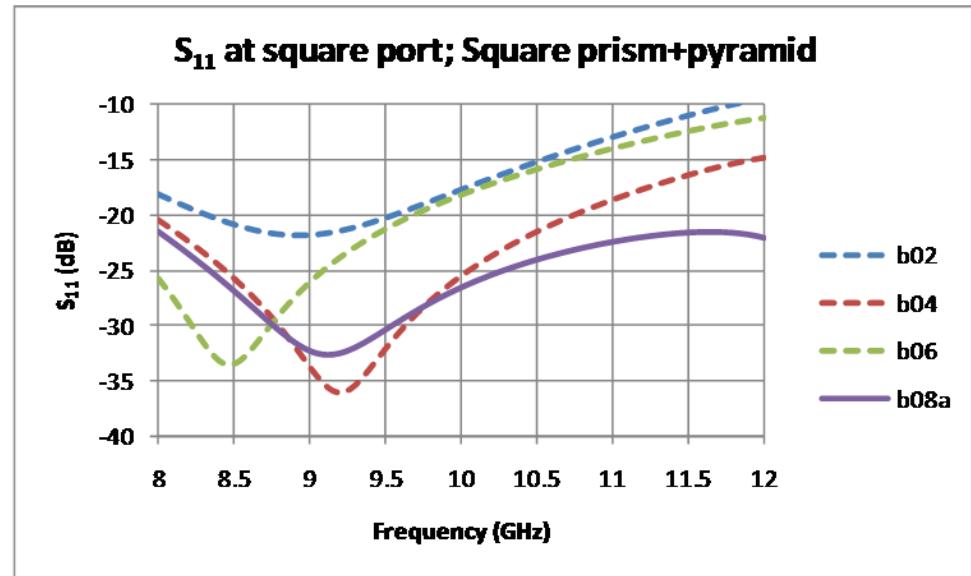
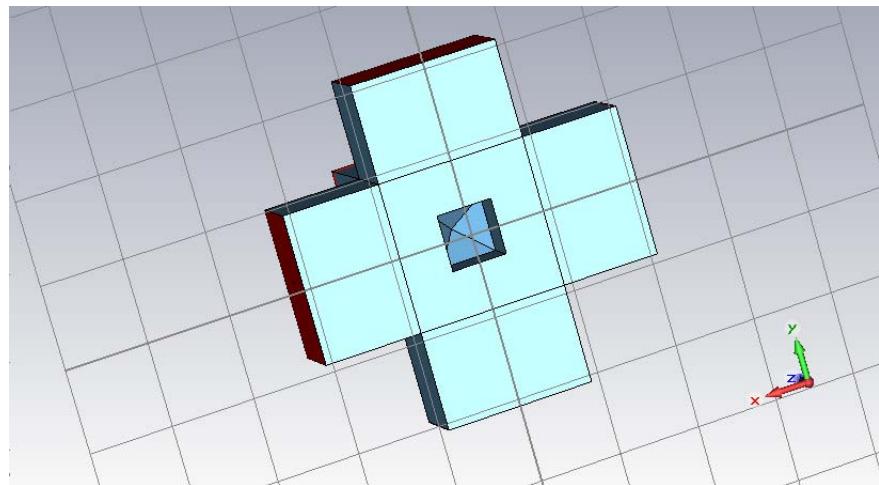


# Turnstile Junction with pyramidal stub



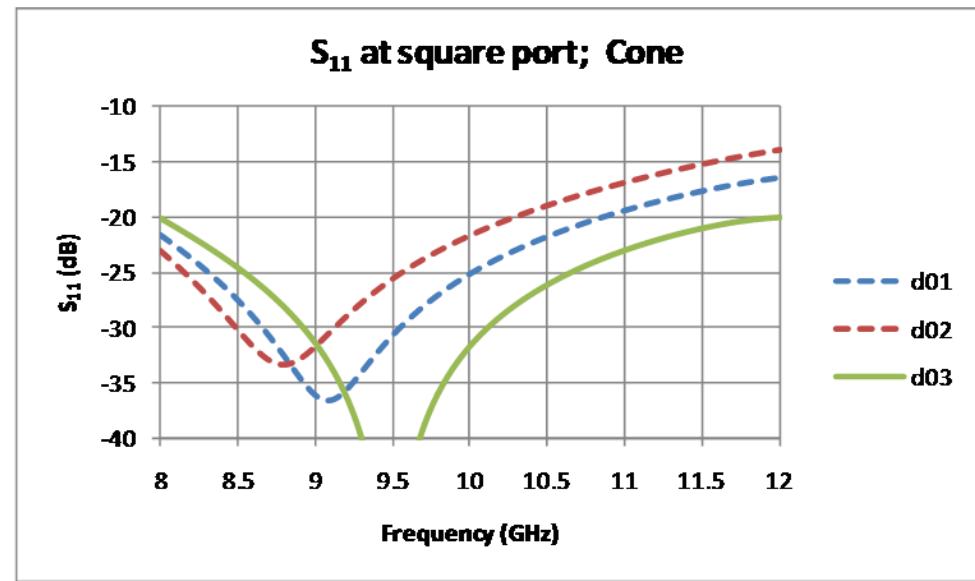
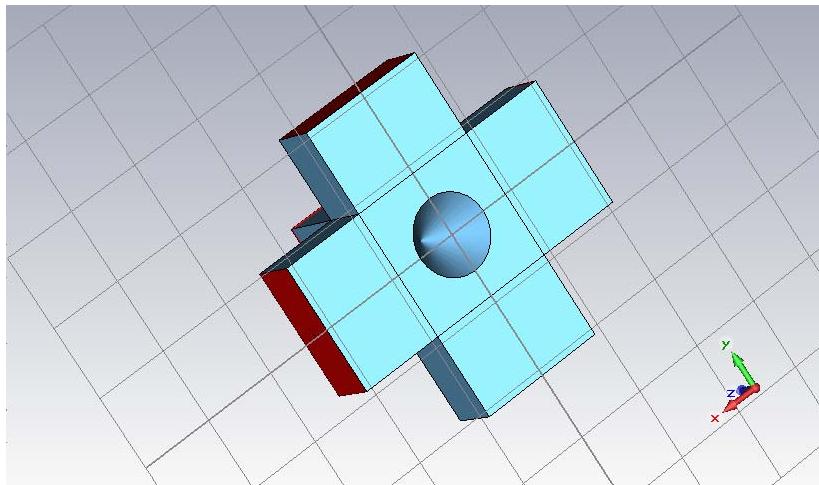
	side	py
b08b	0.562	0.394*
b08	0.562	0.373
$S_{11} \leq$	-17.9	

# Turnstile Junction with square prism + pyramid stub



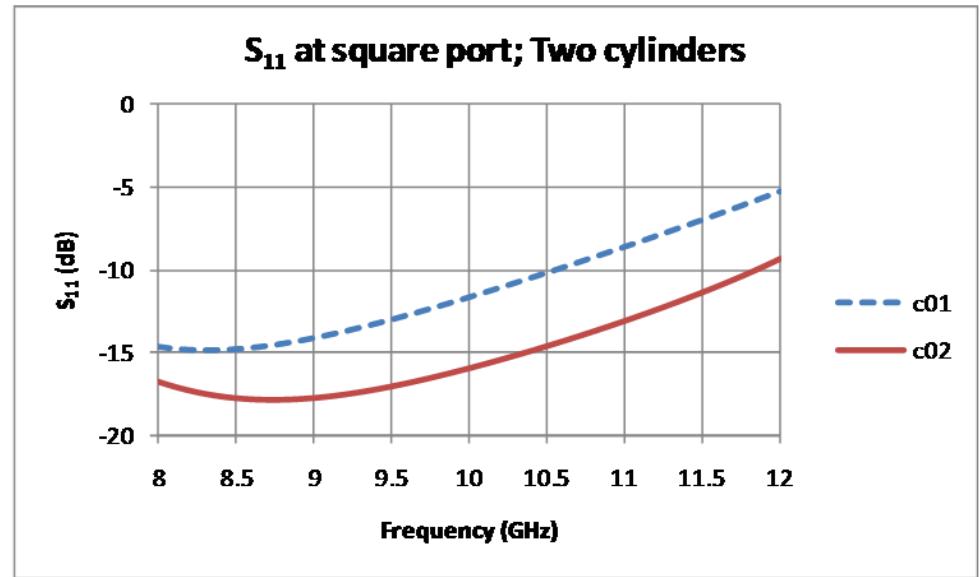
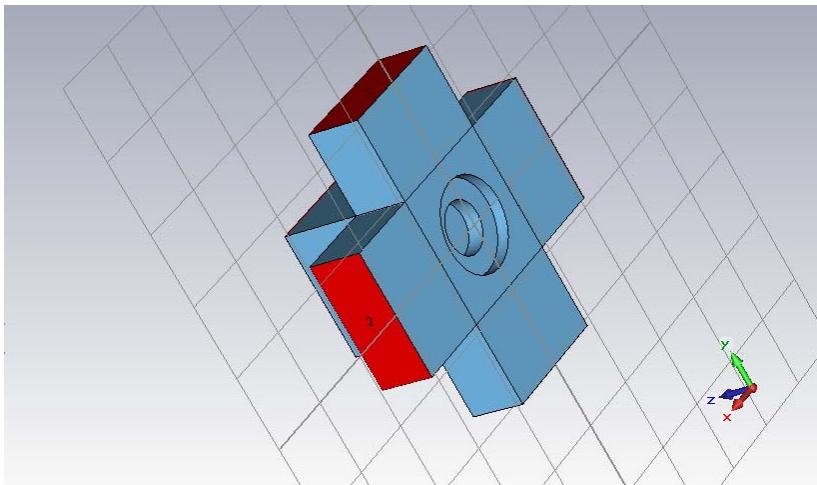
	side	h	pyh
b02	0.335	0.210	0.200
b04	0.335	0.210	0.100
b06	0.300	0.210	0.090
b08a	0.335	0.210	0.030
$S_{11} \leq$	-21.4		

# Turnstile Junction with conical stub



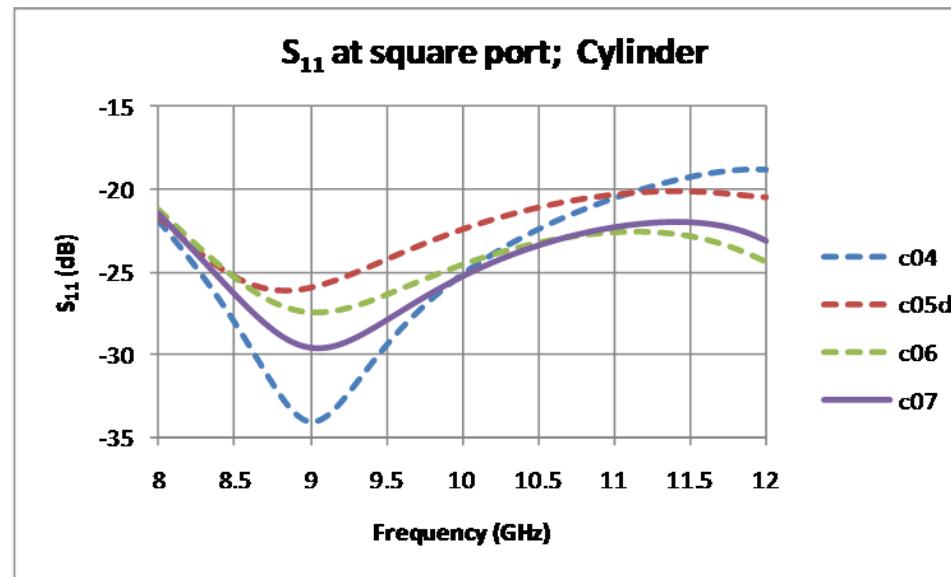
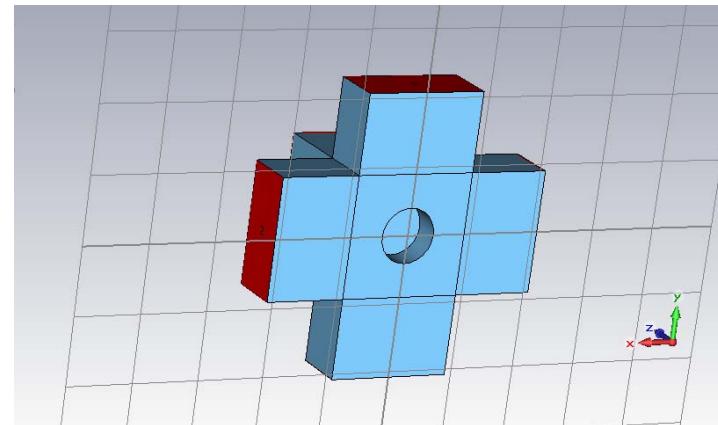
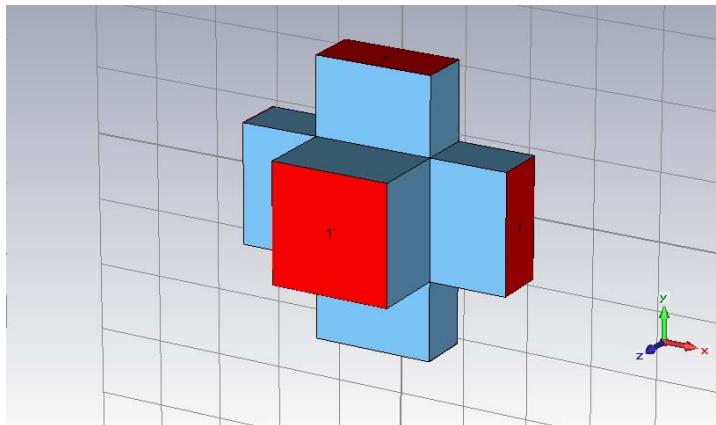
	dia	ht
d01	0.530	0.445
d02	0.510	0.445
d03	0.550	0.450
$S_{11} \leq$	-20.0	

# Turnstile Junction with 2 cylinders



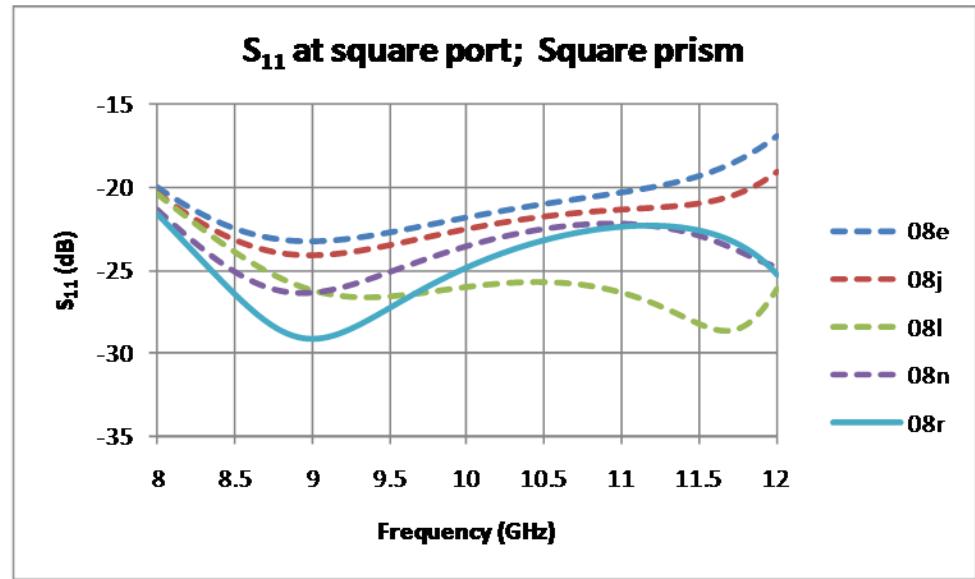
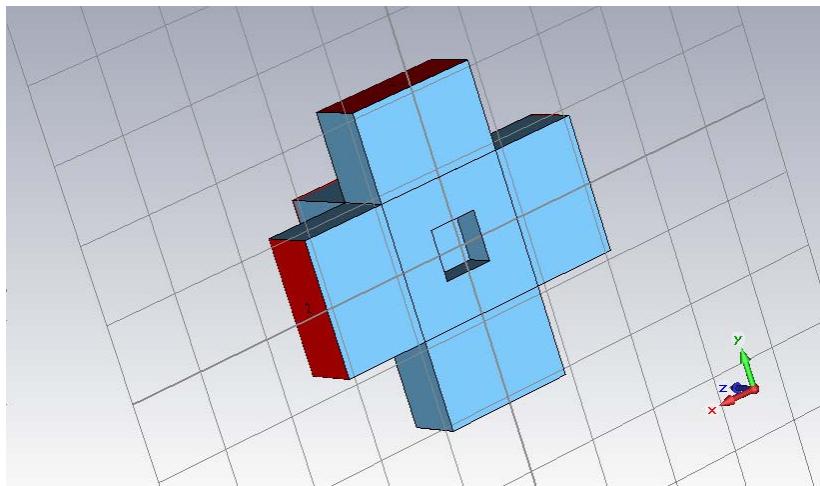
	D	H	d	h
c01	0.705	0.096	0.325	0.184*
c02	0.635	0.086	0.358	0.202
S <sub>11</sub>	≤ -9.4			

# Turnstile Junction with cylindrical stub



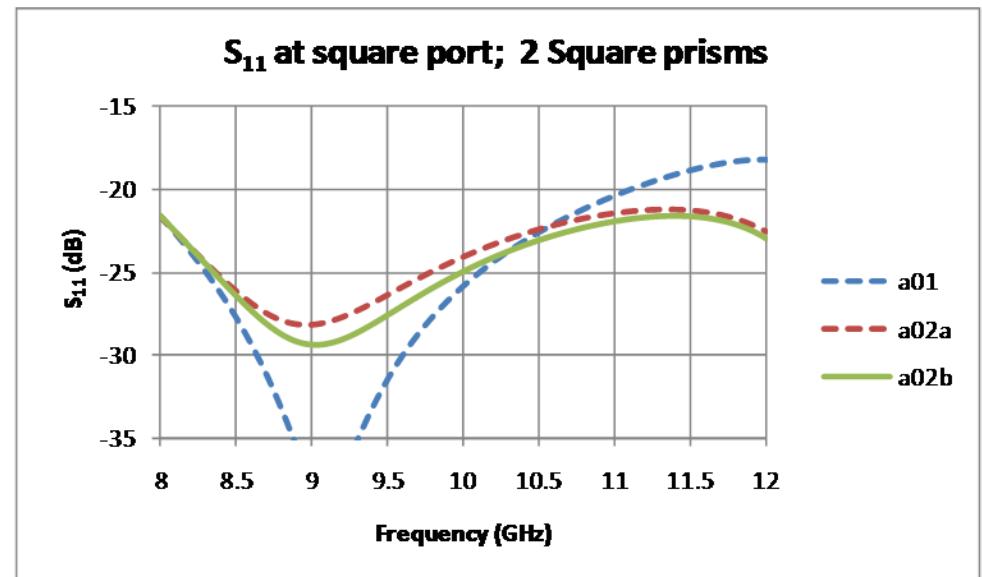
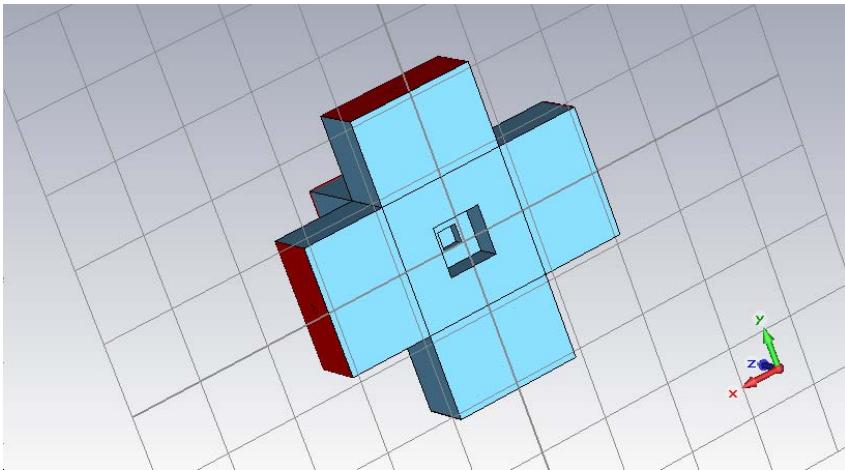
	Dia.	Ht.
c04	0.385	0.217
c05d	0.405	0.195
c06	0.405	0.200
c07	0.396	0.207

# Turnstile Junction with square prism



side	ht	$S_{11}$ (dB)
08e	0.371	0.186 *
08j	0.363	0.190
08l	0.355	0.200
08n	0.345	0.200
08r	0.335	0.210 **used this design
$S_{11} \leq -21.6$		

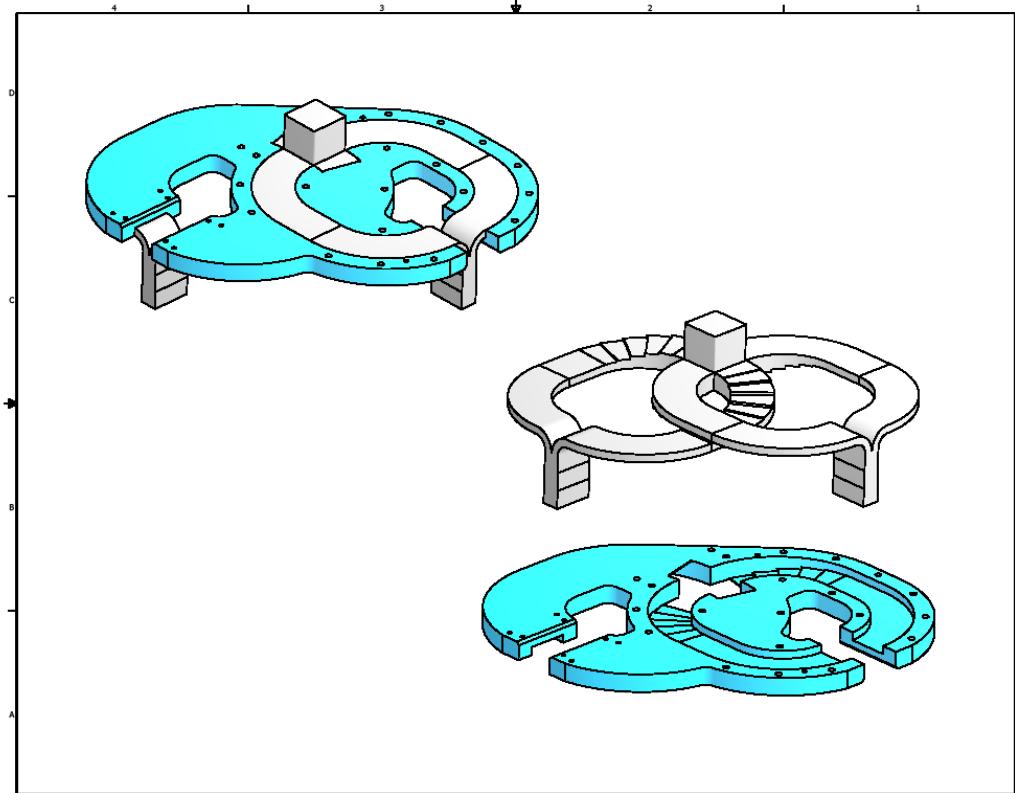
# Turnstile Junctions with 2 square prisms



	s1	h1	s2	h2
a01	0.335	0.210	0.128	0.080
a02a	0.348	0.192	0.128	0.080
a02b	0.346	0.195	0.134	0.076

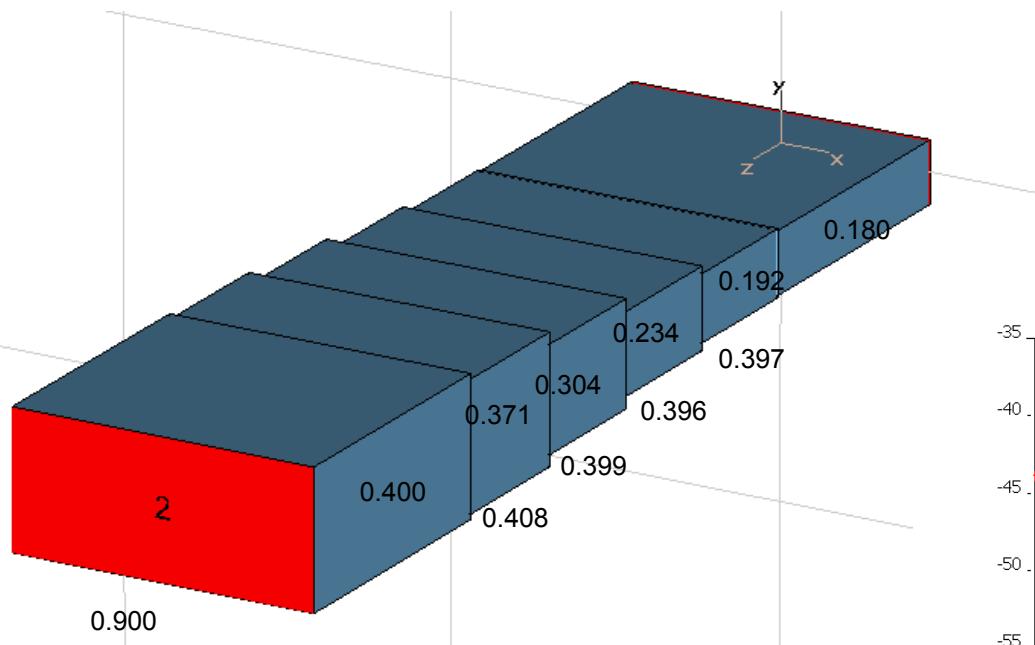
$S_{11} \leq -21.55$

# Waveguide Transformer & H-plane Bends in the side arm

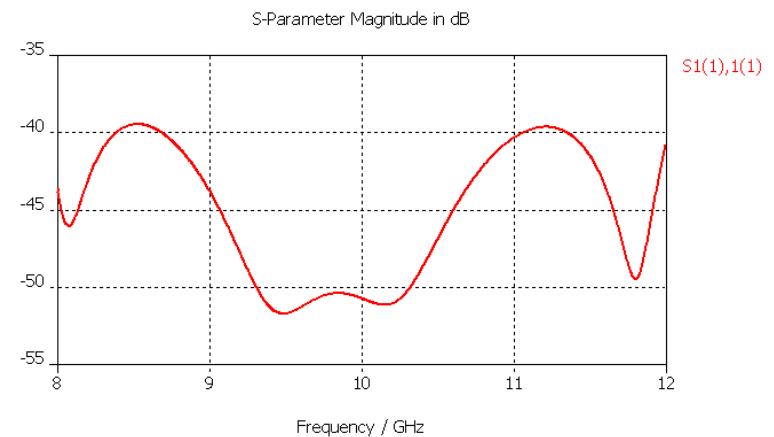


Waveguide Transformer  
0.900 x 0.400  
to  
0.900 x 0.180

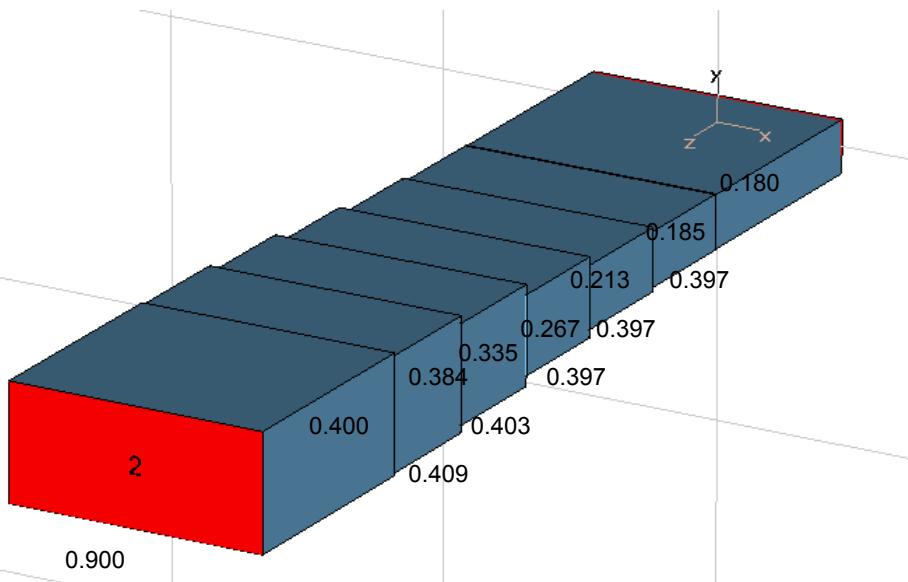
# 4-step Tchebyschev Transformer



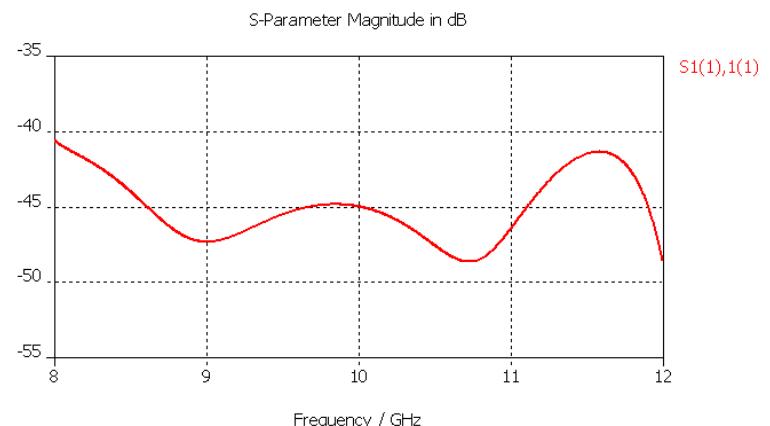
$$\lambda_g = 1.6133''; \lambda_g / 4 = 0.4033$$



# 5-step Tchebyschev Transformer\*



$$\lambda_g = 1.6133"; \lambda_g / 4 = 0.4033$$



\*Used this design

# H-plane bend

$$|\rho| = \frac{\lambda_g^2}{32\pi^2 R^2} \left[ \sin \frac{2\pi l}{\lambda_g} - \frac{128}{\pi^2} \frac{a}{\lambda_g} B \cos \frac{2\pi l}{\lambda_g} \right]^{**} \quad (1)$$

where

$$B = \sum_{2,4}^{\infty} m^2 (m^2 - 1)^{-3} \left[ (m^2 - 1) - \left( \frac{2a}{\lambda_g} \right)^2 \right]^{-0.5} \quad (2)$$

For a given  $|\rho|$  and  $\lambda g$ ,  $l$  is given by

$$\tan \frac{2\pi l}{\lambda_g} = \frac{128}{\pi^2} \frac{a}{\lambda_g} B \quad (3)$$

$a=0.900$  and  $\lambda g=1.6133$

$l=0.105\lambda_g$  or  $l=[0.105+(n/2)]\lambda_g$   
For  $n=3$ ,  $l=2.589$ ;  $R=1.648$

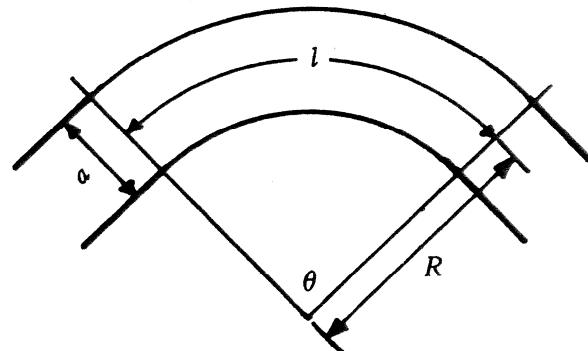
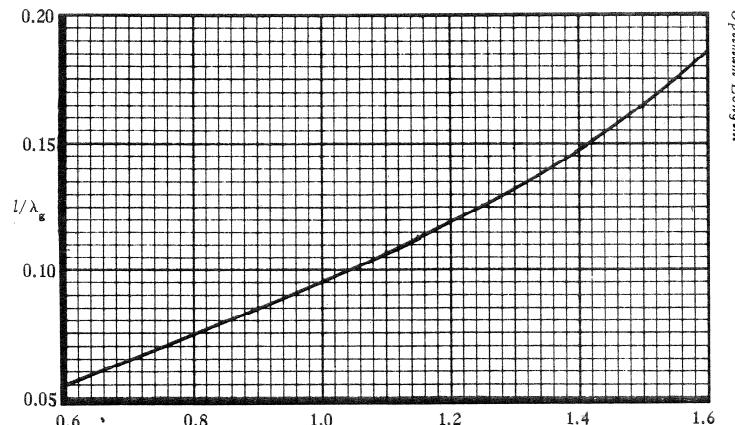
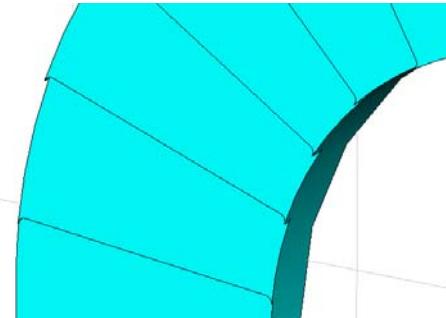
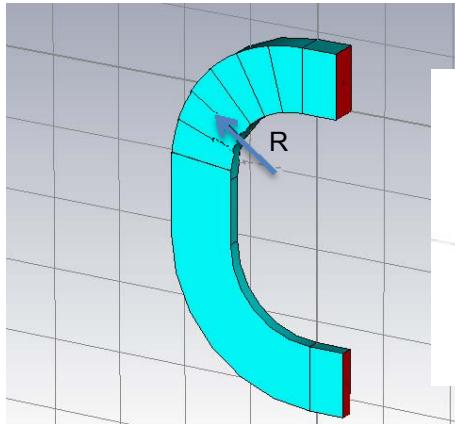


FIG. 10. -- CONSTANT RADIUS H-PLANE BEND.

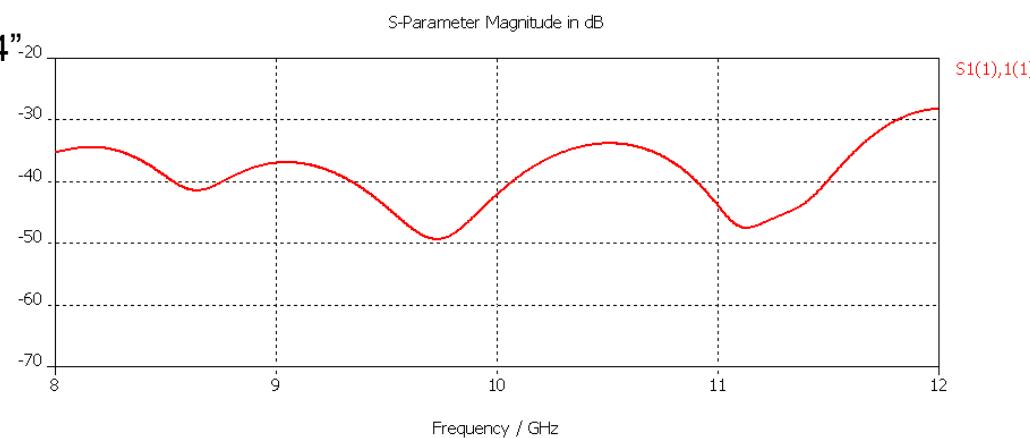


\*\* F.C. de Ronde, "Full Band Matching of Waveguide Discontinuities", IMS, Palo Alto, CA 1966

# H-plane bend with stepped transformer

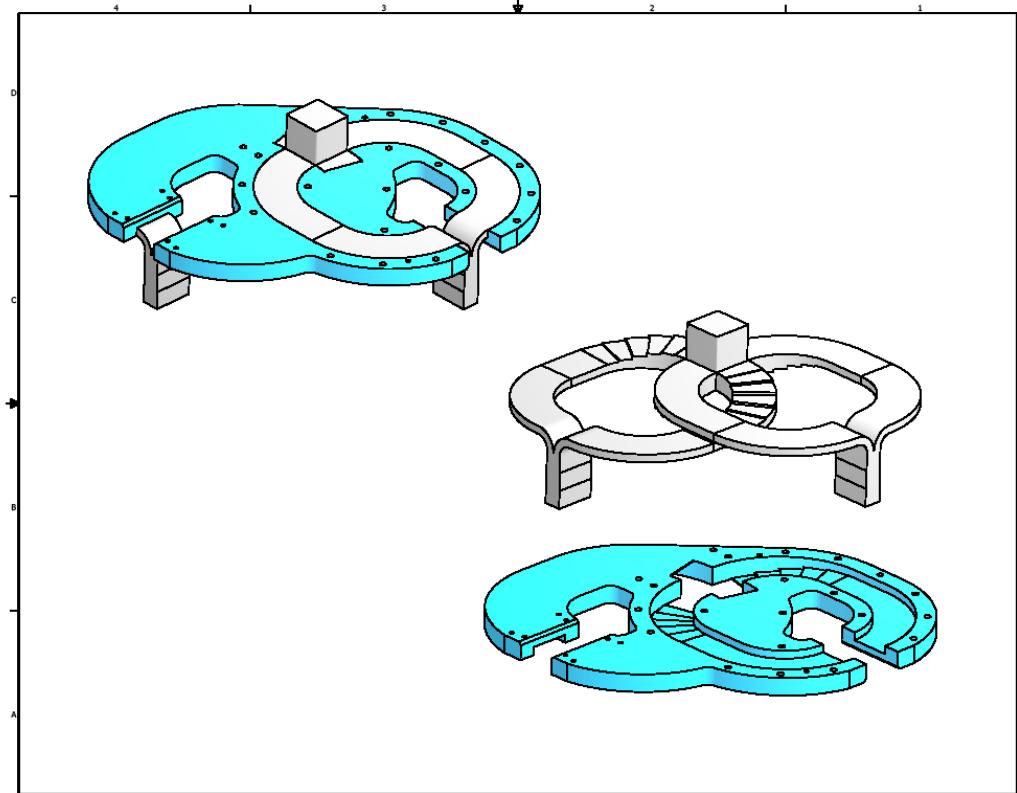


$$R \times \pi/2 = l$$
$$l = 1.605 \lambda_g ; R=1.6484"$$



Cutting tool  
Radius=0.0235  
Length=0.470

# E-plane Y-Junction



Y-junction

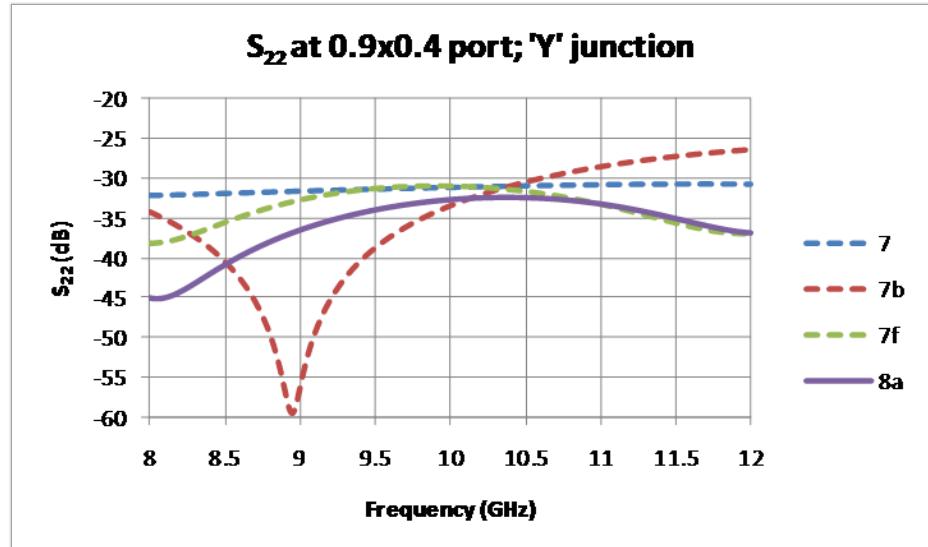
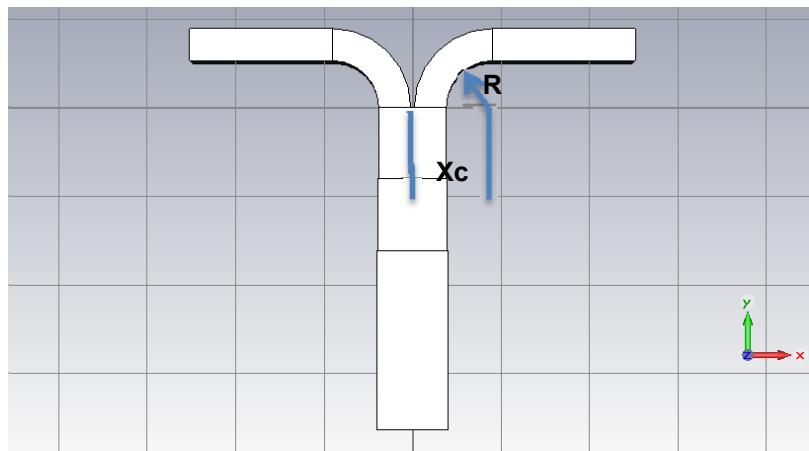
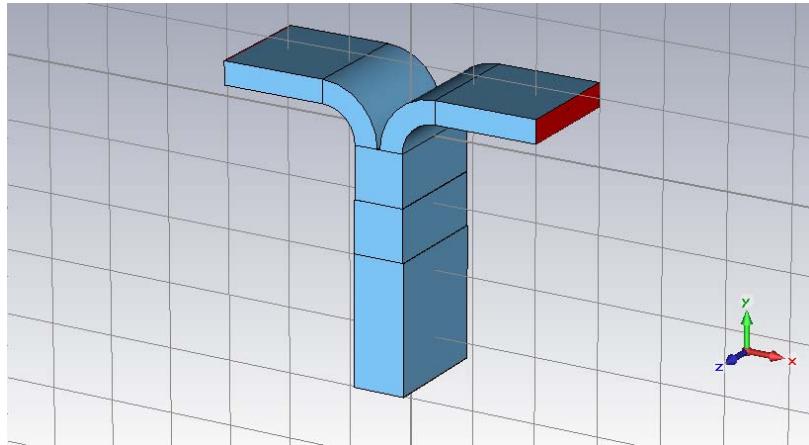
Input: 0.900x0.180

Output: 0.900x0.380

0.900x0.390

0.900x0.400

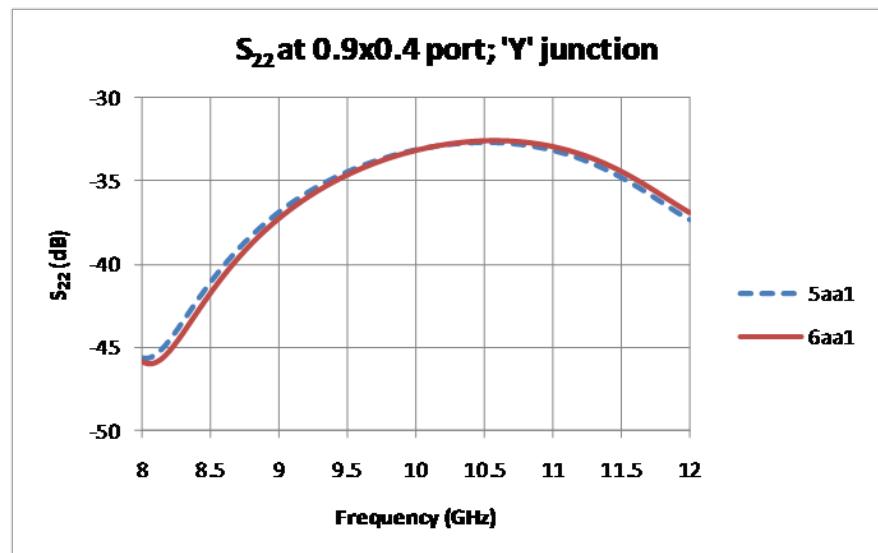
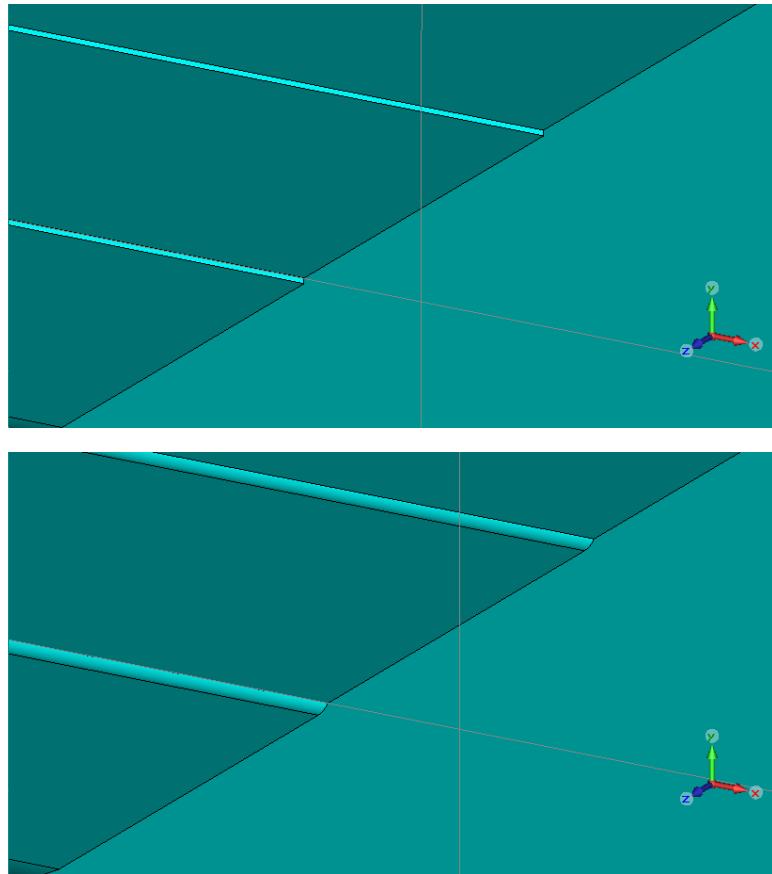
# E-plane Y-junction



	R	Xc
7	0.450	0.640
7b	0.450	0.640
7f	0.450	0.640
8a	0.260	0.450

$S_{11} \leq -32.6$

# E-plane Y-junction

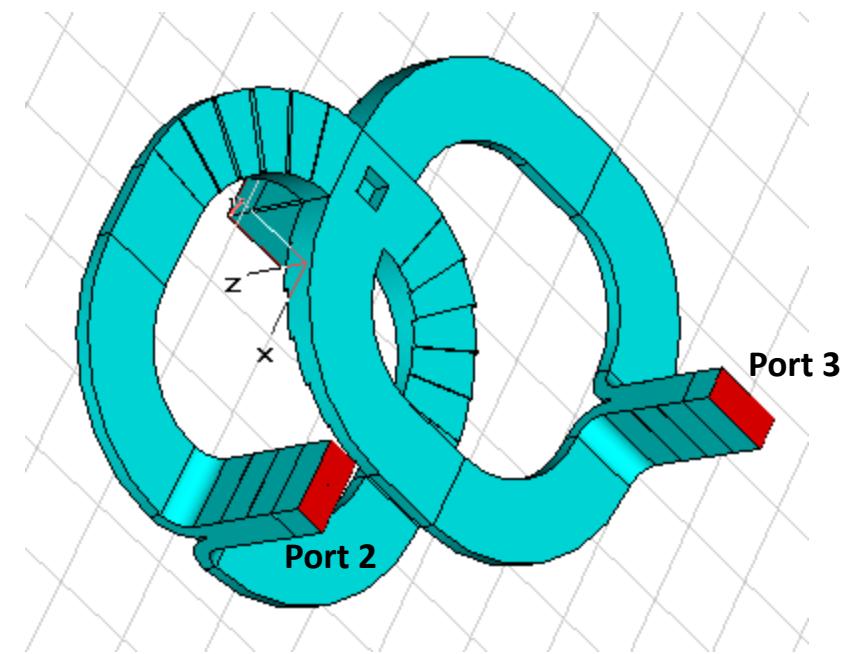
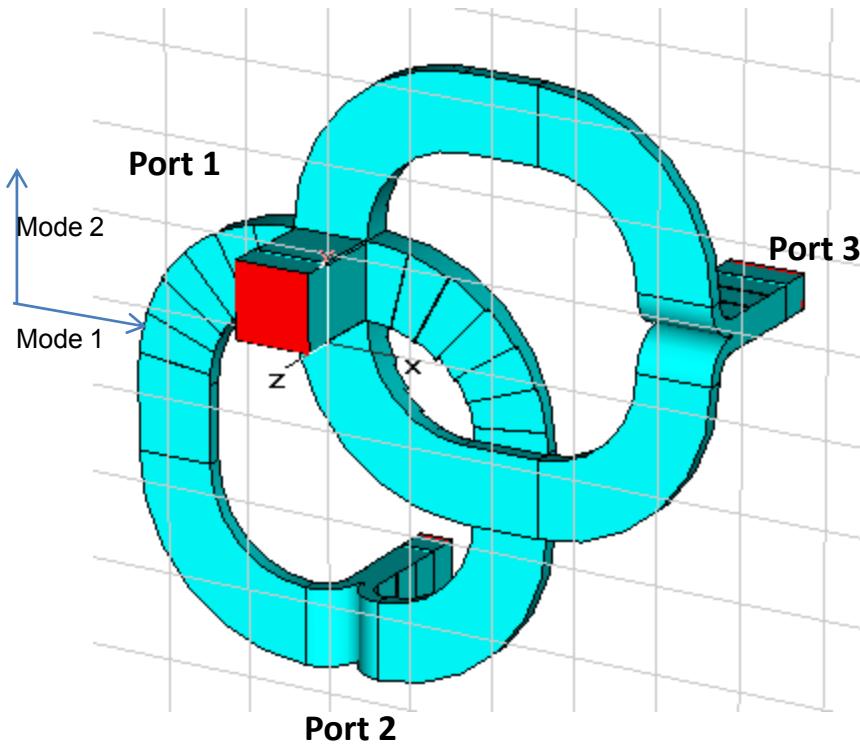


5aa1: No radius on steps

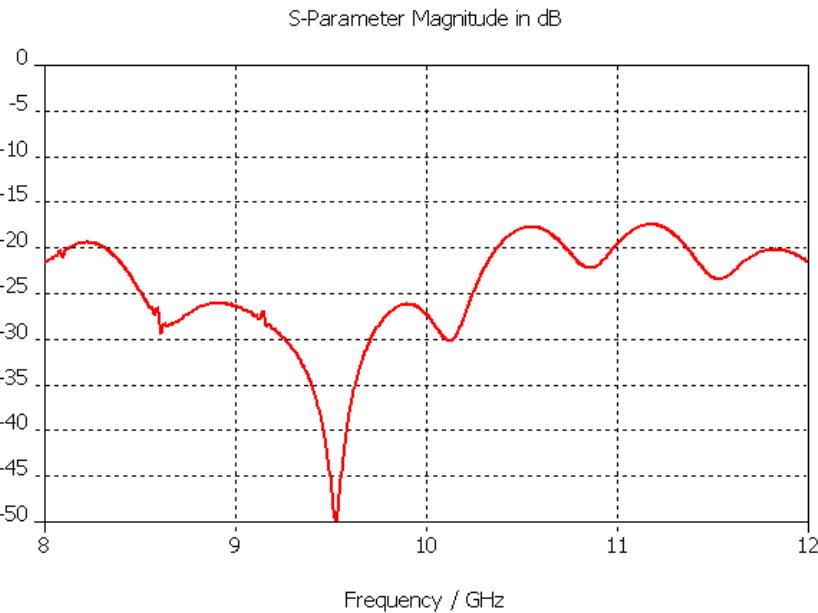
6aa1: 0.0235 radius

$S_{11} \leq -32.6$

# CST Microwave Studio Model

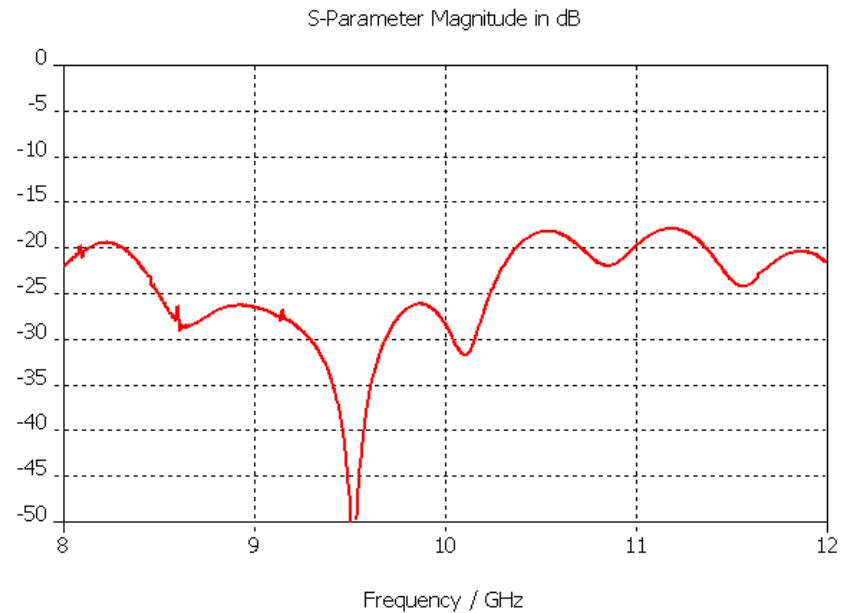


# Input Return Loss



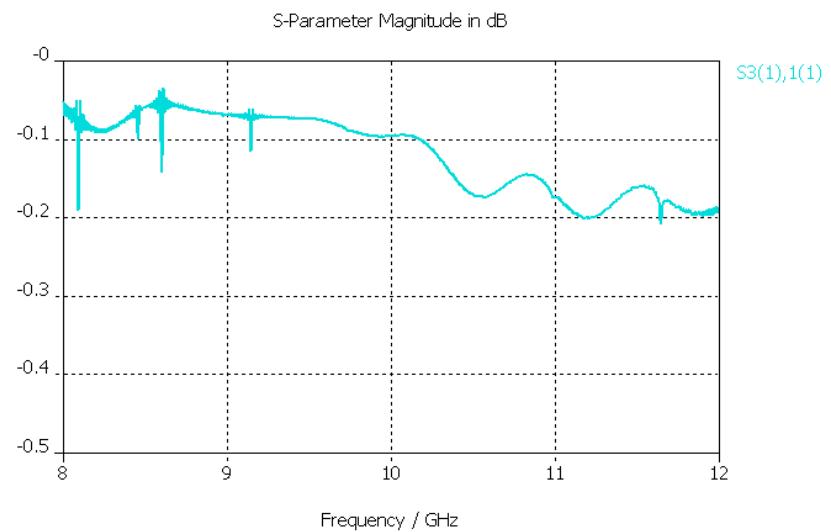
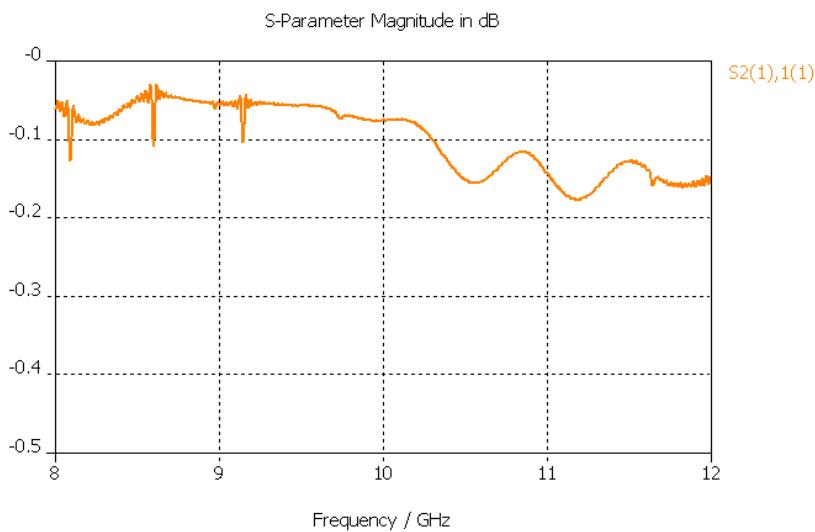
$S1(1),1(1)$

$S_{11} < -17.4 \text{ dB}$

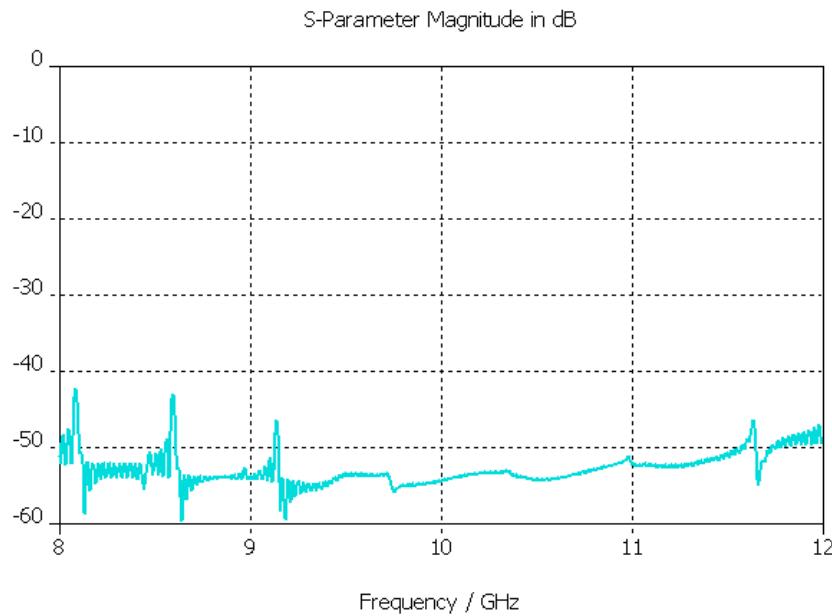


$S1(2),1(2)$

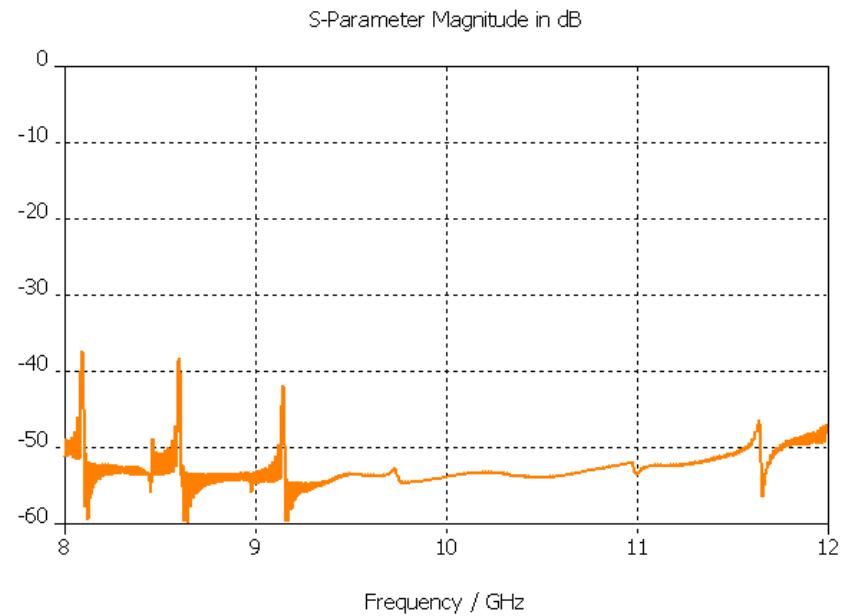
# Insertion Loss



# Crosspolarization

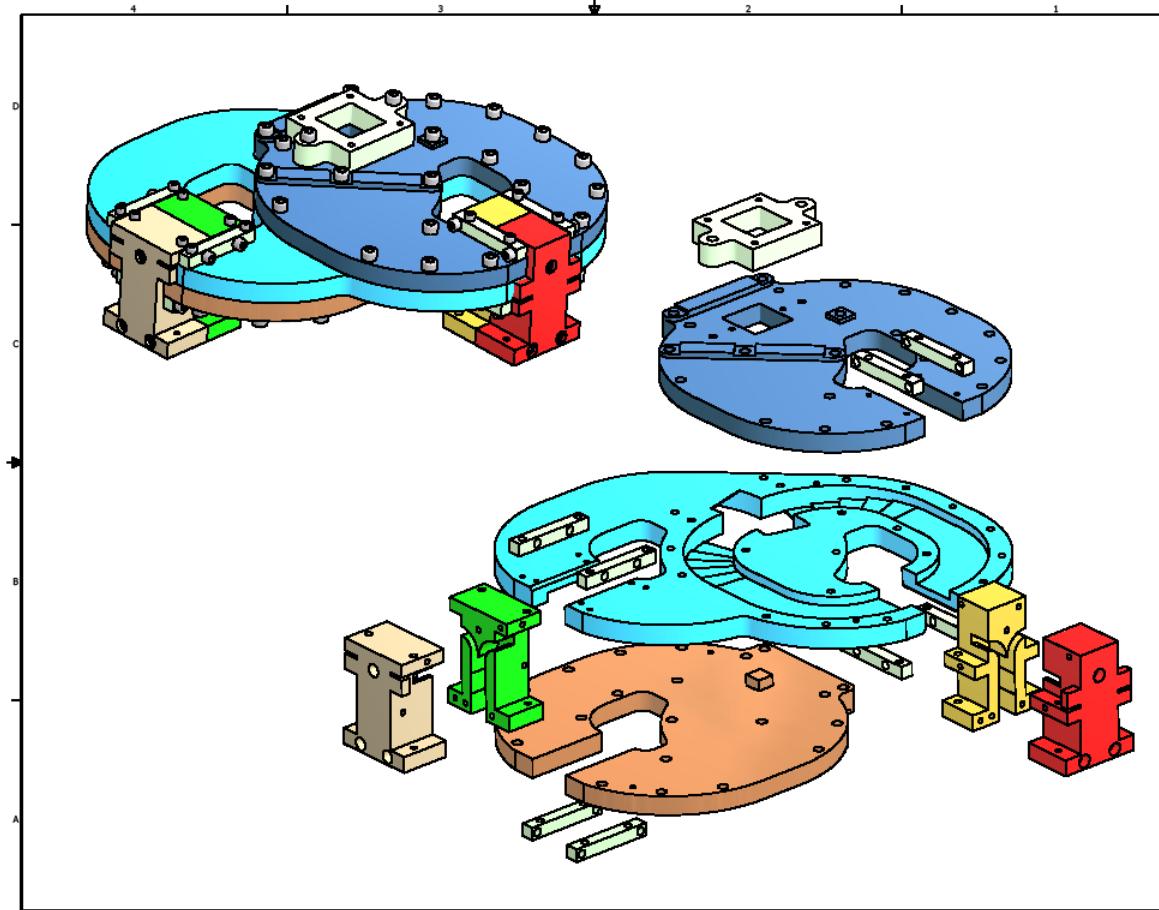


$S3(1),1(1)$



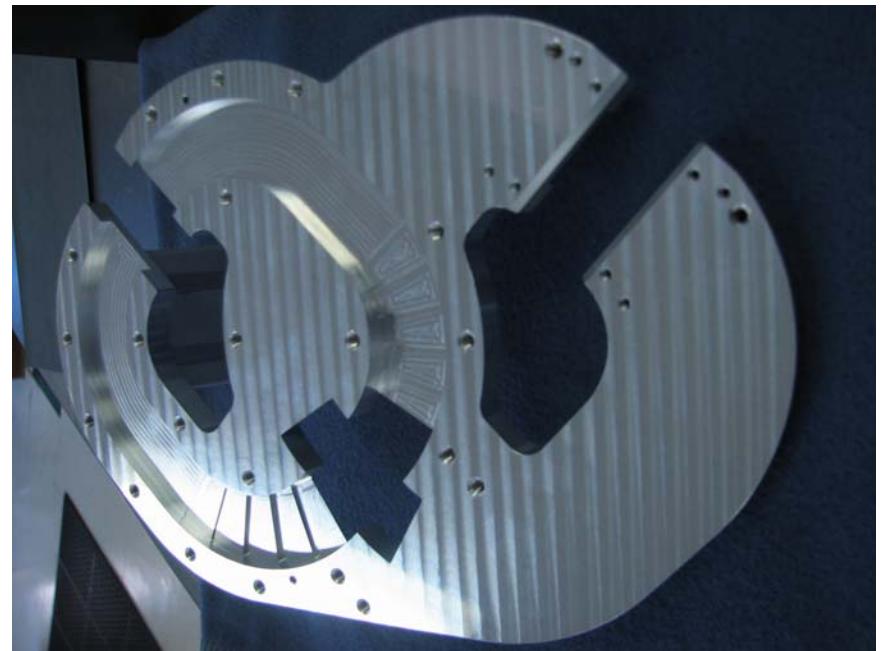
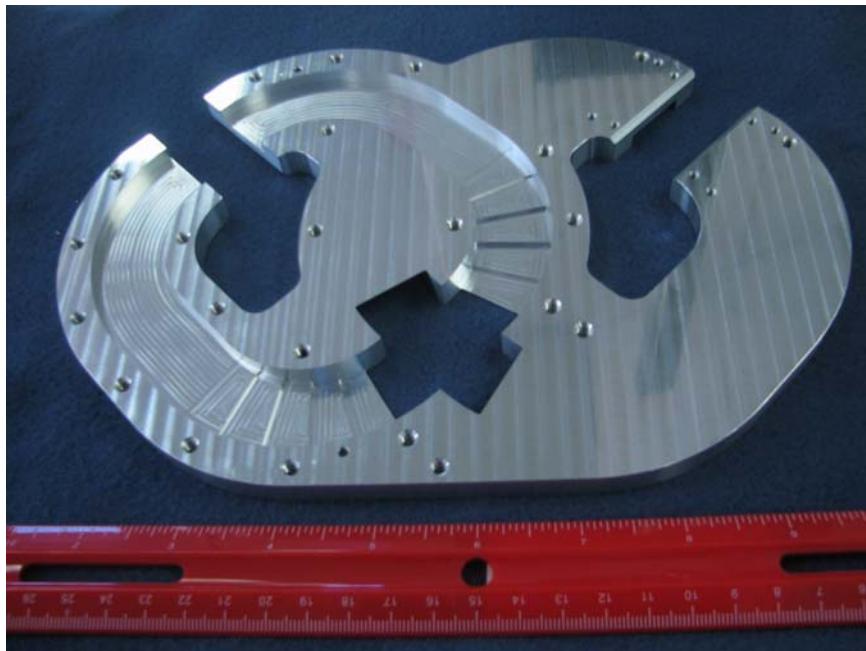
$S2(1),1(2)$

# Mechanical Design



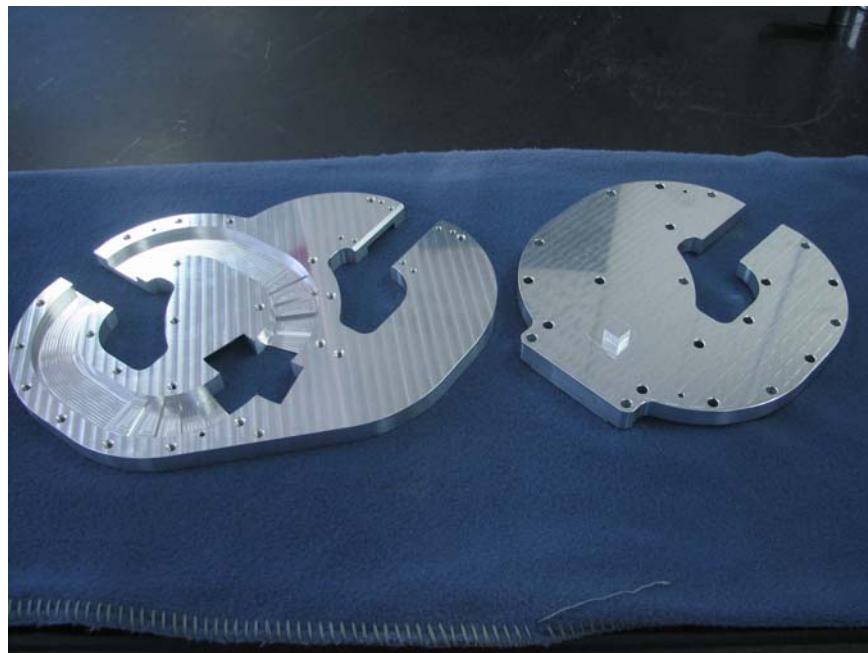
Cross-section 9.25"; Height 2.68"; Measured weight : 4.4 lbs

## Center plate with curved stepped transitions

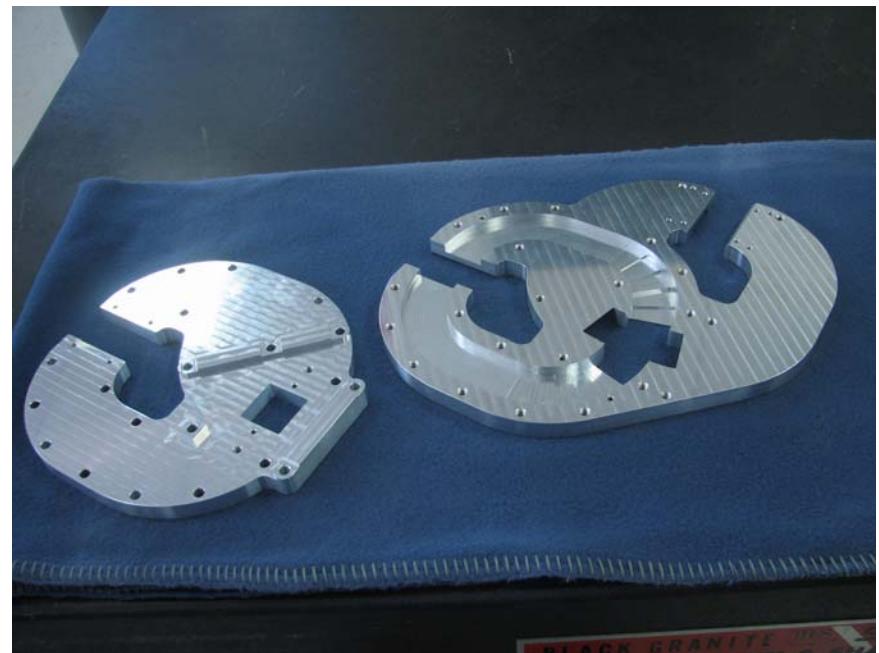


Side arms with bends and stepped transformer

# Bottom and top plates



Bottom plate with square tuning stub

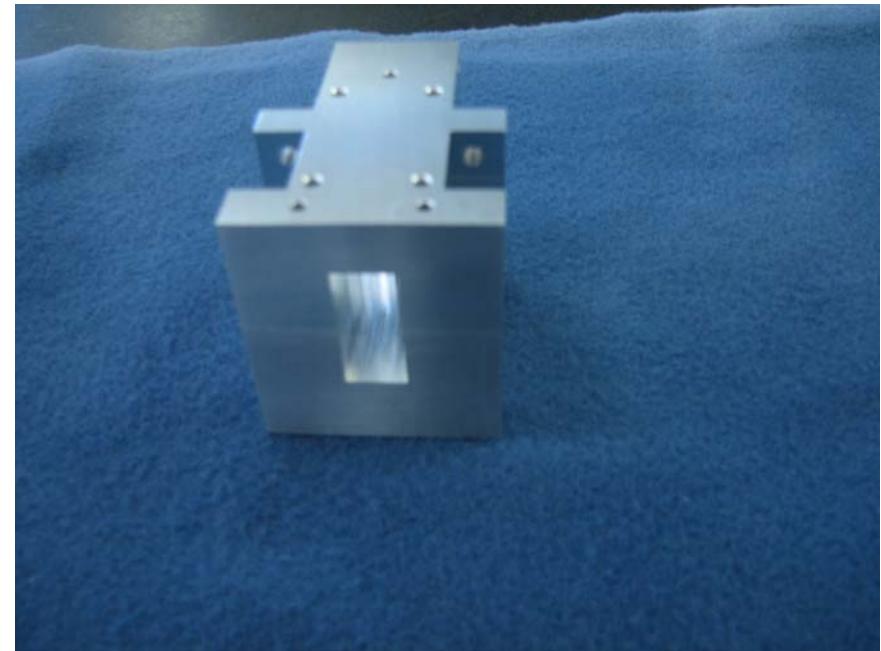


Top plate with input waveguide

# E-plane Y-Junction



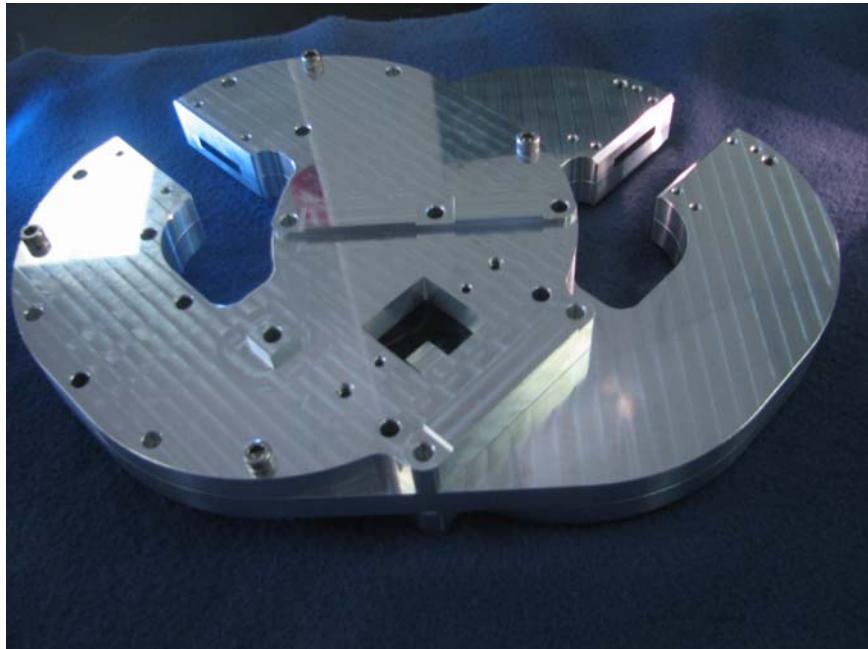
E-plane split block



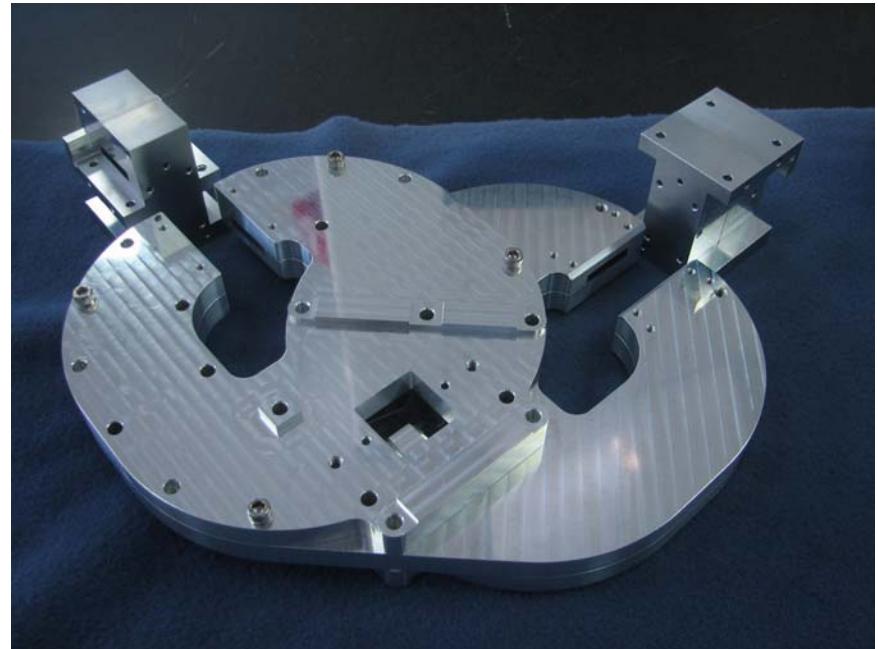
Assembled Y-Junction

Input 0.900x0.180; Output at junction 0.900x0.380  
Inner radius 0.260; Outer radius 0.440; Center 0.450

# Assembly

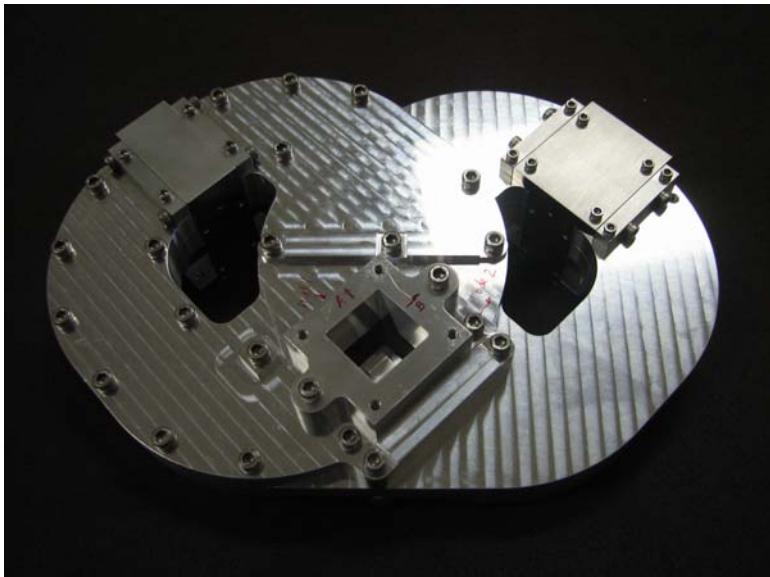


Main body assembled

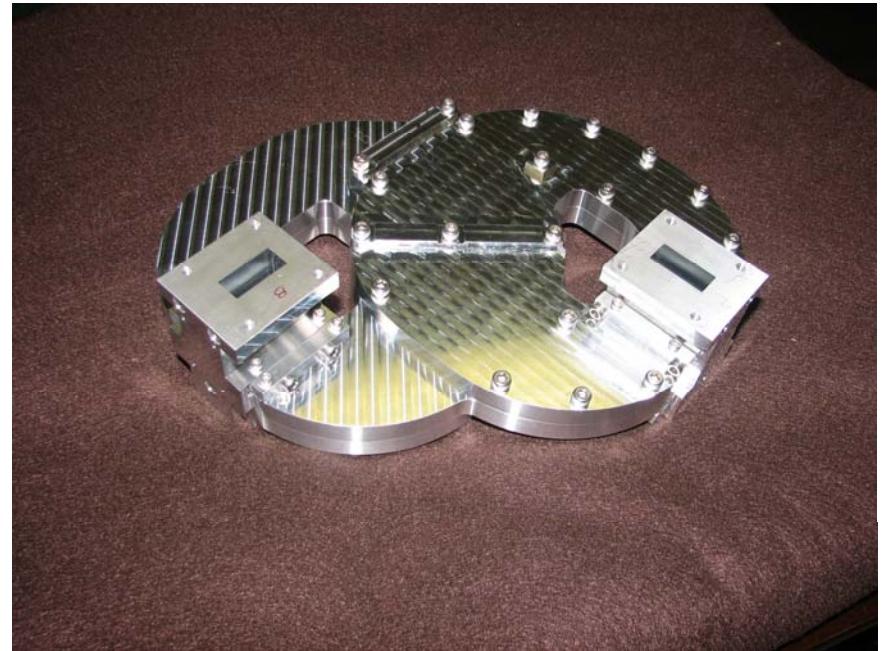
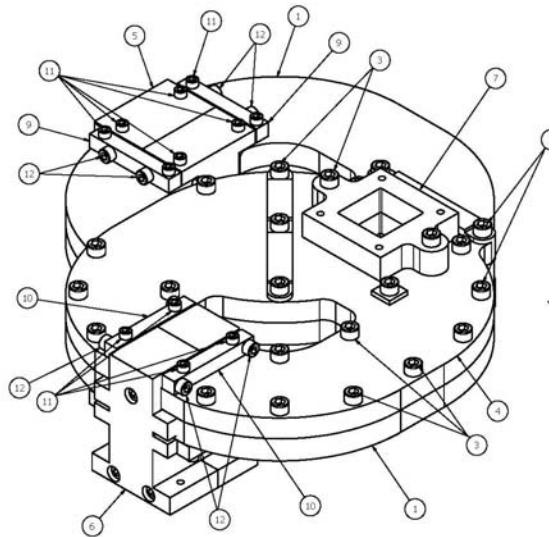


Main body, output ports

# Assembled OMT



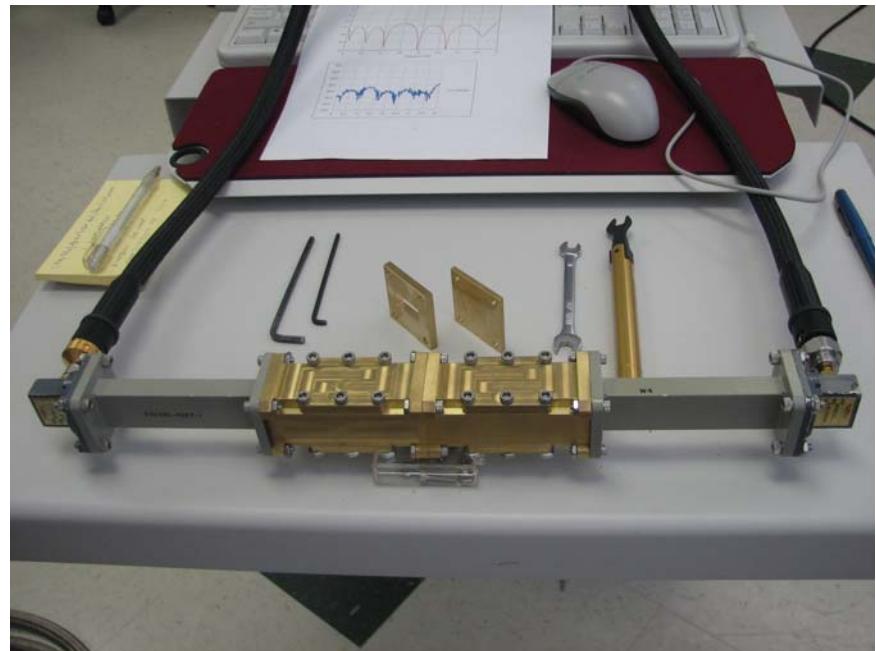
Square port



Rectangular ports

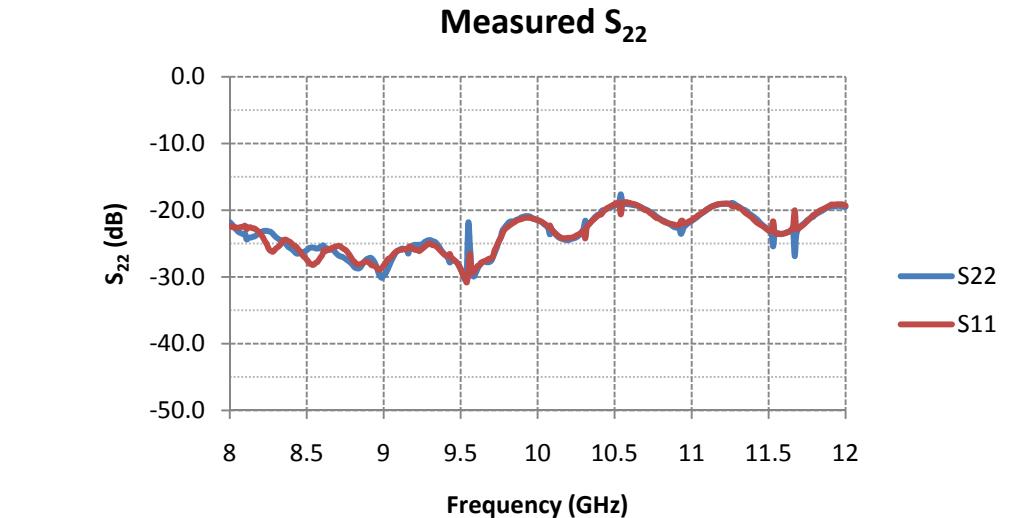
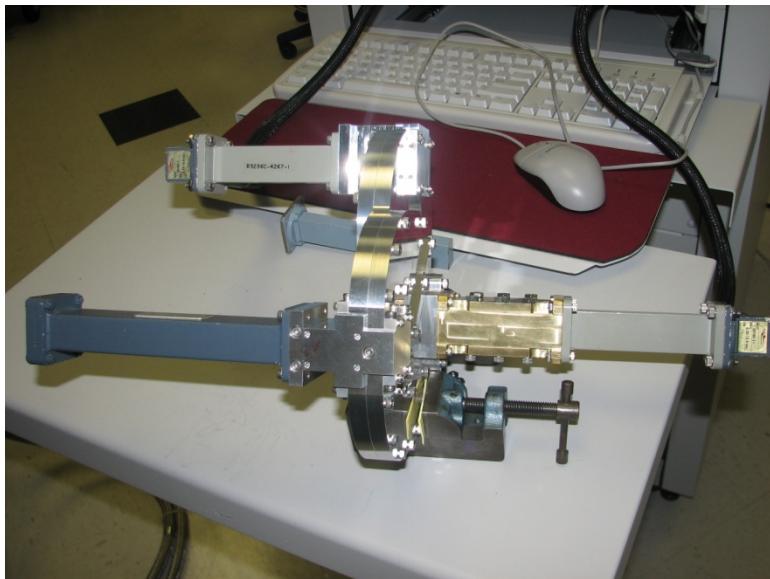
# Measurement

EVLA

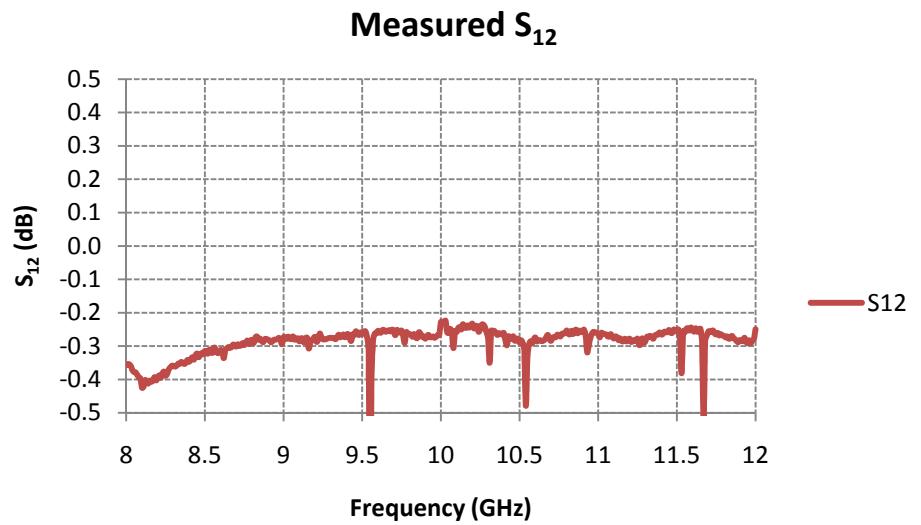


Measurements with Agilent N5245A PNA-X

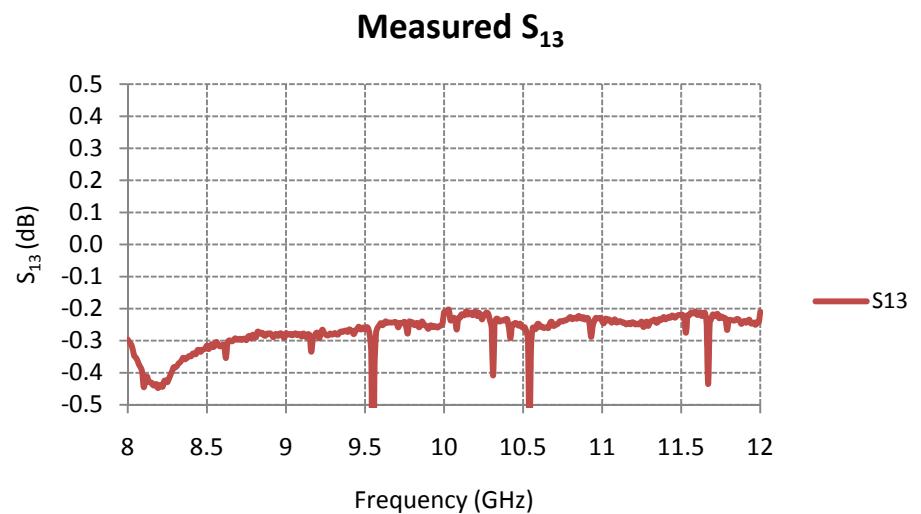
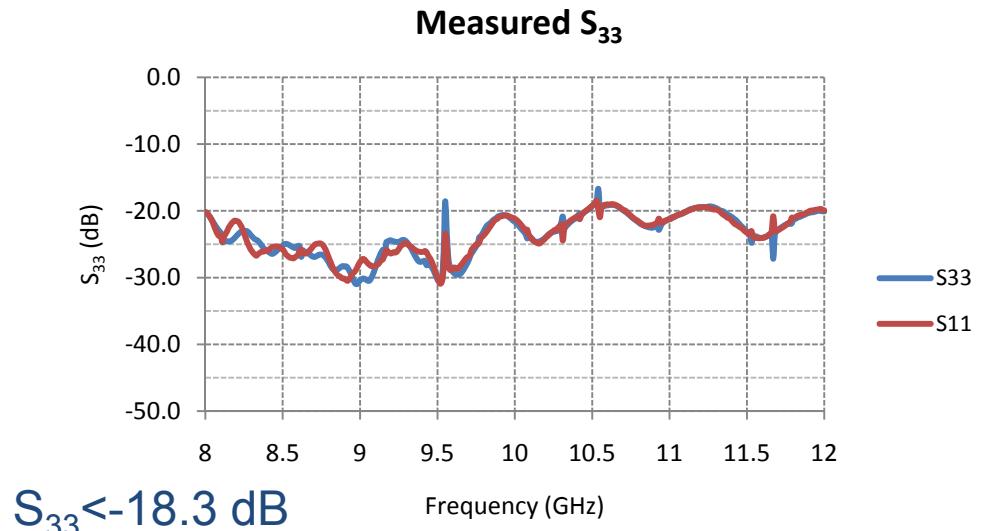
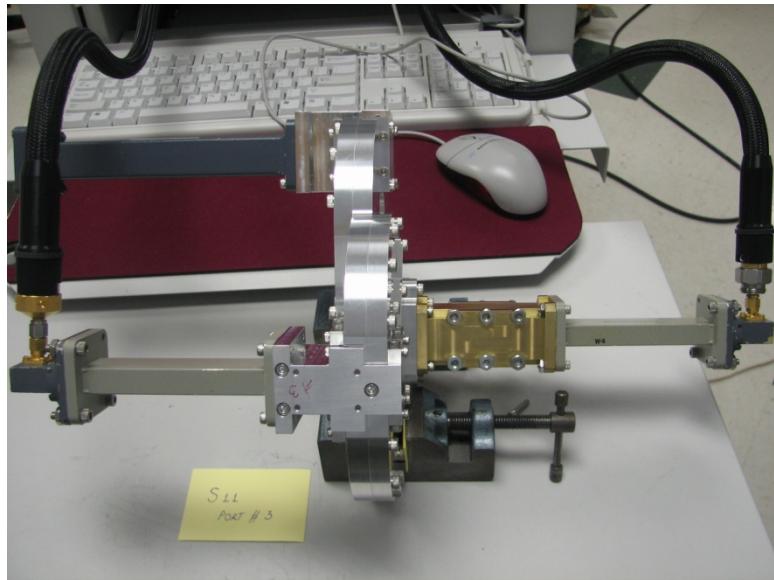
# $S_{22}$ and $S_{12}$ -Port 2



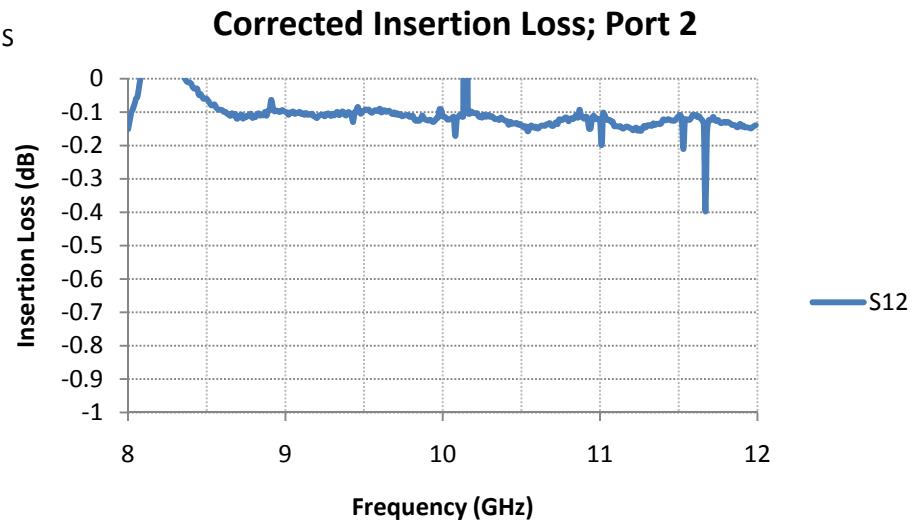
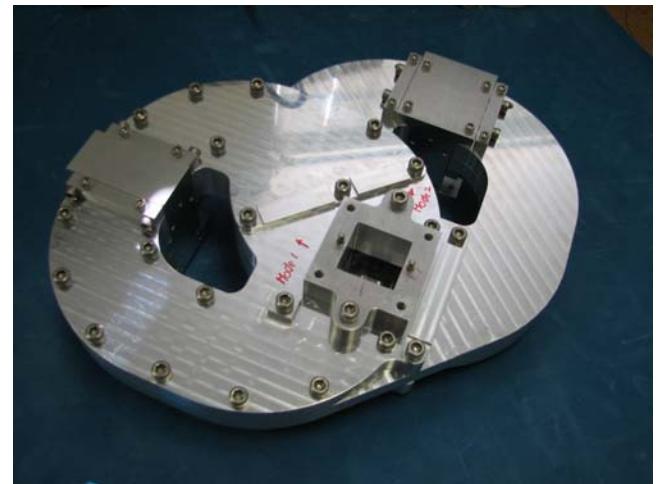
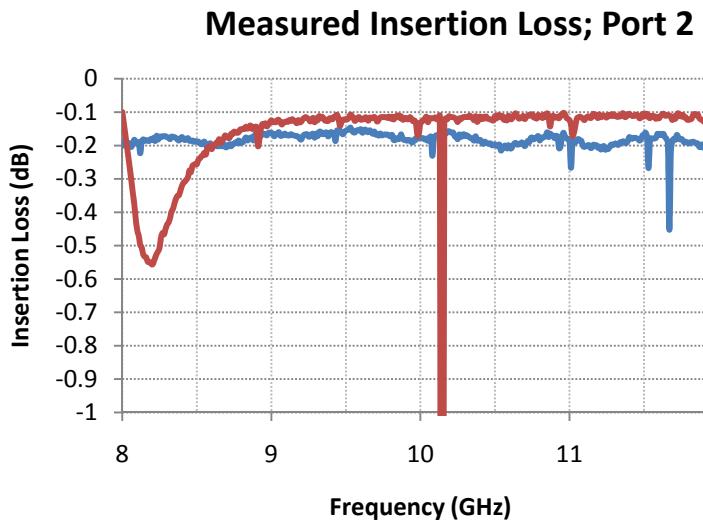
$S_{22} < -18.7 \text{ dB}$



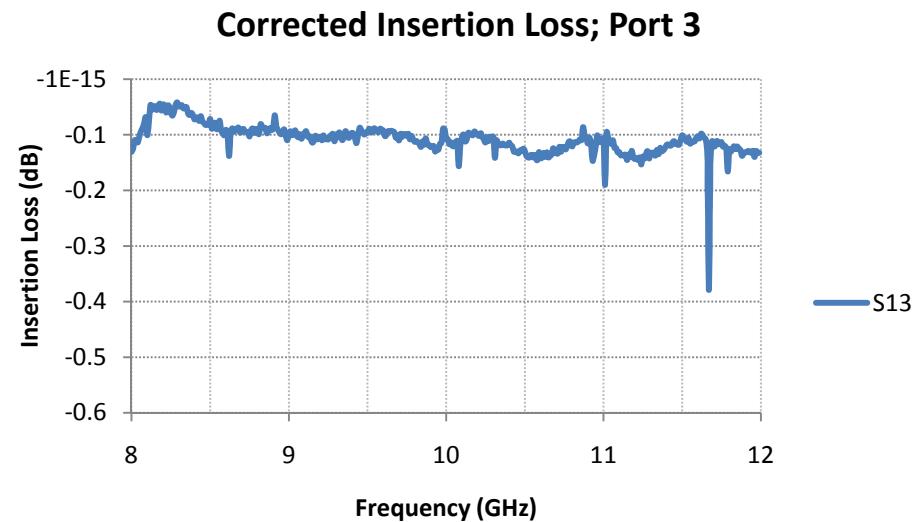
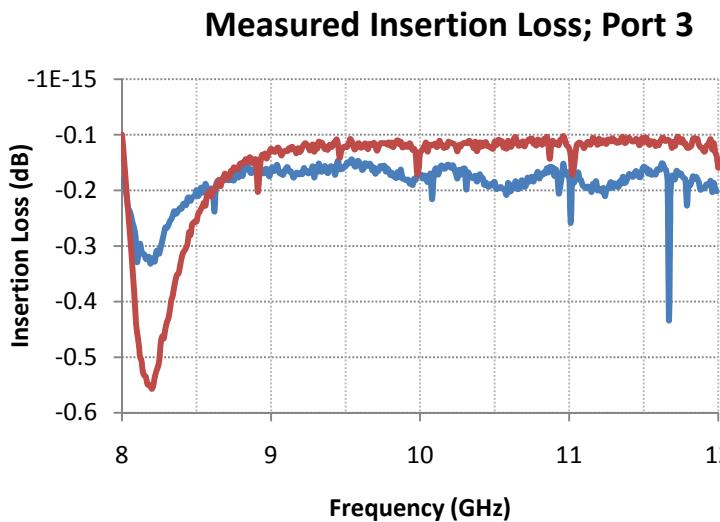
# $S_{33}$ and $S_{13}$ -Port 3



# Measurement of $S_{12}$ after pinning

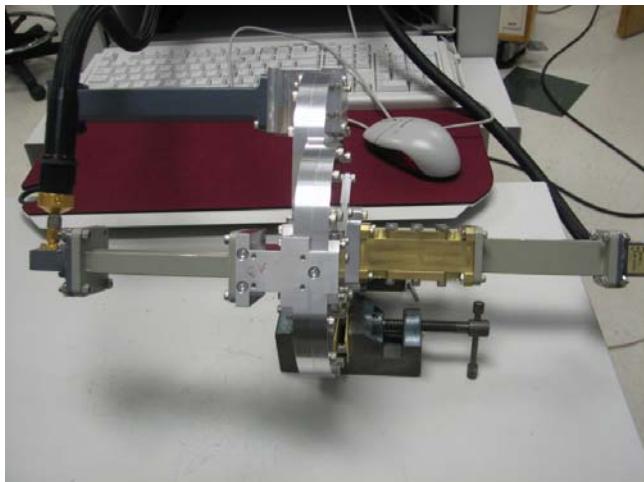
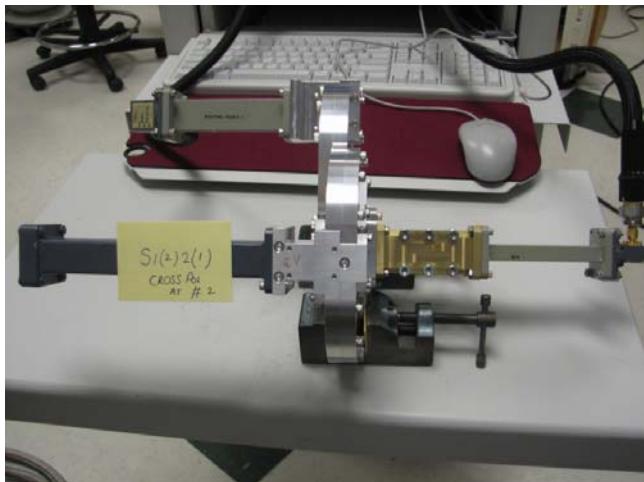


# Measurement of $S_{13}$ after pinning

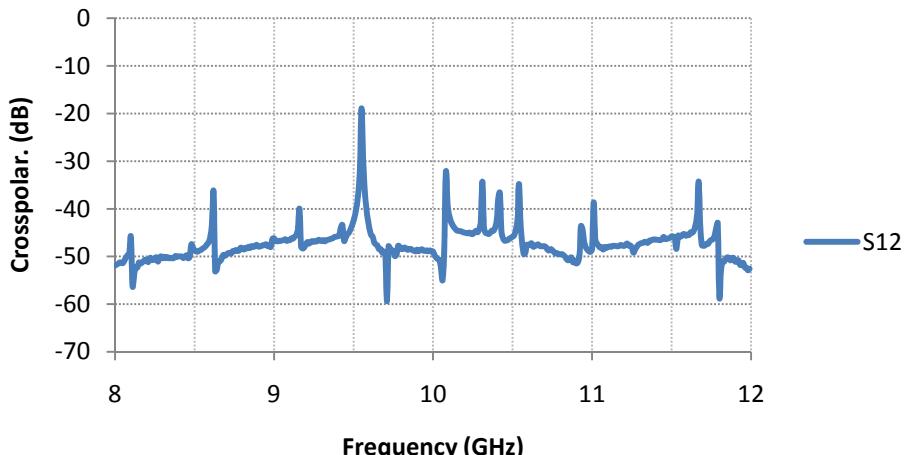


# Crosspolarization

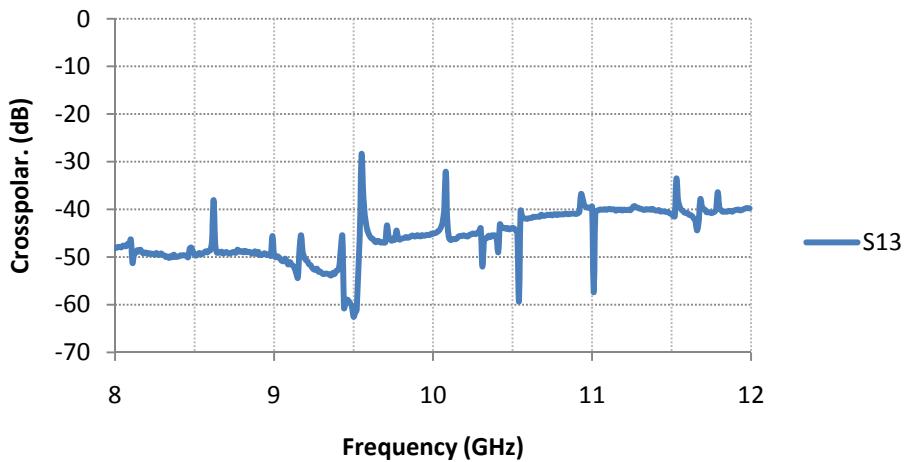
EVLA



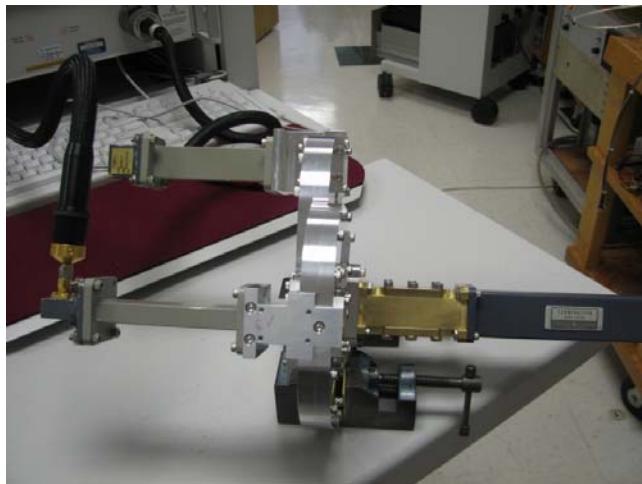
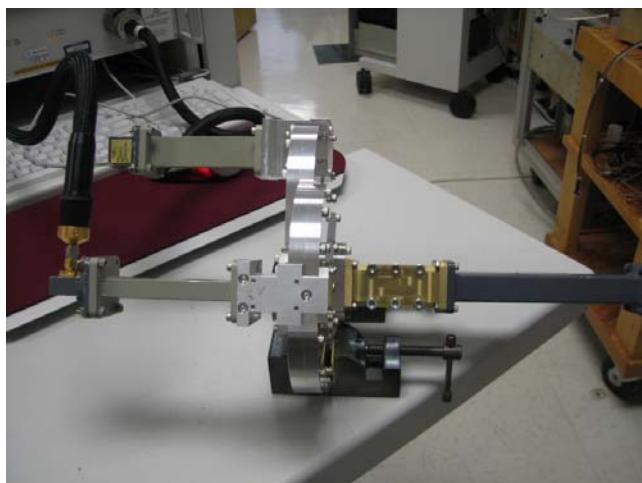
Measured Crosspolarization; Port 2



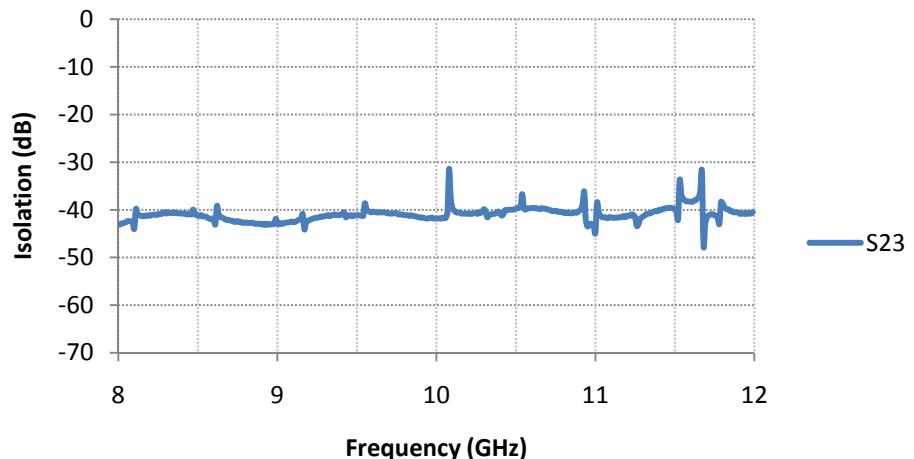
Measured Crosspolarization; Port 3



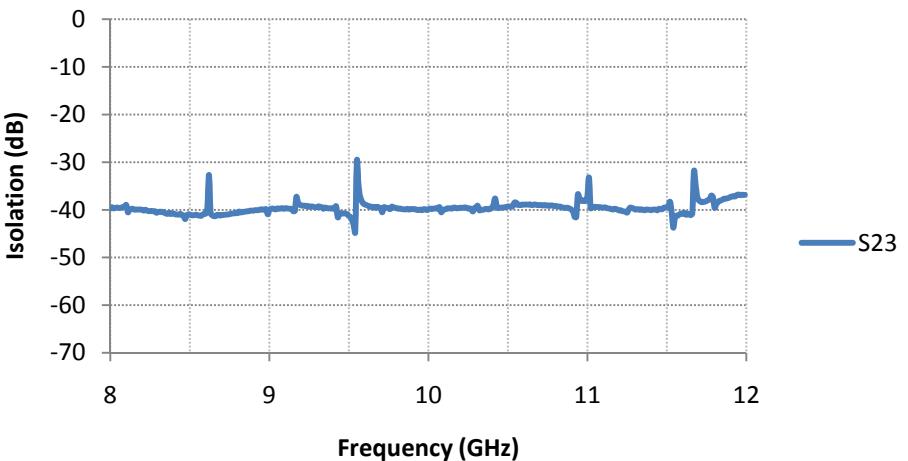
# Isolation between ports



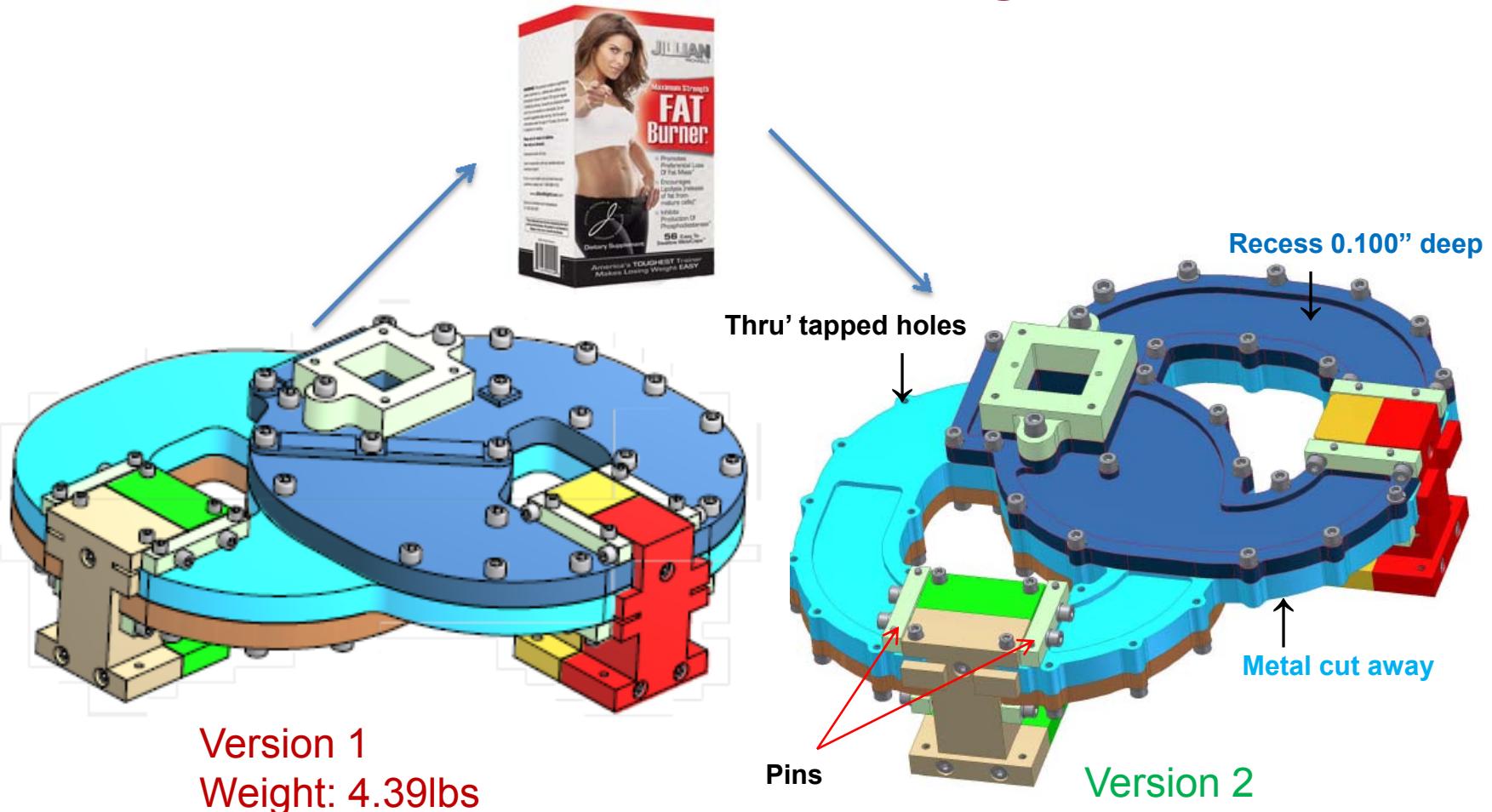
Measured Isolation; Port 2



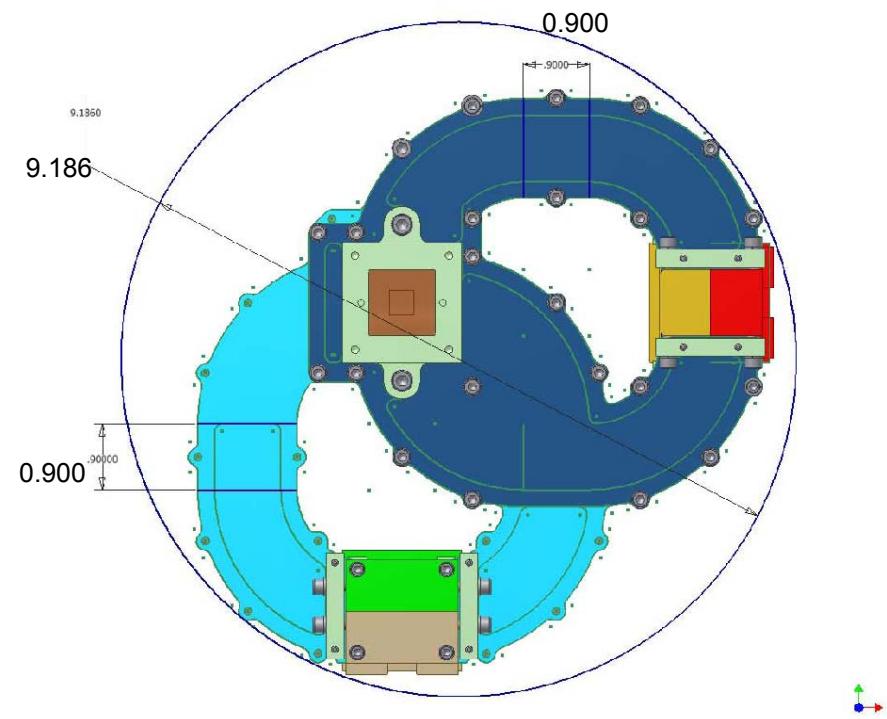
Measured Isolation; Port 3



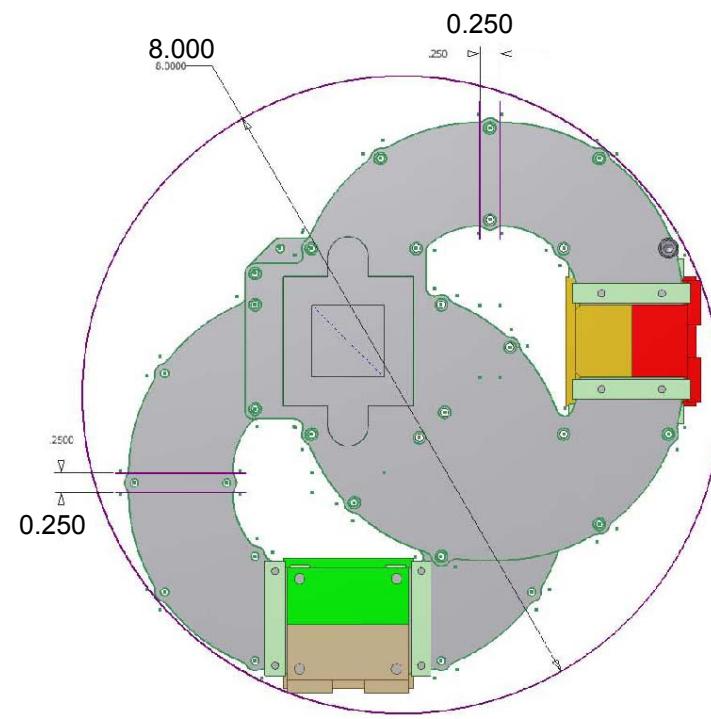
# Jillian Michaels Weight Loss Program



# More compact design

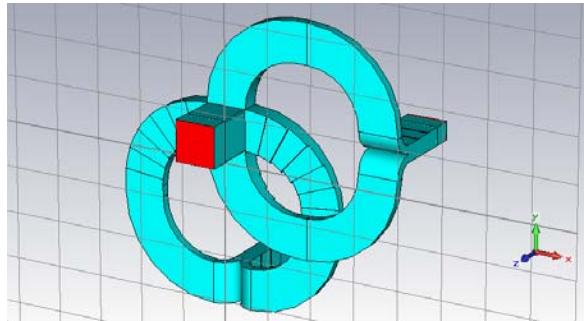


Version 2: 2.55 lbs

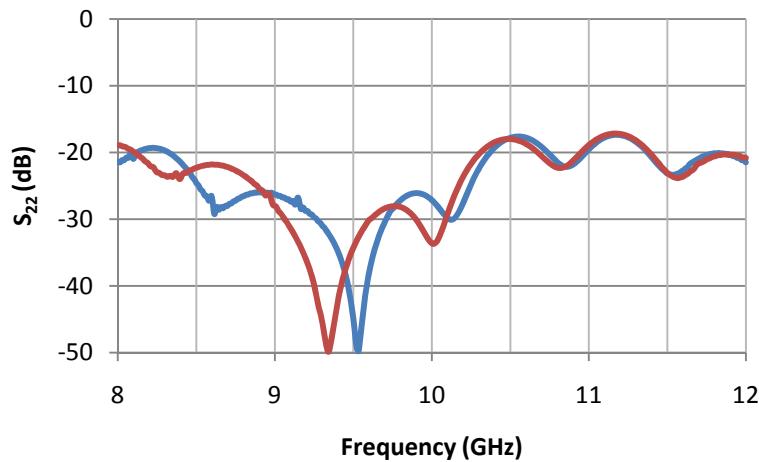


Version 3: 2.2 lbs

# Performance of 9.25" & 8.0" OMTs (CST)

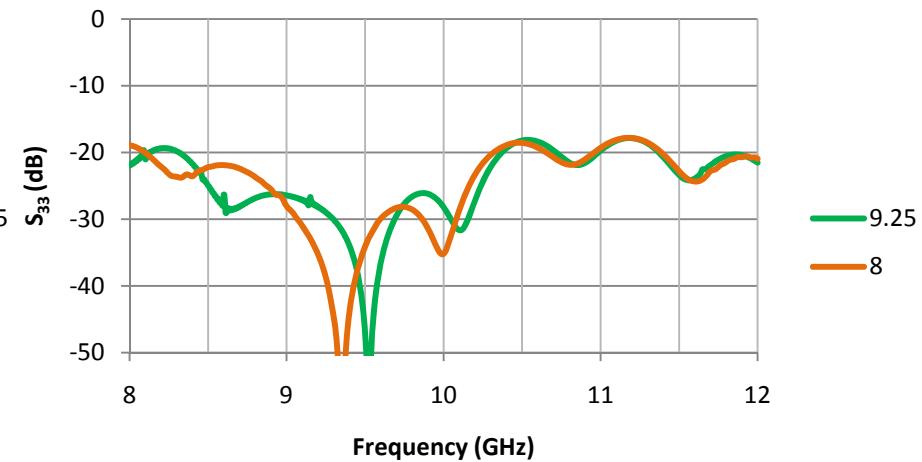


$S_{22}$ ; Port 2; Horz. pol.



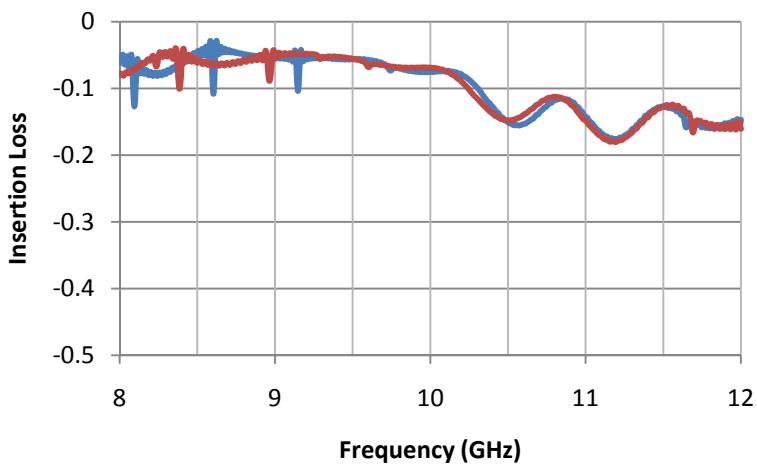
-17.4; -17.2dB

$S_{33}$ ; Port 3; Vert. pol.

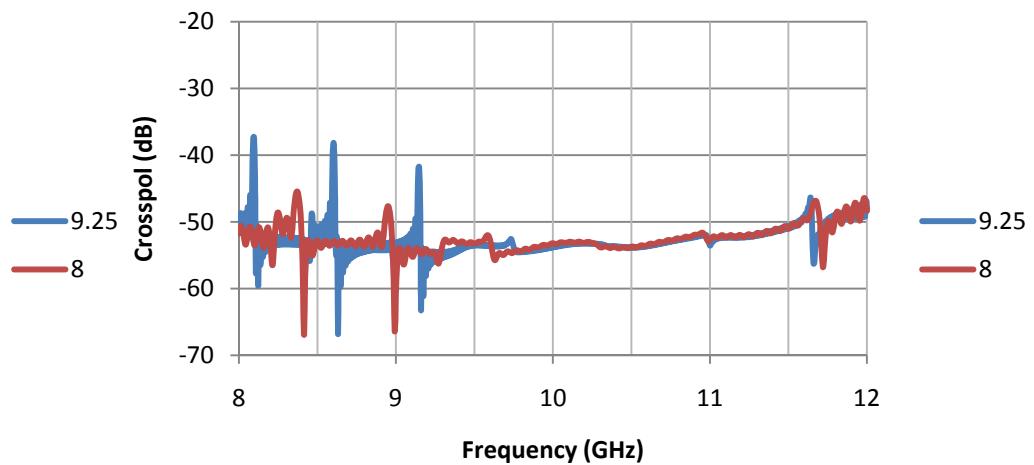


# Performance of 9.25" & 8.0" OMTs (CST)

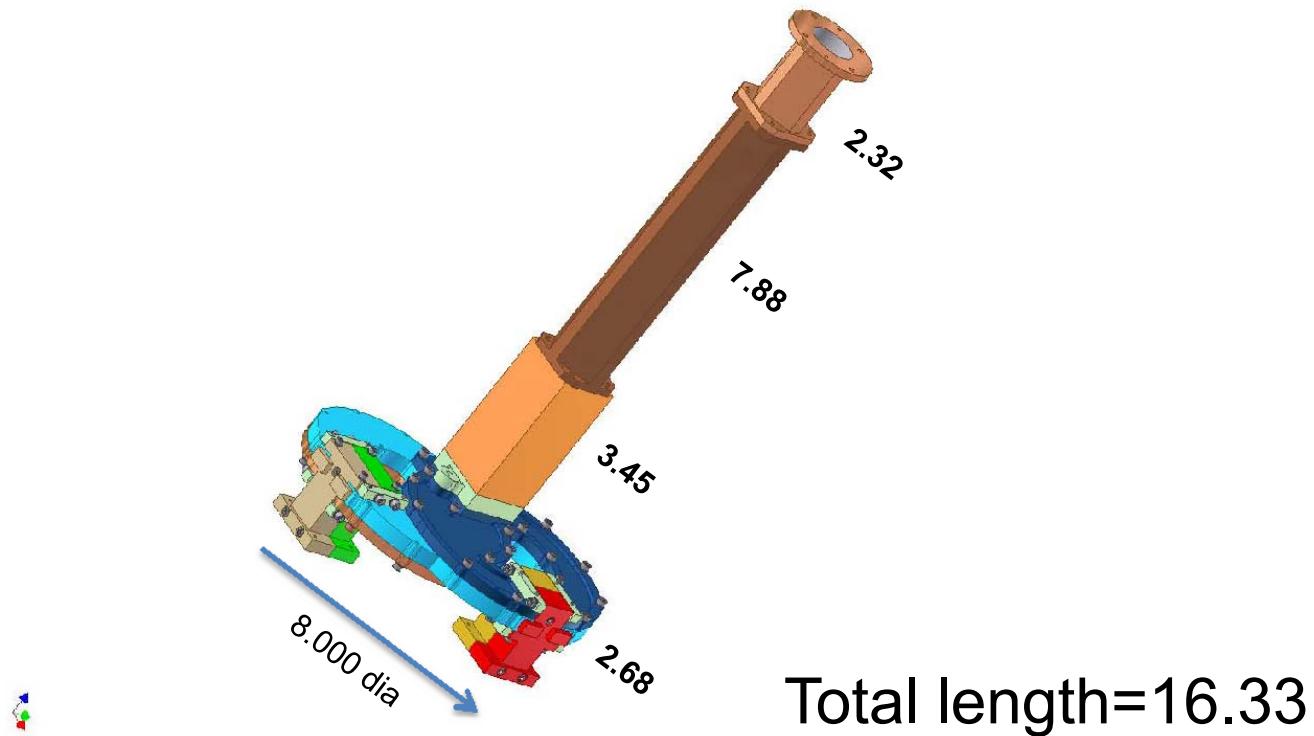
Insertion Loss; Port 2; Horz. pol.



Crosspol at Port 2; Horz. pol.



# Layout of Polarizer components



Total length=16.33

# Conclusions

1. Full waveguide band (8-12 GHz) OMT has been realized
2. Returns loss > 18.3 dB; Insertion loss ~0.1dB;  
Crosspolarization ≤ -50 dB; Port to port isolation ~ -40 dB
3. Compact: Height 2.68"; Cross-section 9.25";Weight 4.4lbs  
**Version 3:Height 2.68", Cross-section 8.00";Weight 2.2 lbs**
4. Fabrication easy; only machined parts
5. No pins, no septum; Sturdy construction (can withstand several 'G' acceleration)
6. Two fold symmetry; only symmetric higher order modes if any and will cancel at output ports
7. Coupling into amplifier in waveguide transmission line

## Conclusions (continued)

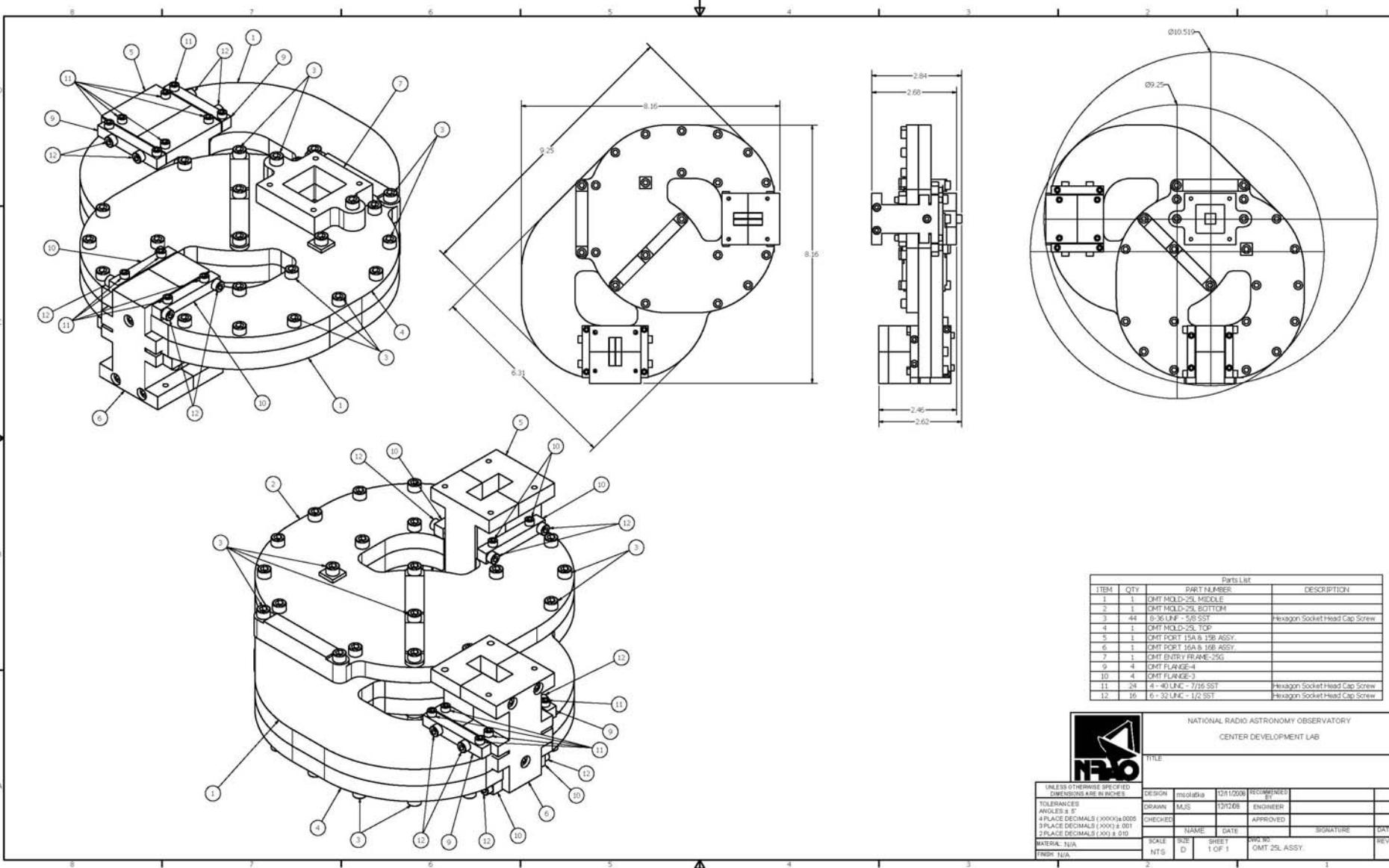
8. Waveguide isolator has ~0.2 dB lower loss compared to coax isolator
9. Turnstile OMT ~0.1 dB lower loss compared to Quadridged OMT (due to coax connector)
10. Loss due to 8 & 9 will contribute to 1.1K lower  $T_{rx}$  at 15K physical temperature; ~5% of  $T_{rx}$  at X-band (3.6% of  $T_{sys}$ )
11. Poor  $S_{11}$  with coax connector may contribute to base line ripple.
12. Limiting factor with subject OMT is the turnstile junction.
13. Cost of OMT \$861/piece for a lot size of 30 (J&E Precision Tool Inc., Southampton, MA)

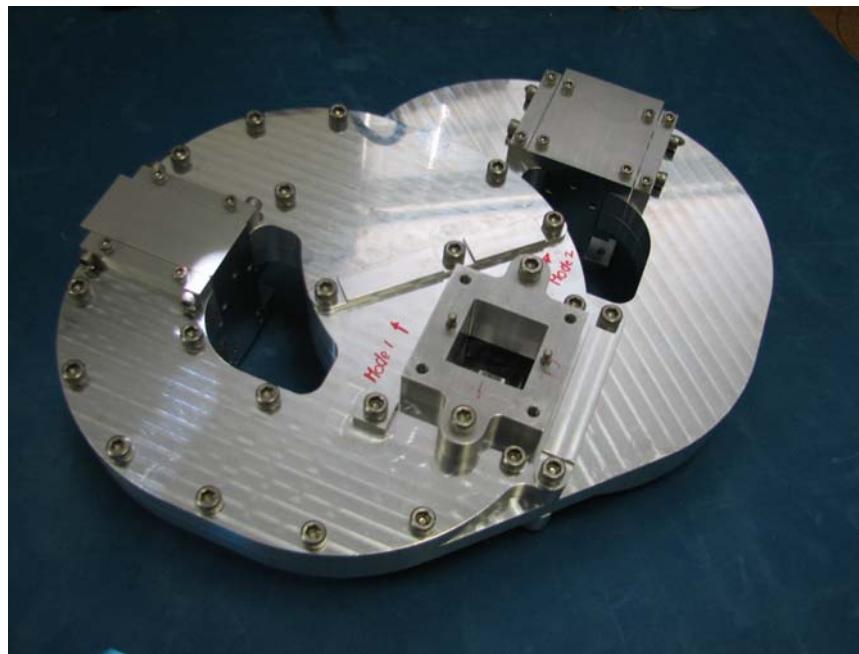
EVLA

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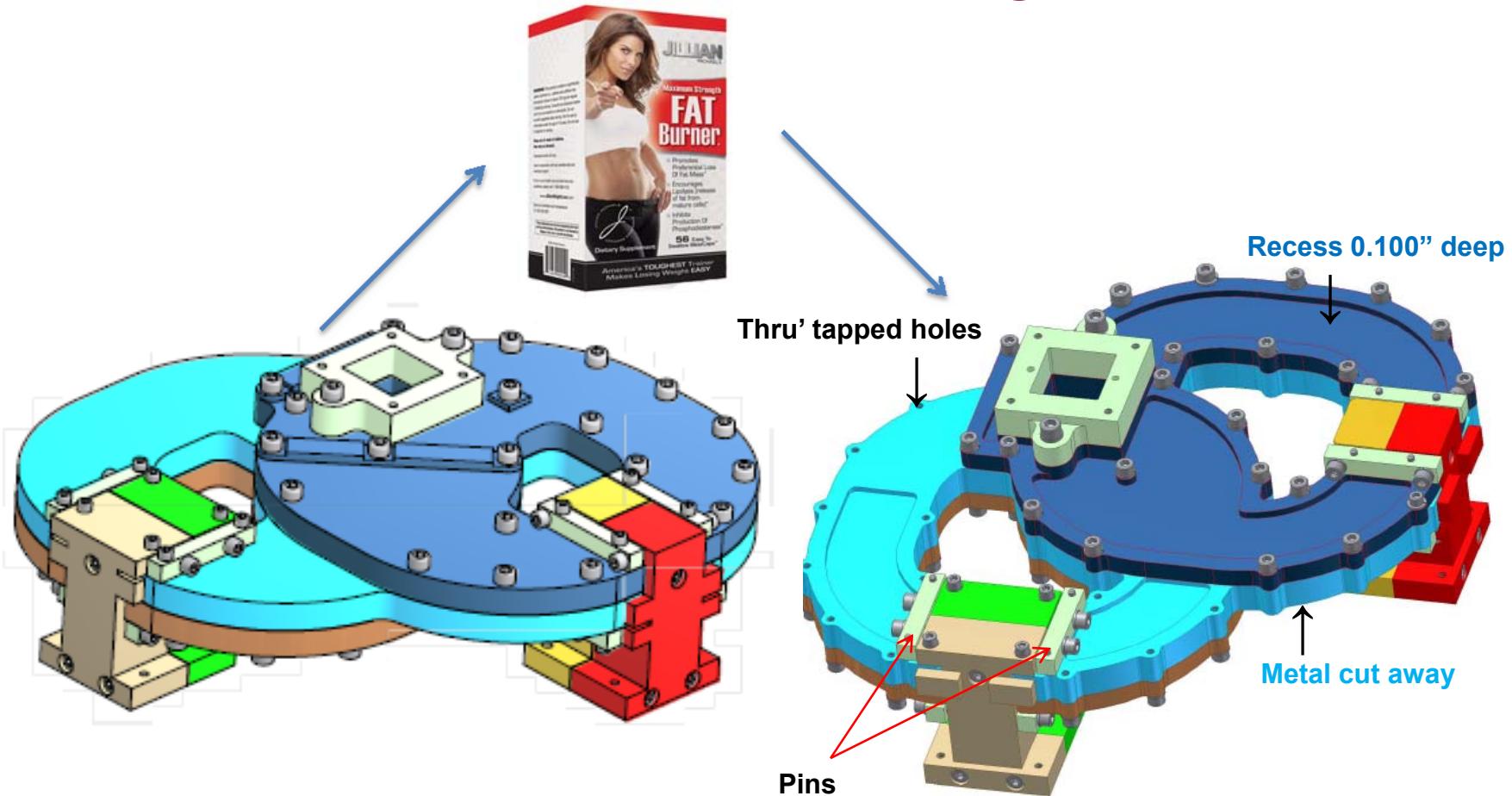
EVLA

EVLA





# Jillian Michaels Weight Loss Program



Weight: 4.39lbs  
Dia 9.25"; Ht 2.68"

Weight: 2.55lbs  
Dia 9.18"; Ht 2.68"