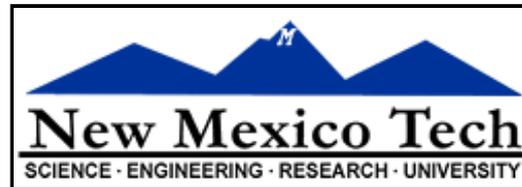


Antennas & Receivers in Radio Astronomy

Mark McKinnon



Twelfth Synthesis Imaging Workshop
2010 June 8-15



Outline

Context

Types of antennas

Antenna fundamentals

Reflector antennas

Mounts

Optics

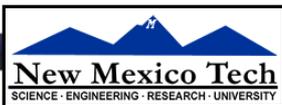
Antenna performance

Aperture efficiency

Pointing

Polarization

Receivers



Importance of the Antenna Elements

Antenna amplitude pattern causes amplitude to vary across the source.

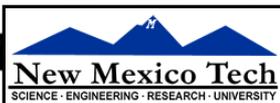
Antenna phase pattern causes phase to vary across the source.

Polarization properties of the antenna modify the apparent polarization of the source.

Antenna pointing errors can cause time varying amplitude and phase errors.

Variation in noise pickup from the ground can cause time variable amplitude errors.

Deformations of the antenna surface can cause amplitude and phase errors, especially at short wavelengths.



VLA @ 4.8 GHz (C-band)

Interferometer Block Diagram

Antenna

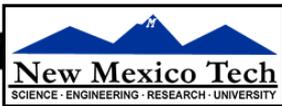
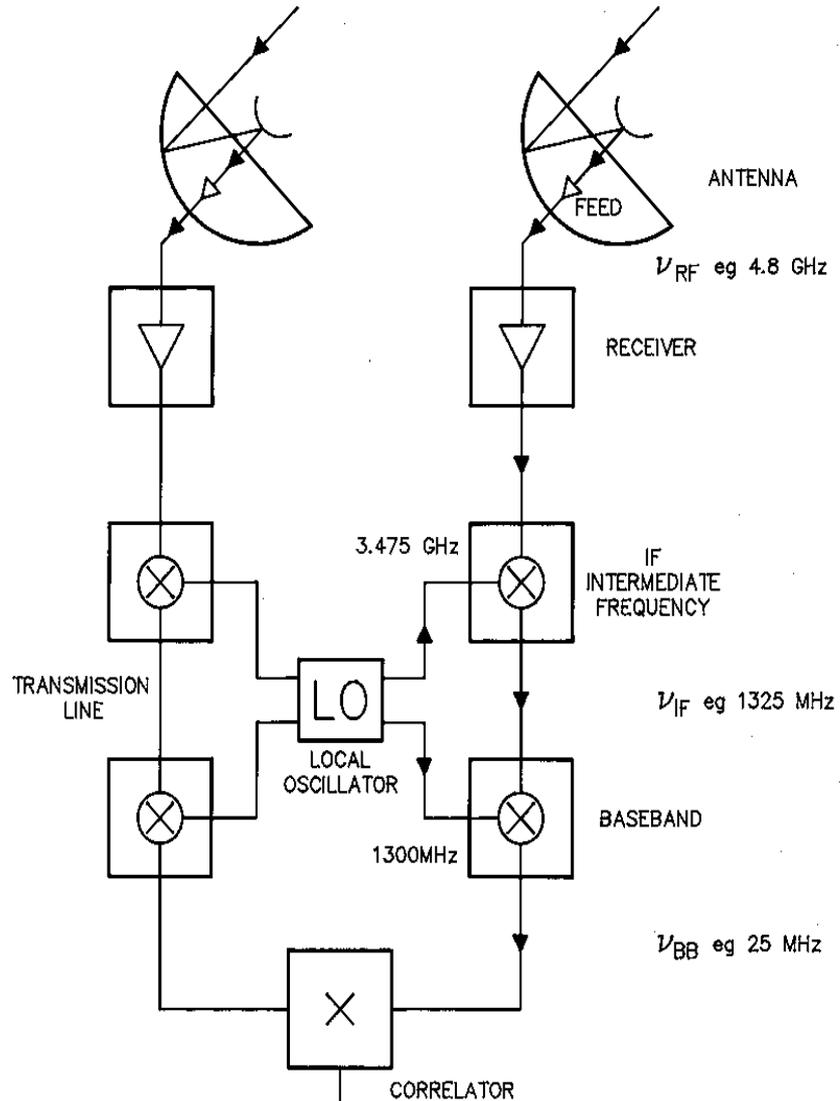
Front End

IF

Back End

Correlator

-  **Amplifier**
-  **Mixer**
-  **Correlator**



Types of Antennas

Wire antennas ($\lambda > 1\text{m}$)

Dipole

Yagi

Helix

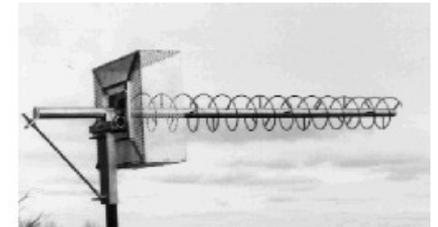
Small arrays of the above ($\lambda < 1\text{m}$)

Reflector antennas ($\lambda \approx 1\text{m}$)

Hybrid antennas

Wire reflectors

Reflectors with dipole feeds



Basic Antenna Formulas

Effective collecting
area $A(n, q, f)$ m²

$$P(\theta, \varphi, \nu) = A(\theta, \varphi, \nu) I(\theta, \varphi, \nu) \Delta\nu \Delta\Omega$$

On-axis response $A_0 = hA$
 h = aperture efficiency

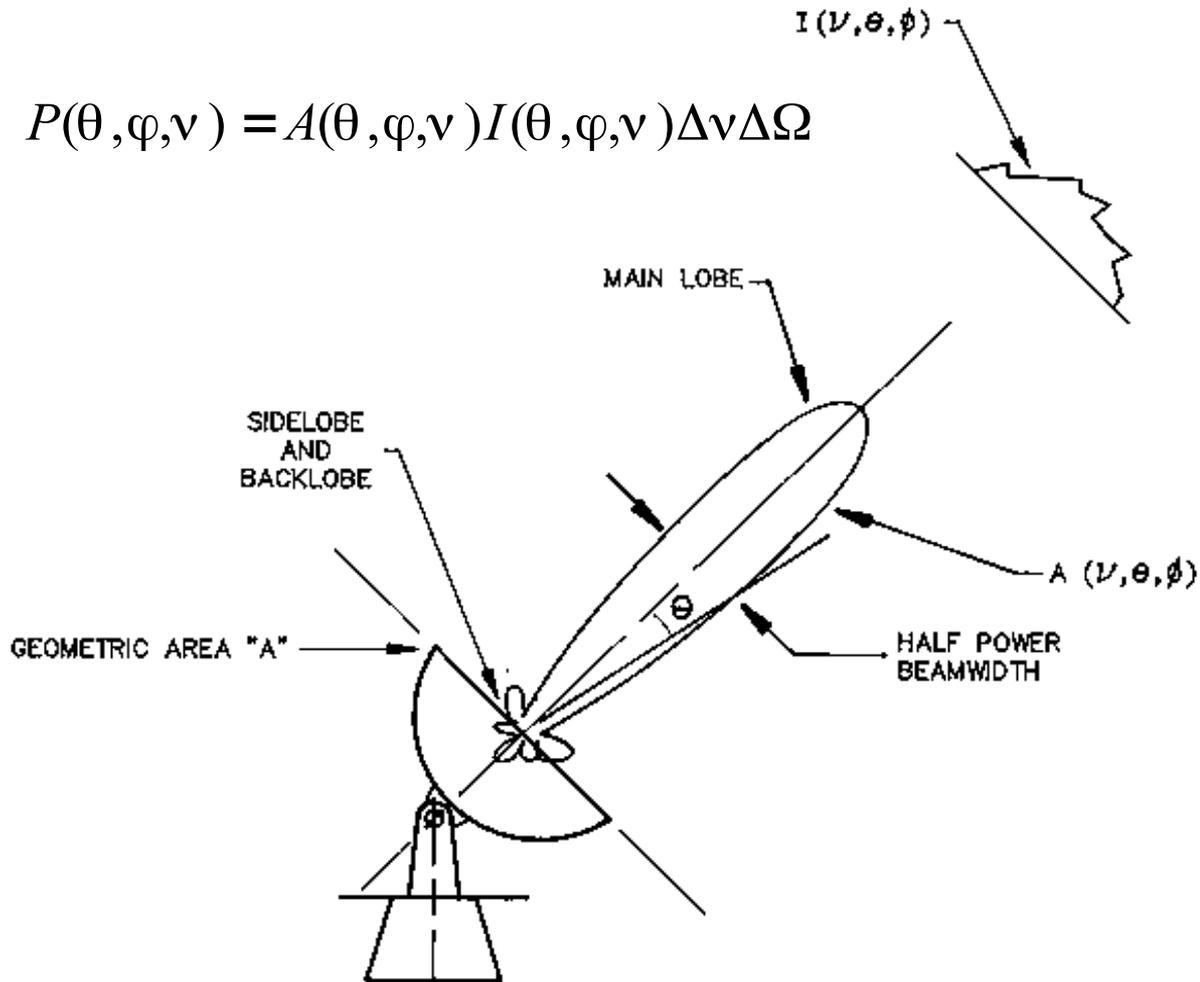
Normalized pattern
(primary beam)

$$A(n, q, f) = A(n, q, f) / A_0$$

Beam solid angle
 $WA = \iint A(n, q, f) dW$
all sky

$$A_0 WA = I_2$$

λ = wavelength, n = frequency



Aperture-Beam Fourier Transform Relationship

What determines the beam shape?

$f(u,v)$ = complex aperture field distribution

u,v = aperture coordinates (wavelengths)

$F(l,m)$ = complex far-field voltage pattern

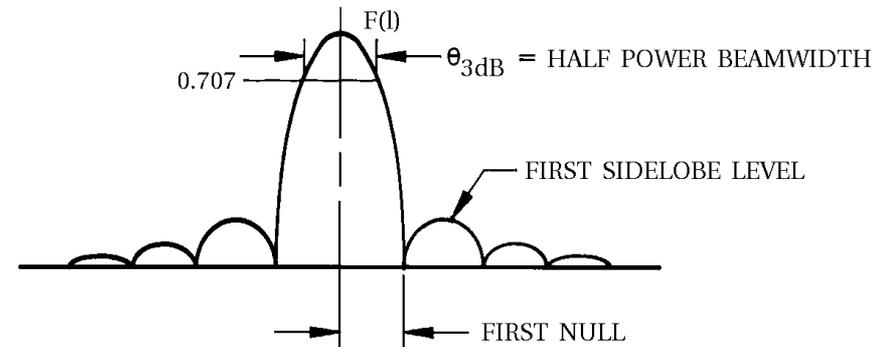
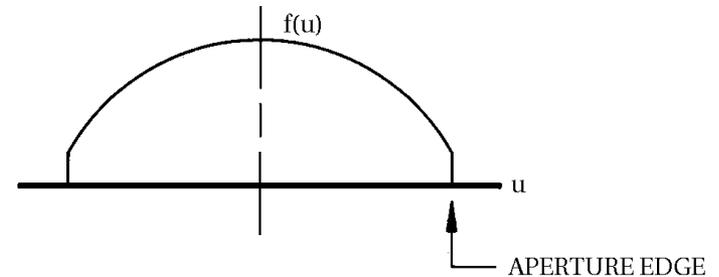
$l = \sin\theta\cos\phi$, $m = \sin\theta\sin\phi$

$F(l,m) = \iint_{\text{aperture}} f(u,v) \exp(2\pi i(ul+vm)) du dv$

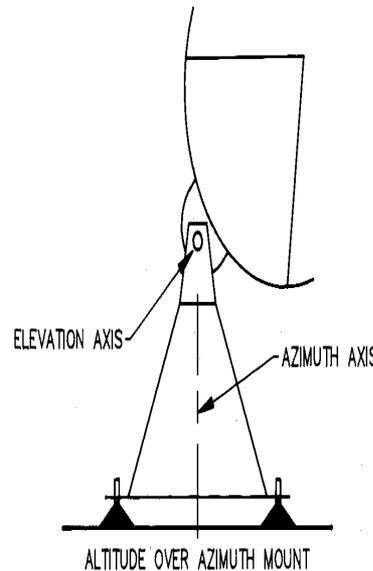
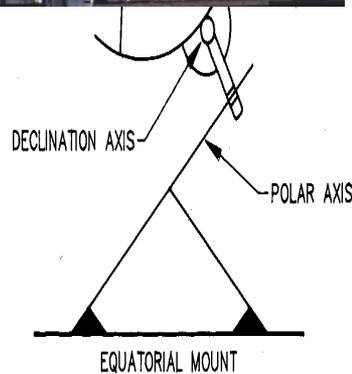
$f(u,v) = \iint_{\text{hemisphere}} F(l,m) \exp(-2\pi i(ul+vm)) dl dm$

For VLA: $\theta_{3dB} = 1.02/D$, First null = $1.22/D$,

D = reflector diameter in wavelengths



Antenna Mounts: Altitude over Azimuth



Advantages

Cost

Gravity performance

— advantages

one of avoidance

can rotate on sky

Antenna Mounts: Equatorial

Advantages

Tracking accuracy

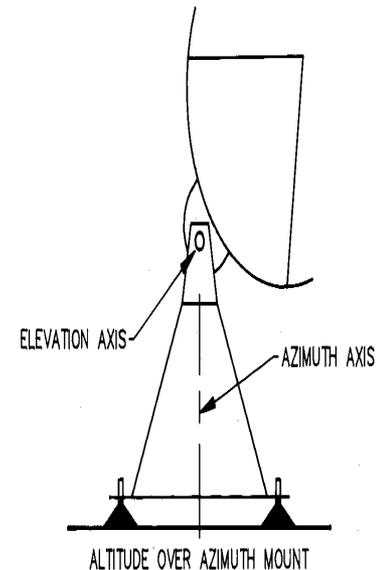
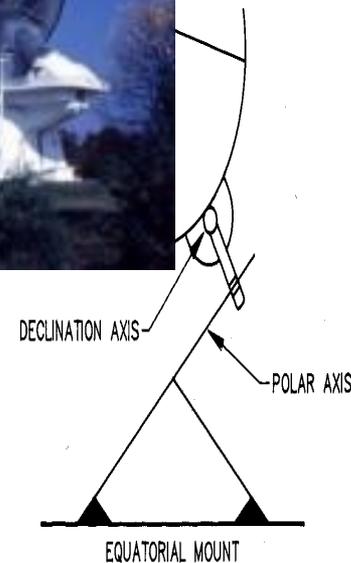
Beam doesn't rotate

Disadvantages

Cost

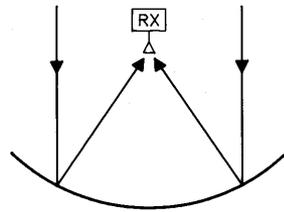
Gravity performance

Sources on horizon at pole

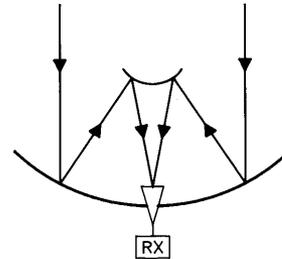


Reflector Optics

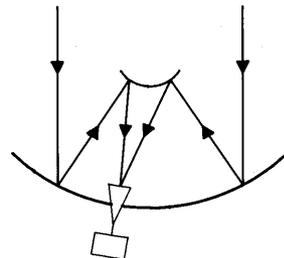
Prime focus



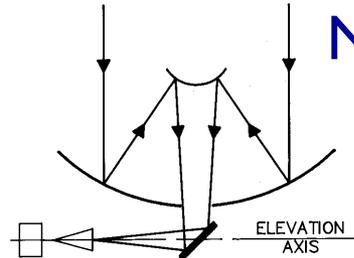
Cassegrain focus



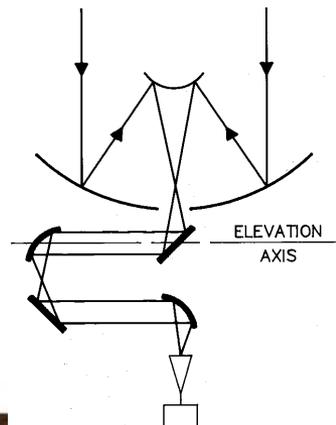
Offset Cassegrain



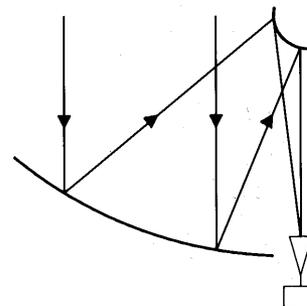
Naysmith



Beam Waveguide



Dual Offset



Reflector Optics: Limitations

Prime focus

Over-illumination (spillover) can increase system temperature due to ground pick-up

Number of receivers, and access to them, is limited

Subreflector systems

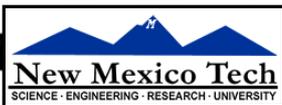
Can limit low frequency capability. Feed horn too large.

Over-illumination by feed horn can exceed gain of reflector's diffraction limited sidelobes

- Strong sources a few degrees away may limit image dynamic range

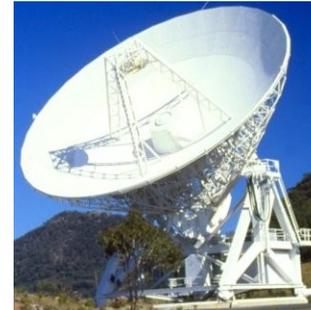
Offset optics

Support structure of offset feed is complex and expensive



Reflector Optics: Examples

Prime focus
(GMRT)



ocus

Offset Cassegrain
(VLA)

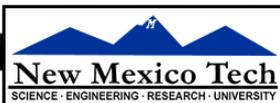


mith

Beam Waveguide
(NRO)



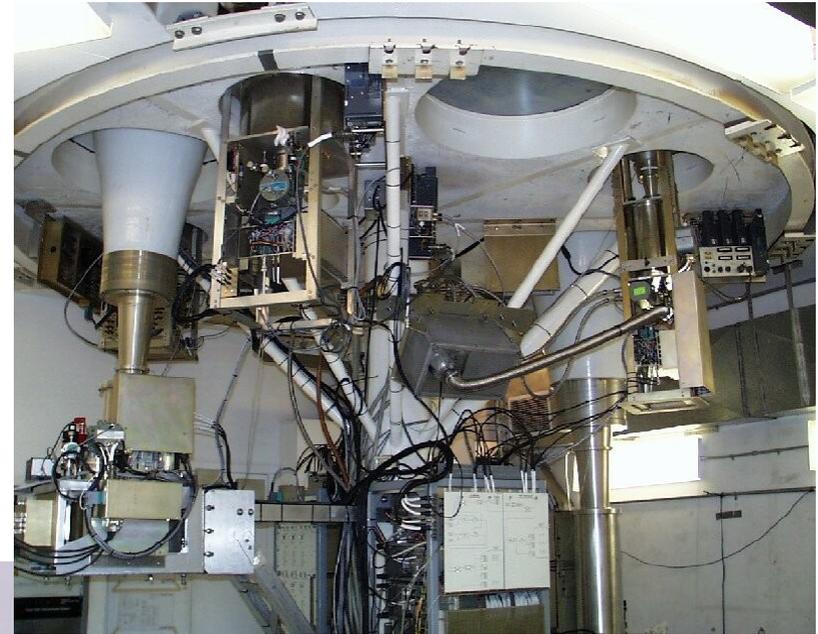
et



Feed Systems



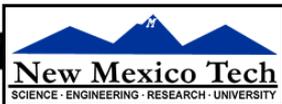
VLA



GBT



EVLA



Antenna Performance: Aperture Efficiency

15
15

On axis response: $A_0 = hA$

Efficiency: $h = h_{sf} \cdot h_{bl} \cdot h_s \cdot h_t \cdot h_{misc}$

h_{sf} = Reflector surface efficiency

Due to imperfections in reflector surface

$h_{sf} = \exp(-4ps/l^2)$ e.g., $s = l/16$, $h_{sf} = 0.5$

h_{bl} = Blockage efficiency

Caused by subreflector and its support structure

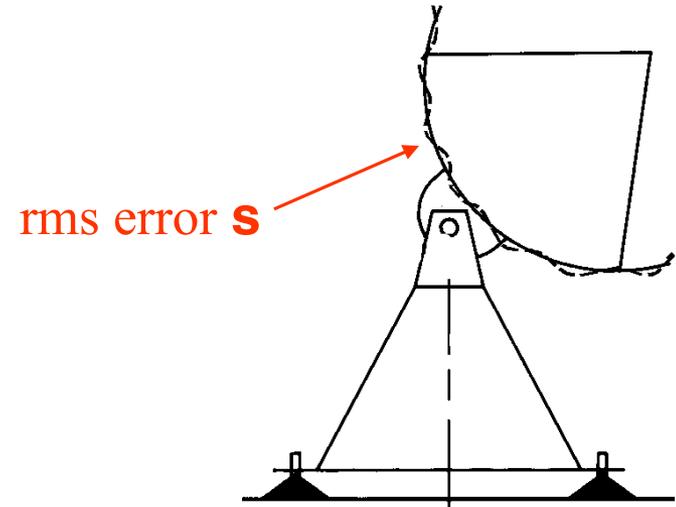
h_s = Feed spillover efficiency

Fraction of power radiated by feed intercepted by subreflector

h_t = Feed illumination efficiency

Outer parts of reflector illuminated at lower level than inner part

h_{misc} = Reflector diffraction, feed position phase errors, feed match and loss



Surface of ALMA Vertex Antenna

Surface measurements of DV02
made with holography

Measured surface rms = 10 μ m

rlucas@gns 25-MAY-2010 04:02:48

ALMA

Result file: DV02-before

- Required panel motion towards focus (μ m)
(positive number means a hole)

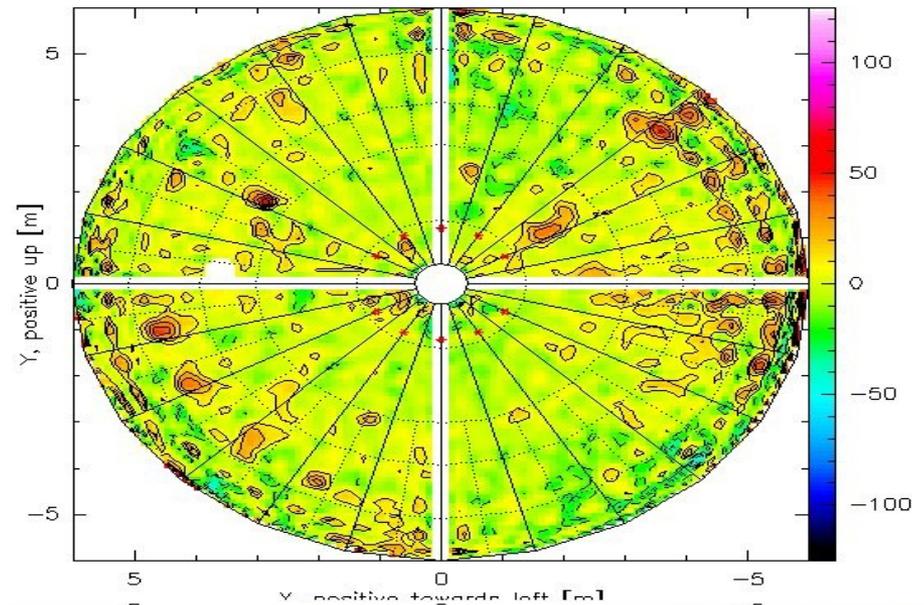
- map as seen from focus.

/users/rlucas/HoloDV02/uid X55 Xbf5 X1.map

rms (unweighted) 11.51 μ m

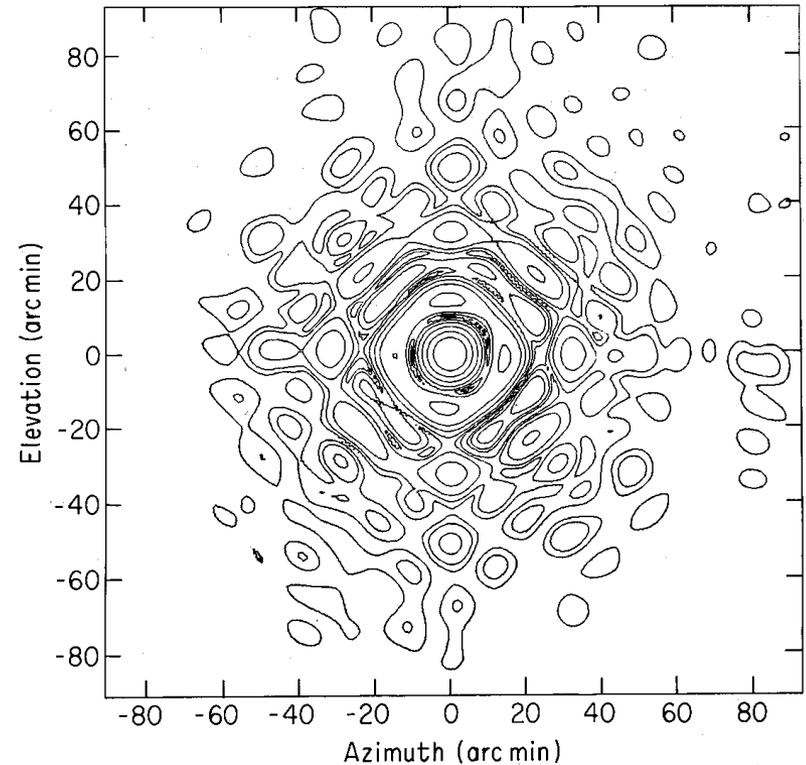
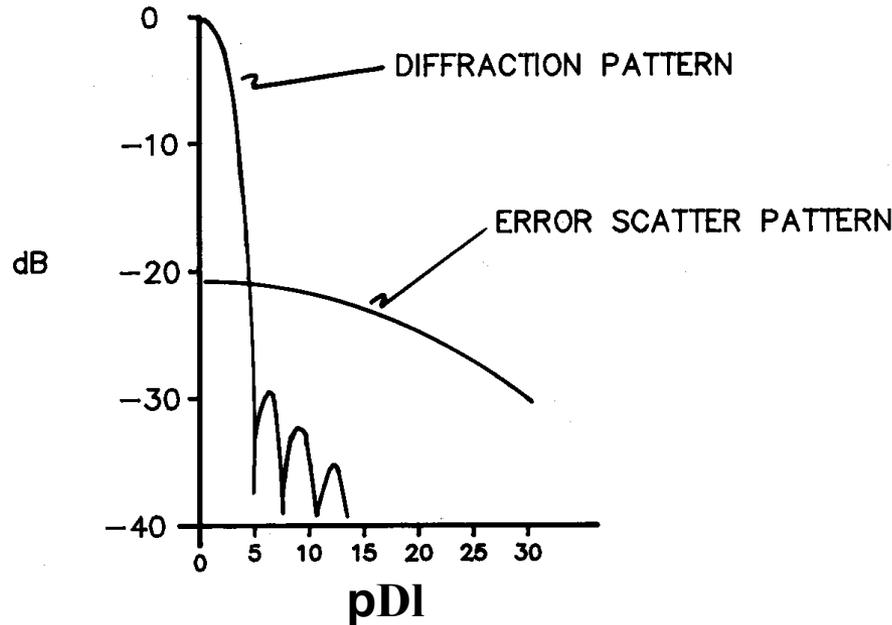
rms (amp. weighted) 9.79 μ m

rms (12dB weighted, cos α included) 9.45 μ m



Antenna Performance: Aperture Efficiency

Primary Beam



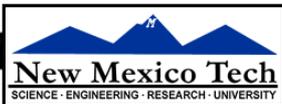
$l = \sin(\theta)$, D = antenna diameter in wavelengths

$\text{dB} = 10\log(\text{power ratio}) = 20\log(\text{voltage ratio})$

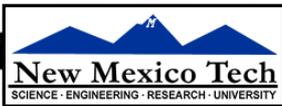
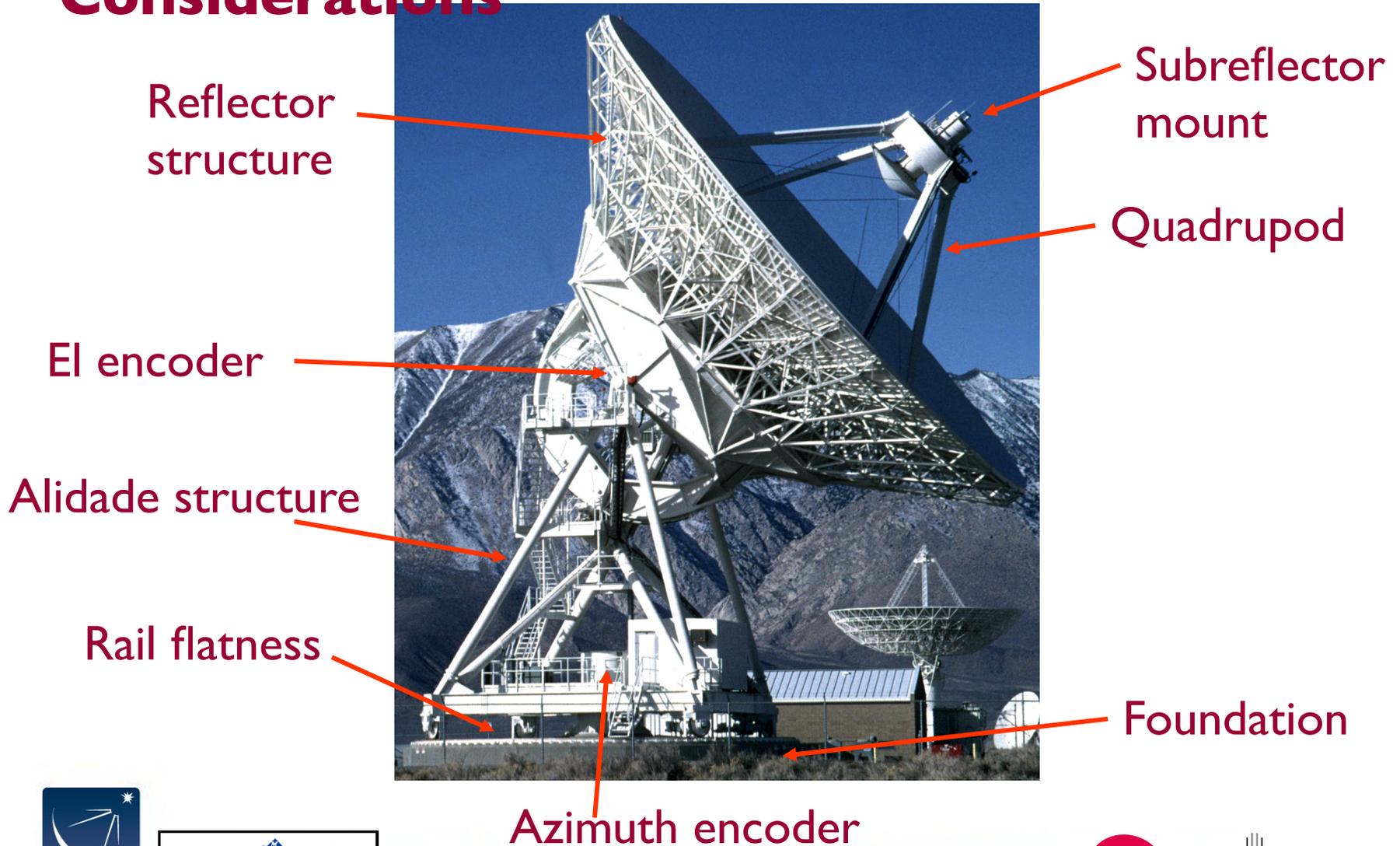
VLA: $\theta_{3\text{dB}} = 1.02/D$, First null = $1.22/D$

contours: -3, -6, -10, -15, -20, -25, -30, -35, -40 dB

Voltage radiation pattern, $|F(l,m)|$



Antenna Pointing: Practical Considerations



Pointing: ALMA Vertex Antennas

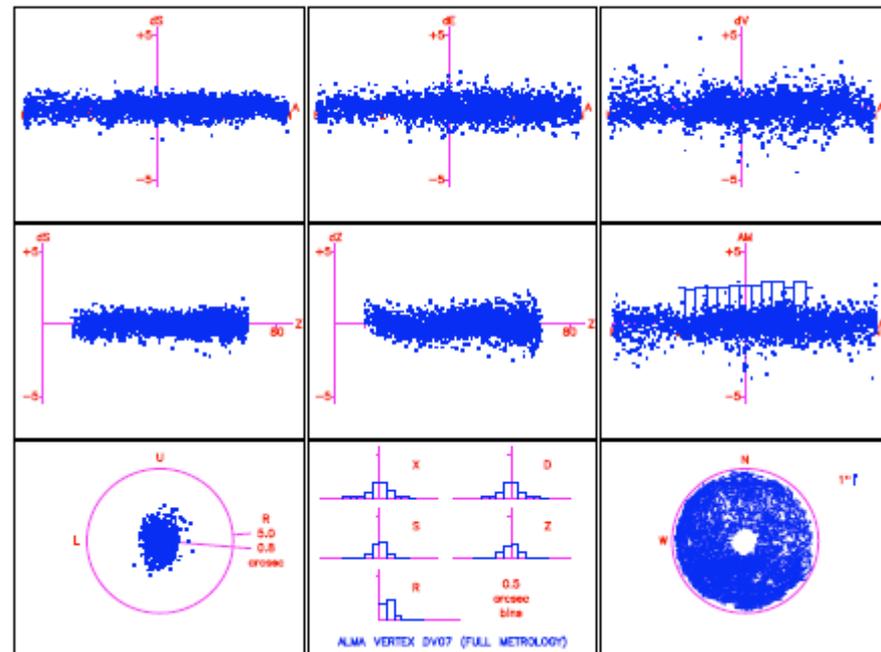
All-sky optical pointing on DV07 completed April 1-14

All-sky results (spec = 2" RMS)

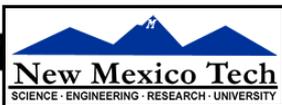
$0.77 \pm 0.12''$ RMS at OSF

$0.84 \pm 0.13''$ RMS scaled to AOS

All-sky and offset pointing within specifications!



DV07 pointing residuals: Mangum, N. Emerson, Mundnich & Stenvers



Antenna Performance: Pointing

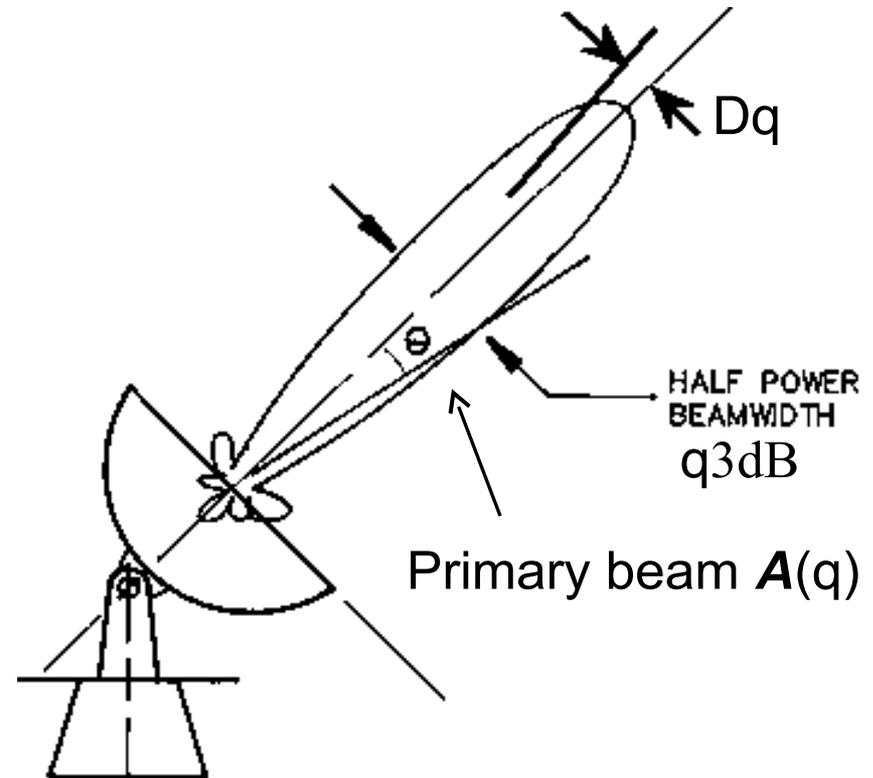
Pointing Accuracy

D_q = rms pointing error

Often $D_q < q_{3dB} / 10$ acceptable,
because $A(q_{3dB} / 10) \sim 0.97$

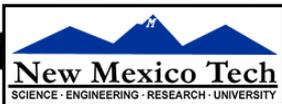
BUT, at half power point in beam

$$A(q_{3dB} / 2 \pm q_{3dB} / 10) / A(q_{3dB} / 2) = \pm 0.3$$



For best VLA pointing use Reference Pointing.

$$D_q = 3 \text{ arcsec} = q_{3dB} / 17 @ 50 \text{ GHz}$$



Antenna Performance: Polarization

Antenna can modify apparent polarization properties of the source:

Antenna structure

Symmetry of the optics

Reflections in the optics

Curvature of the reflectors

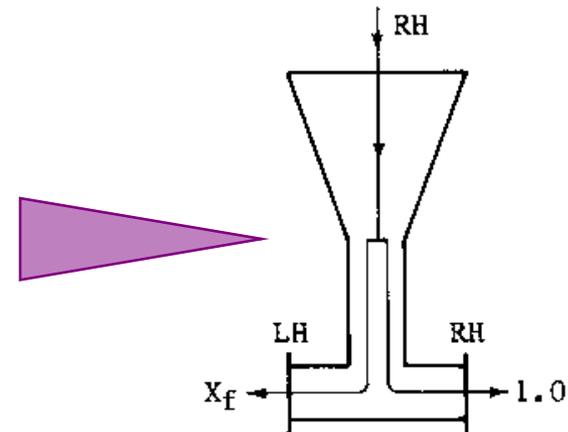
Quality of feed polarization splitter

Constant across the beam

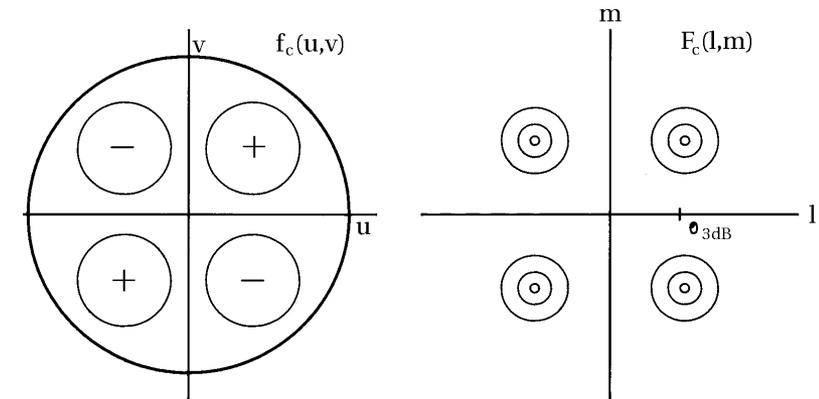
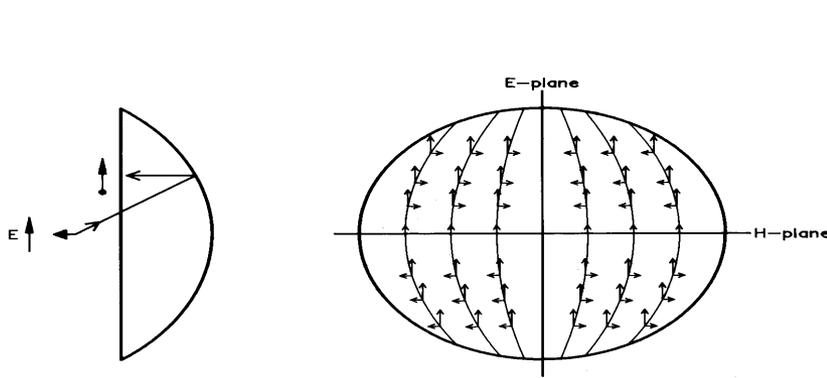
Circularity of feed radiation patterns

No instrumental polarization on-axis,

But cross-polarization varies across the beam ...



Off-Axis Cross Polarization

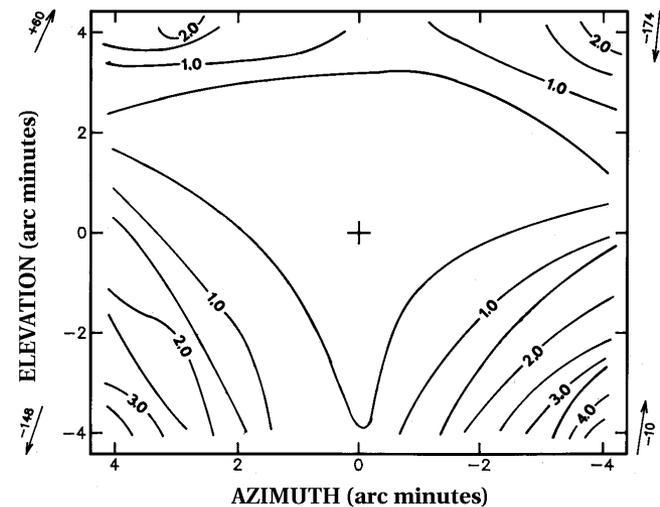


Cross-polarized aperture distribution

Cross-polarized primary beam

Field distribution in aperture of paraboloid fed by electric dipole

VLA 4.8 GHz cross-polarized primary beam



Receivers: Noise Temperature

Reference received power to the equivalent temperature of a matched load at the input to the receiver

Rayleigh-Jeans approximation to Planck radiation law for a blackbody

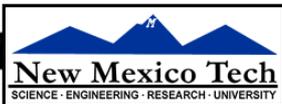
$$P_{in} = kBT \quad (\text{W})$$

k_B = Boltzman's constant (1.38×10^{-23} J/oK)

When observing a radio source, $T_{total} = T_A + T_{sys}$

T_{sys} = system noise when not looking at a discrete radio source

T_A = source antenna temperature



Receivers: SEFD

$$TA = \frac{AS}{2kB} = KS$$

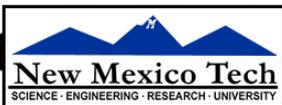
S = source flux (Jy)

SEFD = system equivalent flux density

$$SEFD = T_{sys}/K \text{ (Jy)}$$

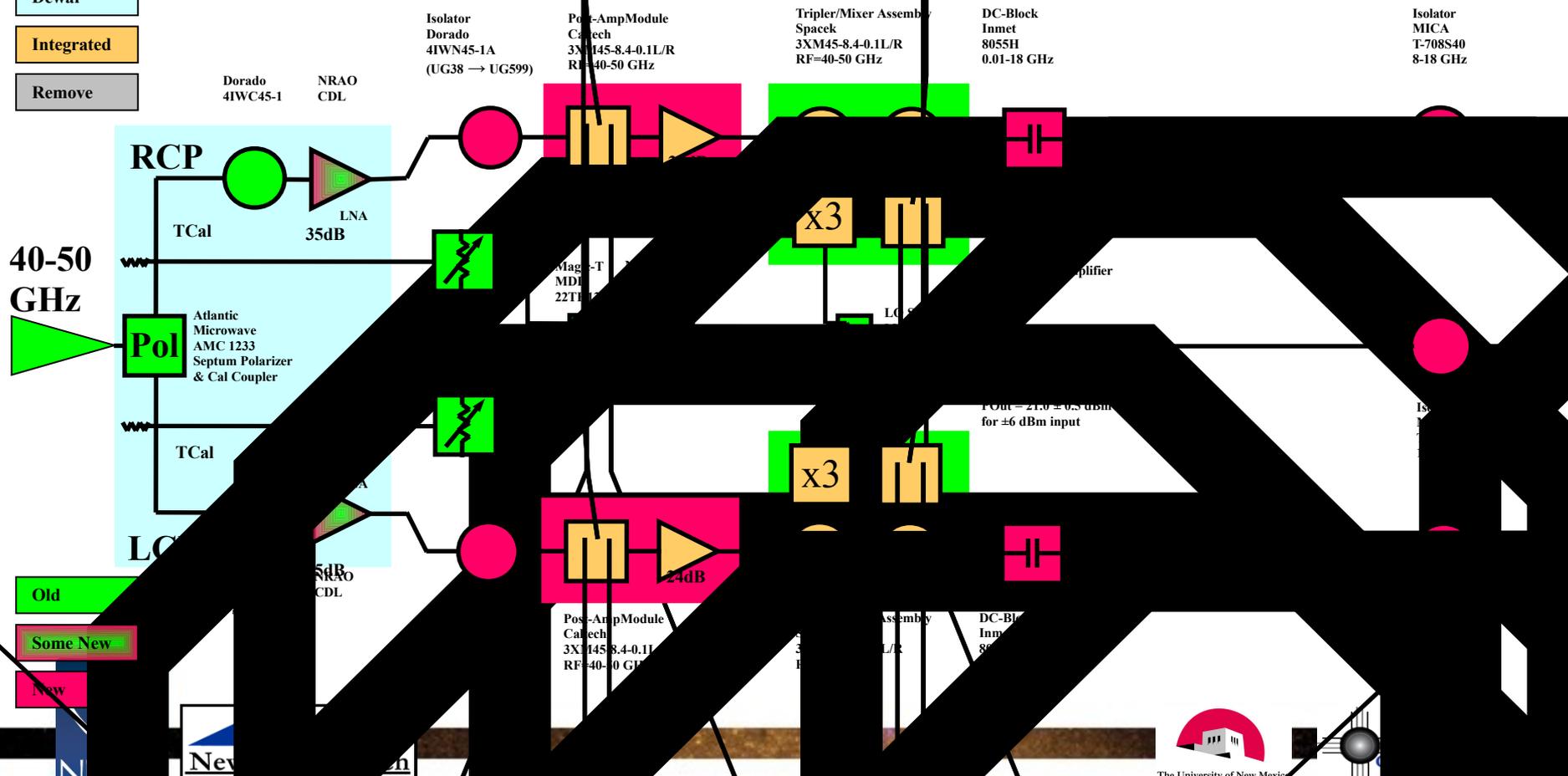
EVLA Sensitivities

Band (GHz)	$\frac{A}{\lambda}$	Tsys	SEFD
1-2	.50	21	236
2-4	.62	27	245
4-8	.60	28	262
8-12	.56	31	311
12-18	.54	37	385
18-26	.51	55	606
26-40	.39	58	836
40-50	.34	78	1290



EVLA Q-Band (40-50 GHz) Receiver

- Dewar
- Integrated
- Remove



- Old
- Some New
- New

