











Spectral Line Observing

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- Spectral line observers use many channels of width δv , over a total bandwidth Δv . Why?
- Science driven: science depends on frequency (spectroscopy)
 - Emission and absorption lines, and their Doppler shifts
 - Slope across continuum bandwidth
- Technical reasons: science does not depend on frequency (pseudo-continuum)







Spectroscopy

- Need high spectral resolution to resolve spectral features
 - Example: SiO emission from a protostellar jet imaged with the VLA (Chandler & Richer 2001).





 High resolutions over large bandwidths are useful for e.g., doppler shifts and line searches => many channels desirable!



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- Science does not depend on frequency, but using spectral line mode is favorable to correct for some instrumental responses:
 - Avoid limitations of bandwidth smearing
 - Avoid limitations of beam smearing
 - Avoid problems due to atmospheric changes as a function of frequency
 - Avoid problems due to signal transmission effects as a function of frequency
- A spectral line mode also allows editing for unwanted, narrowband interference.







Instrument response: beam smearing

- $\theta_{PB} = \lambda/D$
- Band covers λ_1 to λ_2 $\Rightarrow \theta_{PB}$ changes by λ_1/λ_2
- More important at longer wavelengths:
 - VLA 20cm: 1.04
 - VLA 2cm: 1.003
 - EVLA 20cm: 2.0
 - ALMA 1mm: 1.03



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Instrument response: bandwidth smearing

- Also called chromatic aberration
- Fringe spacing = λ/B
- Band covers λ_1 to λ_2
 - Fringe spacings change by λ_1/λ_2
 - uv samples smeared radially
 - More important in larger configurations, and for lower frequencies
- Huge effects for EVLA

Pseudo-continuum uses smaller ranges to be averaged later.











Instrument frequency response

 Responses of antenna receiver, feed, IF transmission lines, electronics are a function of frequency.





 Phase slopes (delays) can be introduced by incorrect clocks or positions.

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Atmosphere changes with frequency

- Atmospheric transmission, phase (delay), and Faraday rotation are functions of frequency
 - Generally only important over very wide bandwidths, or near atmospheric lines
 - An issue for ALMA





Radio Frequency Interference (RFI)

- Avoid known RFI if possible, e.g. by constraining your bandwidth.
- Possible in some cases but not always.



RFI at the VLA, 1.2-1.8 GHz



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Observations: data editing and calibration

- Not fundamentally different from continuum observations, but a few additional items to consider:
 - Presence of RFI (data flagging)
 - Bandpass calibration
 - Doppler corrections
 - Correlator setup
 - Larger data sets







Editing spectral line data

- Start with identifying problems affecting all channels, by using a frequency averaged 'Channel 0' data set.
 - Has better SNR.
 - Copy flag table to the line data.
- Continue with checking the line data for narrow-band RFI that may not show up in averaged data.
 - Channel by channel impractical, instead identify features by using cross-power spectra (POSSM).
 - Is it limited in time? Limited to specific telescope (VLBI) or baseline length (VLA)?
 - Flag based on the feature using SPFLG, EDITR, TVFLG, WIPER.







Example POSSM scalar averaged spectra VLA



• Note: avoid excessive frequency dependent editing, since this introduces changes in the *u*,*v* - coverage across the band.







Spectral response

- For spectroscopy in an XF correlator (VLA, EVLA) additional lags are introduced and the correlation function is measured for a large number of lags.
 - The FFT gives the spectrum.
- However, we don't have infinitely large correlators and infinite amount of time, so we don't measure an infinite number of Fourier components.
 - A finite number or lags means a truncated lag spectrum, which corresponds to multiplying the true spectrum by a box function.
 - The spectral response is the FT of the box, which for an XF correlator is a sinc(πx) function with nulls spaced by the channel separation: 22% sidelobes!





Spectral response: Gibb's ringing



- Thus, this produces a "ringing" in frequency called the Gibbs phenomenon.
- Occurs at sharp transitions:
 - Narrow banded spectral lines (masers, RFI)
 - Band edges
 - Baseband (zero frequency)







Gibb's ringing: remedies

- Increase the number of lags, or channels.
 - Oscillations reduce to ~2% at channel 20, so discard affected channels.
 - Works for band-edges, but not for spectral features.
- Smooth the data in frequency (i.e., taper the lag spectrum)
 - Usually Hanning smoothing is applied, reducing sidelobes to <3%.



$$S_h(\nu_i) = \frac{S(\nu_{i-1}) + 2S(\nu_i) + S(\nu_{i+1})}{4}$$







• We need the total response of the instrument to determine the true visibilities from the observed:

$$V_{ij}(t,v)_{obs} = V_{ij}(t,v)G_{ij}(t)$$

- The bandpass shape is a function of frequency, and is mostly due to electronics of individual antennas.
 - Usually varies slowly with time, so we can break the complex gain $G_{ij}(t)$ into a fast varying frequency independent part, $G'_{ij}(t,v)$, and a slowly varying frequency dependent part $B_{ij}(t,v)$:

$$V_{ij}(t,v)_{obs} = V_{ij}(t,v)G'_{ij}(t)B_{ij}(t,v)$$

• $G'_{ij}(t)$ is calibrated as for continuum, and the process of determining $B_{ij}(t,v)$ is the bandpass calibration.







Why bandpass calibration is important

- Important to be able to detect and analyze spectral features:
 - Frequency dependent amplitude errors limit the ability of detecting weak emission and absorption lines.
 - Frequency dependent phase errors can lead to spatial offsets between spectral features, imitating doppler motions.
 - Frequency dependent amplitude errors can imitate changes in line structures.
- For pseudo-continuum, the dynamic range of final image is limited by the bandpass quality.







Example ideal and real bandpass



- In the bandpass calibration we want to correct for the offset of the real bandpass from the ideal one (amp=1, phase=0).
- The bandpass is the relative gain of an antenna/baseline as a function of frequency.



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- To compute the bandpass correction, a strong continuum calibrator is observed at least once.
- The most commonly used method is analogous to channel by channel self-calibration (AIPS task BPASS)
 - The calibrator data is divided by a source model or continuum, which removes atmospheric and source structure effects.
 - Most frequency dependence is antenna based, and the antennabased gains are solved for as free parameters.
- This requires a high SNR, so what is a good choice of a BP calibrator?







How to select a BP calibrator

- Select a continuum source with:
 - High SNR in each channel
 - Intrinsically flat spectrum
 - No spectral lines
- Not required to be a point source, but helpful since the SNR will be the same in the BP solution for all baselines.

Spectra of three potential calibrators. Only the bottom one is ok.



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How long to observe a BP calibrator

- Applying the BP calibration means that every complex visibility spectrum will be divided by a complex bandpass, so noise from the bandpass will degrade all data.
- Need to spend enough time on the BP calibrator so that SNR_{BPcal} > SNR_{target}. A good rule of thumb is to use

 $SNR_{BPcal} > 3 \times SNR_{target}$

which then results in an integration time:

$$t_{\text{BPcal}} = 3 \times (S_{\text{target}} / S_{\text{BPcal}})^2 t_{\text{target}}$$







Assessing quality of BP calibration

ullet



- Examples of good-quality bandpass solutions for 2 antennas.
- Solutions should look comparable for all antennas.
- Mean amplitude ~1 across useable portion of the band.
- No sharp variations in amplitude and phase; variations are not dominated by noise.
- Phase slope across the band indicates residual delay error.









Bad quality bandpass solutions four 4 antennas

- Amplitude has different normalization for different antennas
- Noise levels are high, and are different for different antennas



Bandpass quality: apply to a continuum source

- Before accepting the BP solutions, apply to a continuum source and use cross-correlation spectrum to check:
 - That phases are flat
 - That amplitudes are constant
 - That the noise is not increased by applying the BP





- G'_{ij}(t) and B_{ij}(v,t) are separable, and multiplicative errors in G'_{ij}(t) (including phase and gain calibration errors) can be reduced by subtracting structure in line-free channels. Residual errors will scale with the peak remaining flux.
- This is not true for B_{ij}(v,t) any errors in the bandpass calibration will always be in your data. Residual errors will scale as continuum fluxes in your observed field.







- Observing from the surface of the Earth, our velocity with respect to astronomical sources is not constant in time or direction.
- Doppler tracking can be applied in real time to track a spectral line in a given reference frame, and for a given velocity definition:

$$V_{radio}/c = (v_{rest} - v_{obs})/v_{rest}$$

$$V_{opt}/c = (v_{rest} - v_{obs})/v_{obs}$$







Rest frames

Correct for	<u>Amplitude</u>	<u>Rest frame</u>
Nothing	0 km/s	Topocentric
Earth rotation	< 0.5 km/s	Geocentric
Earth/Moon barycenter	< 0.013 km/s	E/M Barycentric
Earth around Sun	< 30 km/s	Heliocentric
Sun/planets barycenter	< 0.012 km/s	SS Barycentric (~Helioc)
Sun peculiar motion	< 20 km/s	Local Standard of Rest
Galactic rotation	< 300 km/s	Galactocentric

Start with the topocentric frame, the successively transform to other frames. Transformations standardized by IAU.







- However, the bandpass shape is really a function of *frequency*, not velocity!
 - Applying doppler tracking will introduce a time-dependent and position dependent frequency shift.
 - If you doppler track your BP calibrator to the same velocity as your source, it will be observed at a different sky frequency!
 - In this case, apply corrections during post-processing instead.
 - Given that wider bandwidths are now being used (EVLA, SMA, ALMA) online doppler tracking is unlikely to be used in the future (tracking only correct for a single frequency).







Continuum subtraction

- Spectral line data often contains continuum emission, either from the target or from nearby sources in the field of view.
 - This emission complicates the detection and analysis of line data



Spectral line cube with two continuum sources (structure independent of frequency) and one spectral line source.

Roelfsma 1989







Continuum subtraction: basic concept



- Use channels with no line features to model the continuum
- Subtract this continuum model from all channels







- Spectral lines easier to see, especially weak ones.
- Easier to compare the line emission between channels.
- Deconvolution is non-linear: can give different results for different channels since u,v - coverage and noise differs (results usually better if line is deconvolved separately).
- If continuum sources exists far from the phase center, we don't need to deconvolve a large field of view to properly account for their sidelobes.

To remove the continuum, different methods are available: visibility based, image based, or a combination thereof.







Visibility based continuum subtraction (UVLIN)

- A low order polynomial is fit to a group of line free channels in each visibility spectrum, the polynomial is then subtracted from whole spectrum.
- Advantages:
 - Fast, easy, robust
 - Corrects for spectral index slopes across spectrum
 - Can do flagging automatically (based on residuals on baselines)
 - Can produce a continuum data set
- Restrictions:
 - Channels used in fitting must be line free (a visibility contains emission from all spatial scales)
 - Only works well over small field of view $\theta << \theta_s \nu / \Delta v_{tot}$







UVLIN restriction: small field of view

- A consequence of the visibility of a source being a sinusoidal function
- For a source at distance / from phase center observed on baseline *b*:

 $V = \cos \left(2\pi v l/c \right) + i \sin(2\pi v l/c)$

This is linear only over a small range of v and for small b and l.









Image based continuum subtraction (IMLIN)

- Fit and subtract a low order polynomial fit to the line free part of the spectrum measured at each spatial pixel in cube.
- Advantages:
 - Fast, easy, robust to spectral index variations
 - Better at removing point sources far away from phase center (Cornwell, Uson and Haddad 1992).
 - Can be used with few line free channels.
- Restrictions:
 - Can't flag data since it works in the image plane.
 - Line and continuum must be simultaneously deconvolved.







Visualizing spectral line data

- After mapping all channels in the data set, we have a spectral line data *cube*.
- The cube is 3-dimensional (RA, Dec, Velocity). To visualize the information we usually make 1-D or 2-D projections:
 - Line profiles
 - Channel maps
 - Position-velocity plots
 - Moment maps

(1-D slices along velocity axis)
(2-D slices along velocity axis)
(slices along spatial dimension)
(integration along the velocity axis)







Example: line profiles

- Line profiles shows changes in line shape, width and depth.
- Right: EVN+MERLIN 1667 MHz OH maser emission and absorption spectra in IIIZw35.





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Example: channel maps

- Channel maps show how the spatial distribution of the line feature changes with frequency/velocity.
- Right: Contours continuum emission, grey scale 1667 MHz OH line emission in IIIZw35.



37



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Example 2-D model: rotating disk



Example: position-velocity plots

 PV-diagrams shows, for example, the line emission velocity as a function of radius. Here along a line through the dynamical center of the galaxy





Distance along slice

 Greyscale & contours convey intensity of the emission.

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39

Moment analysis

• You might want to derive parameters such as integrated line intensity, centroid velocity of components and line widths - all as functions of positions. Estimate using the *moments* of the line profile:

$$\begin{split} I_{\text{tot}}(\alpha, \delta) &= \Delta v \sum_{i=1}^{N_{\text{chan}}} S_{\nu}(\alpha, \delta, \nu_{i}) \\ \overline{v}(\alpha, \delta) &= \frac{\sum_{i=1}^{N_{\text{chan}}} v_{i} S_{\nu}(\alpha, \delta, \nu_{i})}{\sum_{i=1}^{N_{\text{chan}}} S_{\nu}(\alpha, \delta, \nu_{i})} \\ \sigma_{v}(\alpha, \delta) &= \sqrt{\langle (v_{i} - \overline{v}(\alpha, \delta))^{2} \rangle} \\ &= \sqrt{\frac{\sum_{i=1}^{N_{\text{chan}}} (v_{i} - \overline{v}(\alpha, \delta))^{2} S_{\nu}(\alpha, \delta, \nu_{i})}{\sum_{i=1}^{N_{\text{chan}}} S_{\nu}(\alpha, \delta, \nu_{i})}} \\ \end{split}$$
Total intensity (Moment 0)
Intensity-weighted velocity dispersion (Moment 2)
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Moment analysis





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Moment maps



Moment 0 (Total Intensity)

Moment 1 (Velocity Field)

Moment 2 (Velocity Dispersion)







42

- Moments sensitive to noise so clipping is required
 - Higher order moments depend on lower ones so progressively noisier.
- Hard to interpret correctly:
 - Both emission and absorption may be present, emission may be double peaked.
 - Biased towards regions of high intensity.
 - Complicated error estimates: number or channels with real emission used in moment computation will greatly change across the image.
- Use as guide for investigating features, or to compare with other λ .
- Alternatives...?
 - Gaussian fitting for simple line profiles.
 - Maxmaps shows emission distribution.







Visualizing spectral line data: 3-D rendering



L. Matthews



Display produced using the 'xray' program in the karma software **Ne** package (http://www.atnf.csiro.au/computing/software/karma/)

