

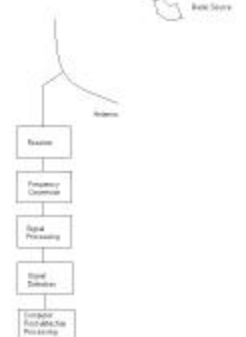


Antennas in Radio Astronomy

Peter Napier

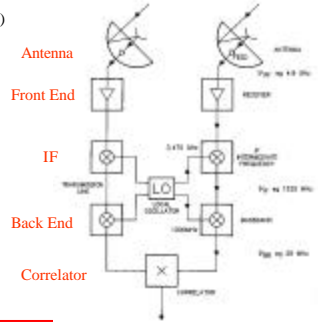
- Interferometer block diagram
- Antenna fundamentals
- Types of antennas
- Antenna performance parameters
- Receivers

RADIO TELESCOPE BLOCK DIAGRAM

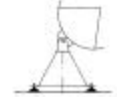


eg. VLA observing at 4.8 GHz (C band)

Interferometer Block Diagram



Importance of the Antenna Elements



- Antenna amplitude pattern causes amplitude to vary across the source.
- Antenna phase pattern causes phase to vary across the source.
- Polarization properties of the antenna modify the apparent polarization of the source.
- Antenna pointing errors can cause time varying amplitude and phase errors.
- Variation in noise pickup from the ground can cause time variable amplitude errors.
- Deformations of the antenna surface can cause amplitude and phase errors, especially at short wavelengths.

General Antenna Types

Wavelength > 1 m (approx) Wire Antennas

- Dipole
- Yagi
- Helix or arrays of these

Wavelength < 1 m (approx) Reflector antennas

Wavelength = 1 m (approx) Hybrid antennas (wire reflectors or feeds)

BASIC ANTENNA FORMULAS

Effective collecting area $A(\theta, \phi, \lambda)$ m^2

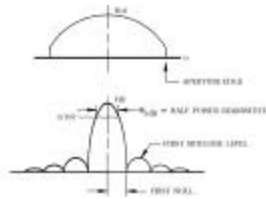
On-axis response $A_0 = \epsilon A$
 ϵ = aperture efficiency

Normalized pattern (primary beam)
 $\mathcal{A}(\theta, \phi, \lambda) = A(\theta, \phi, \lambda) / A_0$

Beam solid angle $\Omega_A = \int \mathcal{A}(\theta, \phi, \lambda) d\Omega$
 λ = wavelength

Aperture-Beam Fourier Transform Relationship

$f(u,v)$ = complex aperture field distribution
 u,v = aperture coordinates (wavelengths)



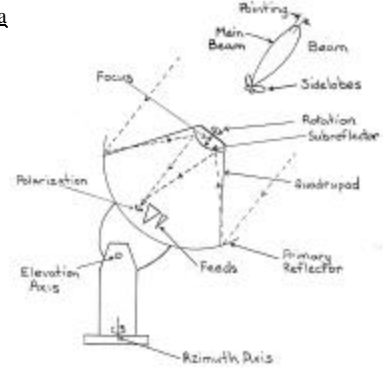
$F(l,m)$ = complex far-field voltage pattern
 $l = \sin\theta \cos\phi$, $m = \sin\theta \sin\phi$

$$F(l,m) = \int_{\text{aperture}} f(u,v) \exp(2\pi i(ul+vm)) du dv$$

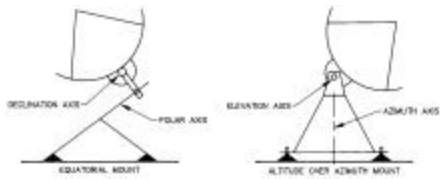
$$f(u,v) = \int_{\text{aperture}} F(l,m) \exp(-2\pi i(ul+vm)) dl dm$$

For VLA: $\theta_{3dB} = 1.02/D$, First null = $1.22/D$,
 D = reflector diameter in wavelengths

Primary Antenna Key Features

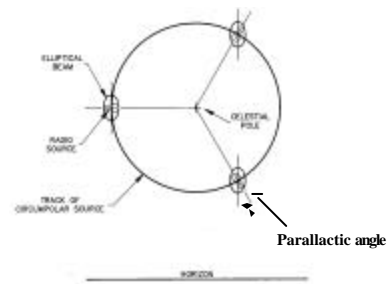


Types of Antenna Mount

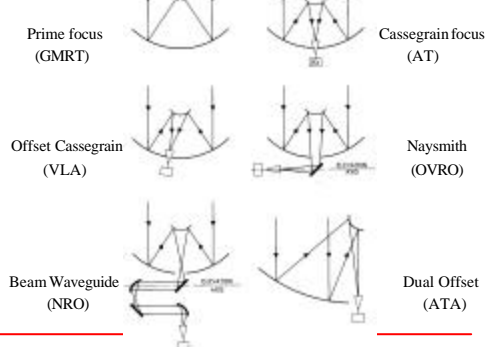


- | | |
|------------------------------|------------------------------|
| + Beam does not rotate | + Lower cost |
| + Better tracking accuracy | + Better gravity performance |
| - Higher cost | - Beam rotates on the sky |
| - Poorer gravity performance | |
| - Non-intersecting axis | |

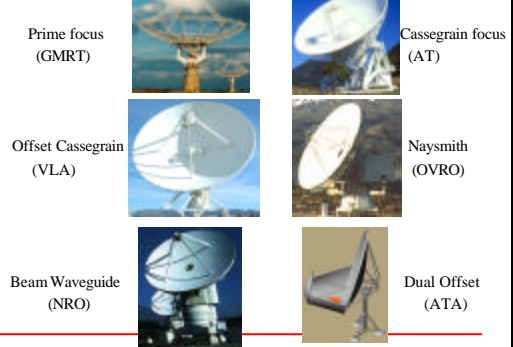
Beam Rotation on the Sky



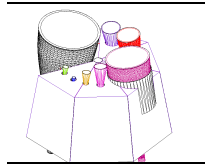
REFLECTOR TYPES



REFLECTOR TYPES



VLA and EVLA Feed System Design



Antenna Performance Parameters

Aperture Efficiency

$$A_0 = \eta A_{\text{phys}} = \eta_{\text{sf}} \times \eta_{\text{bl}} \times \eta_{\text{s}} \times \eta_{\text{t}} \times \eta_{\text{misc}}$$

η_{sf} = reflector surface efficiency

η_{bl} = blockage efficiency

η_{s} = feed spillover efficiency

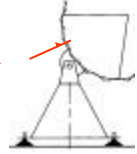
η_{t} = feed illumination efficiency

η_{misc} = diffraction, phase, match, loss

$$\eta_{\text{sf}} = \exp(-4 \left(\frac{\sigma}{\lambda} \right)^2)$$

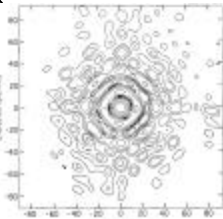
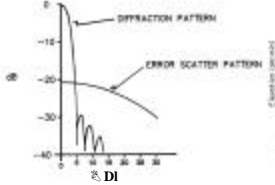
eg $\sigma = \lambda/16$, $\eta_{\text{sf}} = 0.5$

rms error σ



Antenna Performance Parameters

Primary Beam



$l = \sin(\theta)$, D = antenna diameter in wavelengths

contours: -3,-6,-10,-15,-20,-25,-30,-35,-40 dB

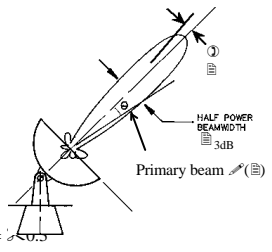
dB = 10log(power ratio) = 20log(voltage ratio)

For VLA: $\theta_{3dB} = 1.02/D$, First null = $1.22/D$

Antenna Performance Parameters

Pointing Accuracy

θ_{rms} = rms pointing error



Often $\theta_{\text{rms}} < \theta_{3dB} / 10$ acceptable

Because $\theta_{3dB} / 10 \sim 0.97$

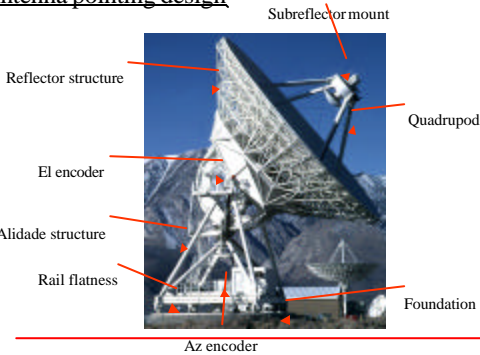
BUT, at half power point in beam

$$\theta_{3dB} / 2 \times \theta_{3dB} / 10 / (\theta_{3dB} / 2) = \theta_{\text{rms}} < 0.5$$

For best VLA pointing use Reference Pointing.

$$\theta_{\text{rms}} = 3 \text{ arcsec} = \theta_{3dB} / 17 @ 50 \text{ GHz}$$

Antenna pointing design



ALMA 12 m Antenna Design

Surface: $\sigma = 25 \mu\text{m}$

Pointing: $\theta_{\text{rms}} = 0.6 \text{ arcsec}$

Carbon fiber and invar reflector structure

Pointing metrology structure inside alidade

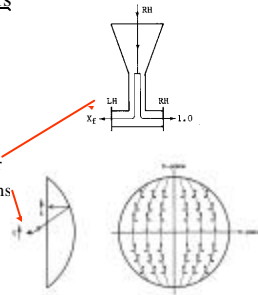


Antenna Performance Parameters

Polarization

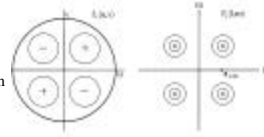
Antenna can modify the apparent polarization properties of the source:

- Symmetry of the optics
- Quality of feed polarization splitter
- Circularity of feed radiation patterns
- Reflections in the optics
- Curvature of the reflectors



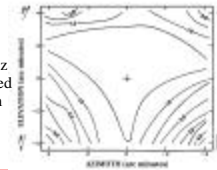
Off-axis Cross Polarization

Cross polarized aperture distribution



Cross polarized primary beam

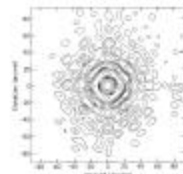
VLA 4.8 GHz cross polarized primary beam



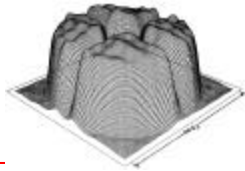
Antenna Holography

VLA 4.8 GHz

Far field pattern amplitude
Phase not shown



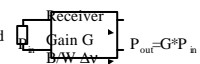
Aperture field distribution
Amplitude.
Phase not shown



Receivers

Noise Temperature

Matched load
Temp T (+K)



Rayleigh-Jeans approximation

$$P_{in} = k_B T_A \Delta\nu \quad k_B = \text{Boltzman's constant } (1.38 \times 10^{-23} \text{ J/K})$$

When observing a radio source $T_{total} = T_A + T_{sys}$
Tsys = system noise when not looking at a discrete radio source

T_A = source antenna temperature

$T_A = \eta AS / (2k_B) = KS$ S = source flux (Jy)

SEFD = system equivalent flux density

SEFD = Tsys/K (Jy)

EVL A Sensitivities			
Band (GHz)	B	T _{sys}	SEFD
1-2	50	21	236
2-4	62	27	245
4-8	60	28	262
8-12	56	31	311
12-18	54	37	385
18-26	51	55	606
26-40	39	58	336
40-50	24	78	1290



Corrections to Chapter 3 of Synthesis Imaging in Radio Astronomy II.

Equation 3-8: replace u,v with l,m

Figure 3-7: abscissa title should be λ/D

