

**ALMA Memo. No. 477**

## **Notes on Axis Intersection for MMA Antennas**

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### **1 Introduction**

This memo incorporates some notes I wrote down on 1998-Dec-10 when Peter Napier asked me to look into the problem of specifying the axis intersection quantities (two angles and a separation) for the MMA antennas. I provide no further information than what is directly in the notes, but it seemed that the information therein should be retained historically, so I've made this electronic version.

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①

Some notes on azimuth & elevation axis  
non-intersection for MMA

much of this is based on Cam Wade's memo  
(VLA Test Memo # 104)

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first, what if angles are not precisely  $90^\circ$ ?  
I've drawn on Cam's figure 1 the angles  
that we are specifying for MMA antennas  
( $\theta_1$  &  $\theta_2$ ).

If  $\theta_2 \neq 90^\circ$ , this simply mimics an azimuth  
pointing offset, and can be handled as such,  
I think.

If  $\theta_1 \neq 90^\circ$ , this changes the vector  $D$   
which connects  $P$  to  $P'$  (see figure). If we  
let  $\theta_1 = 90^\circ - \psi$ , and assume  $\psi$  is small so  
that  $\cos \psi \sim 1$  and  $\sin \psi \sim \psi$ , then,

$$D \cong \begin{bmatrix} (a - b \sinh) \cos z + (c - b \psi) \sin z \\ -(c - b \psi) \cos z + (a - b \sinh) \sin z \\ c \psi + b \cosh \end{bmatrix}$$

this adds some terms (involving  $b\psi$  &  $c\psi$ )  
to the fringe phase error:

$$\Delta \phi = \alpha \cosh - \Delta h (\alpha \sinh - \beta) - \gamma \Delta z \cosh + \Delta \phi_0$$

the  $\Delta \phi_0$  are the additional terms:

$$\begin{aligned} \Delta \phi_0 &= \beta \psi \Delta h \cosh + \gamma \psi (\sinh + \Delta h \cosh) \\ &= \psi \Delta h \cosh (\beta + \gamma) + \gamma \psi \sinh \end{aligned}$$

assuming  $\psi$  is small,  $\Delta \phi_0$  is negligibly small

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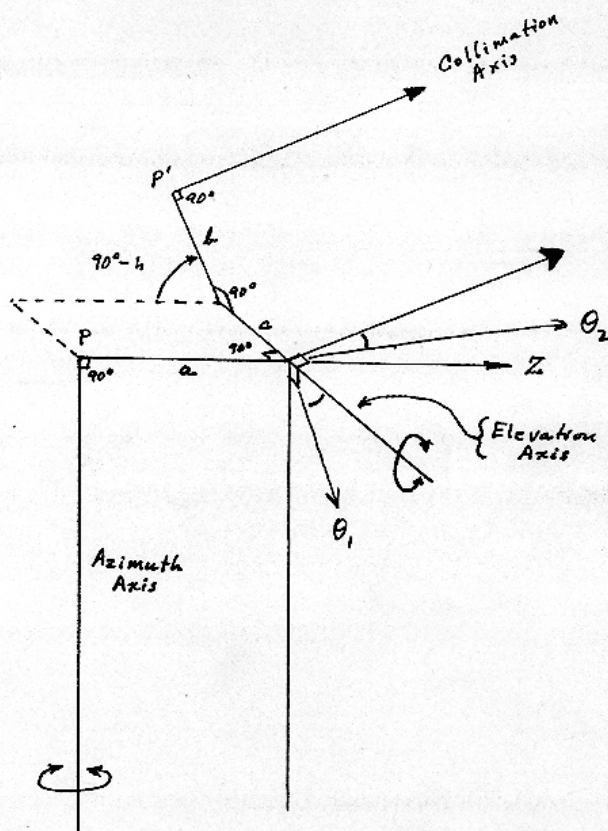


Figure 1 from Wade 1974

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Now, what if we make no attempt to measure  $a$ ,  $b$ , and  $c$  on the antennas, and rely on our secondary calibrator to account for  $\Delta\phi$ ?

in the simplest case, assume that at  $t=0$ , we measure phase on a calibrator at elevation  $h_{c_0}$ , then after some interval  $\Delta t$ , we measure it again (at elevation  $h_{c_1}$ ). if we use simple linear interpolation of these measured phases, and apply them to the source visibilities, we get an error like:

$$\begin{aligned}\Delta\phi_k(t) &= \alpha \cos[h_s(t)] - \phi_e(t) \\ &= \alpha \left\{ \cos[h_s(t)] - \left[ \cos h_{c_0} + \frac{\cos h_{c_1} - \cos h_{c_0}}{\Delta t} \cdot t \right] \right\}\end{aligned}$$

i.e., there is some error due to the calibrator not being at the same elevation as the source, and some due to approximating a cosine by a linear interpolation.

← { as long as  $\Delta t$  is relatively small ( $\leq 30$  mins) the error due to the different source and calibrator elevations dominates. in this case,

$$|\Delta\phi_k|_{\max} \lesssim \alpha \delta h \sin h_{\max}$$

where  $\delta h$  is the elevation difference between source & calibrator.

what to use for  $\delta h$ ?

based on Bob Brown's noise temps (in his SPIE paper), and Scott Foster's derived distances to calibrators at 90 GHz (MMA memo 124), and a scaling for source number counts which goes like:

unless the variation of elevation due to time causes phase to go through  $\approx \frac{1}{2}$  turn. (so that you can't interpolate  $\phi_e$  correctly).  
30 min  $\rightarrow$  7.5 deg, so about same constraint (of same order anyway) as derived on next page...

$$N_{\nu} \propto S_{\nu}^{-1.5} \nu^{3.5}$$

(see Kitayama et al. for  $S_{\nu}$  scaling, and Franceschini et al. for  $\nu$  scaling)

and assume you need 10 $\sigma$  per baseline in a 1 min calibration scan, then you might have the following:

$\nu$ (GHz)	$\delta h$ (deg)
115	1.5
230	0.6
345	0.4
410	0.4
675	0.6

this is for 90% of sources...

these numbers seem a bit small. let's assume that  $\delta h$  might be as large as 3 deg. let us also assume that we want  $|\Delta\phi_x|$  to be less than 20° (1/8 turns). then:

note that this  
fundamentally  
limits  
astrometry...  
(this  
error, if  
left  
unaccounted  
for)

$$\frac{1}{18} \approx \alpha \cdot 0.052$$

$$\Rightarrow \alpha \leq 1.1$$

at MMA's shortest wavelength (850 GHz)  
-  $\lambda \sim 350 \mu\text{m}$ , so

accuracy of  $a \lesssim 200 \mu\text{m}$

REMEMBER THAT THIS IS ONLY  
NEEDED IF  $\alpha_{\text{cash}}$  IS NOT  
MEASURED/CALIBRATED

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(4)

what if we measure/calibrate the  $\alpha \cosh$  term, but ignore the rest?

NOTE: this is what the VLA does - this is the so-called k-term correction. It is measured every year or so, when in C or D-config, and is usually quite stable over time. The measurement of  $\alpha$  (a) is made possible by being able to go OTT. This makes  $\alpha$  (a) easily distinguishable from other baseline/pointing terms.

in this case, the residual phase is:

$$\Delta\phi'' = -\alpha \Delta h \sinh + \beta \Delta h - \gamma \Delta z \cosh$$

use this to constrain a, b & c separately...

$$\Delta\phi_a'' = -\alpha \Delta h \sinh$$

$$\text{let } h \rightarrow 90^\circ, \Rightarrow \sinh \rightarrow 1$$

$$|\Delta\phi_a''| = \alpha \Delta h$$

$\alpha = a/\lambda$ , and let  $\Delta h$  be some multiple of HPBW ( $\Delta h = n\lambda/D$ ), then

$$|\Delta\phi_a''| \sim an/D$$

let  $D=10$  m and  $|\Delta\phi_a''| \leq 20^\circ$  ( $\frac{1}{18}$  turns,  $\frac{\pi}{9}$  rad)  
and  $n \sim 10$ , then

$$\text{accuracy of } a \leq 3 \text{ cm}$$

Similar constraint for b & c, so this is unimportant... (relatively)

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what about decorrelation due to  $\alpha \cosh$  term?

even if you correct for  $\alpha \cosh$ , you have to worry about how much it changes over an integration cycle. the change in  $\alpha \cosh$  over 1 integration is roughly:

$$\Delta(\alpha \cosh) \sim \alpha \Delta h$$

with the <sup>max</sup> elevation change given by:

$$\Delta h \sim \frac{2\pi \Delta t}{86400} \text{ rad}$$

for integration time  $\Delta t$  sec. if we want the error over an integration cycle to be less than 20 deg, then,

$$\alpha \times \frac{2\pi \Delta t}{86400} \lesssim \frac{20}{360}$$

$$\Rightarrow \alpha \lesssim \frac{760}{\Delta t} \text{ turns}$$

at 350  $\mu\text{m}$ , this corresponds to:

$$\text{accuracy of } a \lesssim \frac{130}{\Delta t} \text{ mm}$$

e.g. @  $\Delta t = 10$  sec,  
accuracy of  $a \lesssim 1.3$  cm

if this is not satisfied, given eventual values for  $a$  and  $\Delta t$ , then we may need a 2<sup>nd</sup> order  $\alpha \cosh$  correction (provide  $\alpha \cosh$  and  $\frac{\partial}{\partial t} \alpha \cosh$  to fringe frequency

calculator - this is how VLA-PT will be done).

[other refs: Wade, *ApJ*, 167, 381  
Sovers et al., *Rev. Mod. Phys.*, 70, 1393]